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RADC-TR-76-261, Volume I, Part 1, Book 1  
Final Technical Report  
October 1976



SPACE SURVEILLANCE SOFTWARE SUPPORT  
Project Summary and Computer Program Documentation

PRC Information Sciences Company

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ROME AIR DEVELOPMENT CENTER  
AIR FORCE SYSTEMS COMMAND  
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <i>The objective of this effort was to modify the RADC trajectory program orbit program and various radar cross section programs were modified to run on the RADC HIS 6180 computer under the GCOS system software. The RADC trajectory program was modified to include the capability of processing multiple (20) radar sites and multiple (20) targets in the program so that various radar parameters could be determined. This type of information is essential in performing radar coverage analyses for systems such as COBRA TALON, SEEK SAIL, COBRA DANE and COBRA JUDY. This portion of the effort is documented in Vol 1</i>		

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Line 20 (continued)

Vol VI documents a procedure for punching cards in ASCII format and reading the data onto a HP cassette for subsequent plotting with an HP9820 calculator system.

Vol VI documents some Radar Signature and Radar Scattering computer programs. A three dimensional plot program contained in this volume has been incorporated into the Interactive Radar Simulator for plotting three dimensional antenna patterns and cross section aspect angle histories.

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## ABSTRACT

The objective of the effort documented herein was to provide computer programming support for Space Surveillance system analysis. The two primary tasks of the effort were to complete the modification of the RADC Trajectory Program and to modify various radar cross-section and other computer programs so that they could be accessed from the interactive system for the RADC Radar Simulator. The documentation is organized as follows:

Volume I, Part 1, Book 1 - Project Summary and Computer Program Documentation (Chapters I-III of Volume I, Part 1)

Volume I, Part 1, Book 2 - Computer Program Documentation (Chapter IV)

Volume I, Part 1, Book 3 - Computer Program Documentation (Chapters V-VI and Appendices A-E)

Volume I, Part 2 - RADC Trajectory Program - Numerical/Analytical Data

Volume II - Generalized Data Entry and Plot Program

Volume III - Radar Signature and Radar Scattering Principles Investigation Software

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## EVALUATION

The objective of this effort is to provide RADC systems engineers with the software commonly required for systems studies and the necessary software for plotting the data. The RADC trajectory program was modified to handle multiple targets and multiple radar sites. This program is required to perform coverage analyses for radar surveillance systems and has been used in support of SEEK SAIL, COBRA TALON and COBRA DANE. The cross section programs are used to determine the cross sections of targets that a radar system would be required to detect.

Since the RADC computer facility does not have a means of plotting data, most of the computer data generated was of limited value and extremely time consuming to use. Vol II documents a procedure for punching cards in ASCII format and reading data onto an HP cassette for subsequent plotting with an HP 9820 calculator system. This capability has proven extremely useful.

Vol III documents some Radar Signature and Radar Scattering computer programs. A three dimensional plot program contained in this volume has been incorporated into the Interactive Radar Simulator for plotting three dimensional antenna patterns and imaged wideband cross section data. These programs can serve as a starting point in the Tactical Target Identification Program.



JOHN C. CLEARY  
Project Engineer

## I. Introduction

### A. Purpose and Scope

This document is Volume I, Part 1 of the technical report and computer program documentation for the Space Surveillance Software Support Contract, F-30602-75-C-0167, and is submitted in fulfillment of items A002 and A003 of the contract data requirements list. The work represented herein has been performed by Information Sciences Company (ISC) of Planning Research Corporation (PRC).

Contained herein are a summary of the work done on the project in the modification of the RADC Trajectory Program and others and the documentation for all computer programs modified.

### B. Document Organization

Volume I, Part 1 is organized as follows:

Chapter II is, basically, the project summary. Appropriate exhibits are interleaved with the text material.

Chapters III and IV contain descriptions of the trajectory computer programs and radar cross-section computer programs, respectively. Included are source listings, sample test cases, and sample output from the test cases.

Chapter V contains descriptions of several auxiliary programs developed during the project, while chapter VI gives a list of references.

Appendices A through E contain analyses relating to the trajectory programs and descriptions of several small radar simulation-type programs.

Volume I, Part 1 is subdivided into 3 Books, Book 1 containing Chapters I-III, Book 2 containing Chapter IV, and Book 3 containing Chapters V-VI and Appendices A-E.

## II. Space Surveillance Software Support Project Summary

### A. Project Overview

The essential purpose of the Space Surveillance Software Support project was to provide computer programming support to aid Space Surveillance system analysis. This support took the form of modifying numerous, existing trajectory and radar-cross section programs and implementing them on the Honeywell 635 and 6180 computers at RADC. These programs were written in FORTRAN Y and placed in the appropriate time-sharing CARDIN format so that they could be accessible from the interactive system for the RADC Radar Simulator.

The work on the project was divided into two major task areas. One of these tasks was to bring the modification of the RADC Trajectory Program to a completion; the initial modification of the program was performed under Contract F30602-72-C-0136. This second modification included the capability of processing multiple radar sites and multiple targets in the program so that various radar parameters could be determined. The trajectory program can now accommodate up to 20 different radar sites and up to 20 targets.

The second task consisted of the modification and implementation of a number of trajectory, target model, and radar cross-section programs. There were 12 programs, altogether, involved in the task, and they were made executable via the remote batch system (CARDIN) of the RADC Honeywell computers. The 12 programs were the: Cobra Talon Trajectory Program, Nodal Crossing Prediction Program, Orbit Prediction Program, Cone Program, Cone-Cylinder Program, Frustum Program, Frustum-Cylinder Program, Hemisphere-Cylinder Program, Radar Scatter from Missile Program, Dihedral Corner Reflector Program, Cylinder Program, and Cylinder-Flare Program.

### B. Program Development

The required modifications to the various computer programs and their

implementation on the Honeywell computing system were carried out in a certain manner. The procedure followed with respect to the two major tasks of the project will be described in the following paragraphs.

1. Modification of the RADC Trajectory Program

It was realized initially that the plotting capability had to be restored to the RADC Trajectory Program in order to make full use of it. The XYNECTICS plotter, by which plots of radar data were produced for the version of the program as modified under the original contract, was no longer available. However, the Hewlett-Packard 9820A calculator/plotter, with the capacity to read data cards was available. What was done was to write a short program to read the plot file created by the trajectory program and to punch out the file data onto cards for plotting on the HP9820A. This short program served as the basis of another plot program which could read the plot file created by the multiple site/multiple target version of the trajectory program and which was used quite often.

After checking that the first modified version of the trajectory program executed correctly, a detailed flow-chart of the major processing within the program was drawn up. This flow-chart was to serve as a basic reference for making further modifications to the program. It was thought that the modification involving multiple radar sites would be easier (less complicated) to include first in preference to that involving the multiple targets, and this is what was done. The multiple site addition was thoroughly tested using the results produced from prior, valid computer runs. The additional capability of printing out a message to the effect that an object was not detected by a radar site, when this was the case, was also incorporated. Next, the multiple target (or trajectory) capability was implemented. Basically, this involved putting an outer loop around the processing of the program; the multiple site modification had been made to process a single target only. Again, the multiple target addition to the program was carefully checked using previous, good computer runs.

After check-out of the multiple target/multiple site modification, other capabilities were added to the program. An atmospheric model for

simulating atmospheric effects on missiles was included and tested. This model was essentially the one that was in the original, unmodified version of the program. The generation of circular orbit trajectories with the program was tested, and the option to select either inertial velocity or burnout velocity was added. Finally, inclusion of radar parameter difference computations for multiple sites and trajectories was worked on.

## 2. Modification of Other Programs

The discussion here generally refers to all programs modified except the RADC Trajectory Program. These programs consisted of 3 trajectory-type programs and 9 target model or radar cross-section programs. The basic procedure which was followed in modifying these programs and implementing them on the Honeywell system is given below.

The existing source deck for a program was loaded on a disc file, compiled, and compilation errors were eliminated. Routines common to several programs were removed from the programs and processed separately. An attempt was then made to execute the error-free object form (also on a disc file) of the program using a given input test case. The results were compared against results obtained from previous, reliable runs of the program. If the results compared favorably, then the program inputs were converted to NAMELIST format, where it had not already been done so, in order to facilitate the use of the CARDIN system for program execution. When the results did not check out, a search was made for program and/or load errors, and after being found and corrected, then the input conversion to NAMELIST was made. The NAMELIST conversion was also tested through computer runs. The last thing that was done to a program was to produce plots of its computations as a final output and check-out. In most cases this meant adding a subroutine to the program to place the required data on a file so that it could be punched onto cards later. In addition, it should be mentioned that each program was executed in the CARDIN system by means of their respective job streams which had been placed on file.

### C. Program Usage

This is a general discussion indicating how to use the programs which have been implemented under this contract. The reader should refer to other chapters of this volume for more detail.

#### 1. RADC Trajectory Program

After the user selects the appropriate missile, radar, etc. input parameters, he must decide what input options to exercise. Basically, these options will be determined by what type of run he desires and what output he wants. Incidentally, in choosing values for the missile parameters (initial velocity, re-entry angle, etc.), the reader is referred to the appendices, Part 2 of this volume, section II.E, and other documents which may have been produced on the subject. By selecting appropriate values for the main processing switch, NSWTCH, and the plotting options, IPLOT1 or IPLOT2, the user can, for the most part, control the flow of a program execution and the output from it for immediate and/or later use. NSWTCH = 0 will cause the computation of trajectory parameters only, the printout of them, and the storage on a file of those needed for determining radar parameters. No radar computations will be made when NSWTCH = 0. By setting NSWTCH = 1, the program will produce trajectory data, storing appropriate parameters on a file as for NSWTCH = 0, and will calculate radar parameters (range, azimuth, etc.) for each of the input radar sites. NSWTCH = 2 will cause the generation of radar data, only, from trajectory data placed on file when NSWTCH = 0 or 1. By setting either plot option, IPLOT1 or IPLOT2, equal to .TRUE., the user can have radar data placed on a plot file for later access in producing plots. For this purpose, cards would be punched out from the file through the use of a short auxiliary program (1st program of Chapter V), and they would be plotted on the HP9820A by means of the Generalized Data Entry and Plot Program.

#### 2. Other Trajectory Programs and Target Model Programs

Most of these programs do not have any input options so that their use is relatively straight-forward. The possible exceptions are the Cobra Talon Trajectory Program which requires the setting of such switches

as those for selecting the nominal trajectory and inertial velocity and the Orbit Prediction Program which has a switch for putting data on a plot file. The basic procedure in running any one of the programs would be to choose desired values for the input parameters, enter them in the appropriate job stream file, and execute the job stream via CARDIN and the Honeywell 6180 computer. A plot file is created automatically when a target model (cross-section) program is executed. If one desires the file to be punched onto cards, the BPUNCH subsystem of CARDIN can be utilized as each file is written in BCD format. For the Cobra Talon and Orbit Prediction Programs, if it is desired to punch out their plot files, the appropriate auxiliary punch programs would be employed.

#### D. Conclusions

There are several accomplishments of this project which have resulted from the work performed:

The RADC Trajectory Program has been made into a more efficient tool for the performance of radar system analysis. It can now process up to 20 different radar sites and up to 20 targets (or trajectories) and determine radar coverage parameters. Data from multiple trajectories can be permanently stored on a file and used many times over for computing radar parameters. This would result in considerable saving of computer time as the trajectory generation is by far the most time-consuming process in the program. Plots of radar data can now be made on the HP 9820A calculator/plotter. Refer to Figure II-1 for an example of such a plot. Also, the RADC Trajectory Program has been implemented on the Honeywell 6180 CARDIN subsystem, so that it is executable by means of the interactive system for the RADC Radar Simulator.

The target model programs have been checked out on the Honeywell 635 and 6180 computers and made accessible through the remote batch CARDIN subsystem. The capability of storing data for plotting was also added to these programs. The Cobra Talon Trajectory Program had several corrections made to it while it was being implemented on the CARDIN system. It also was given the added capability to generate circular orbits. In addition, the Orbit Prediction Program (as well as the Cobra Talon Program) was

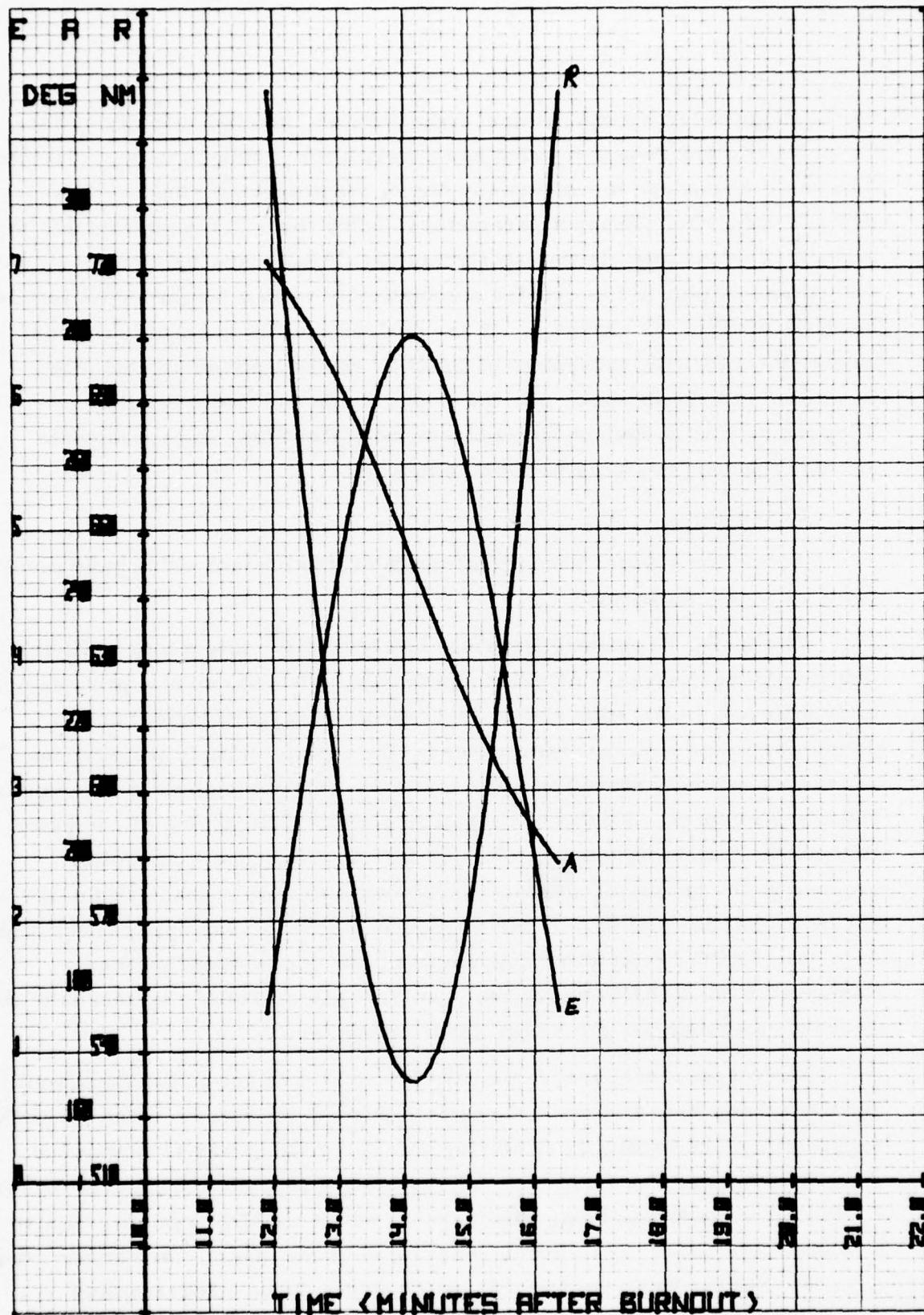


Figure II-1. Plot from RADC Trajectory Program

provided the capacity for obtaining plots of its results, and both it and the Nodal Crossing Prediction Program were made executable via CARDIN.

In the course of modifying and implementing the many programs involved in this project, several computer runs were attempted in which a spaceborne radar system was simulated. A plot from one of the runs, showing the decrease in range of a missile as it approaches impact at the radar, is illustrated in Figure II-2.

Several observations concerning the RADC Trajectory Program can be made; some of them may also apply to the Cobra Talon Trajectory Program. Most of the major trajectory and radar computations in the program are currently performed in double precision floating point. It might be worthwhile to perform an experiment on the program with the computations changed to single precision. If the experiment is successful, the benefit would be a significant reduction in both computer processing time and required memory. In the modified program, the trajectory data stored on file was in single precision; radar computations made with this data showed no noticeable difference from those made with double precision data. The basic integration time for trajectory iterations was set at 0.01 min. In the original program this time changed according to certain conditions, e.g., altitude of missile below a certain level. Results from the modified program were compared, in several instances, against corresponding results from the original program for which the integration time varied and no significant difference was discovered.

#### E. Trajectory Computer Programs

The trajectory computer programs deserve special attention here because they are the most important and widely used of the programs worked on for this project. This section could be considered as an introduction to their detailed description in chapter III and the analyses of Appendices A through E and Volume I, Part 2. Most of the following paragraphs have been excerpted from the "Cobra Talon Study Computer Programs" document (see References). Updates have been inserted in the text where appropriate.

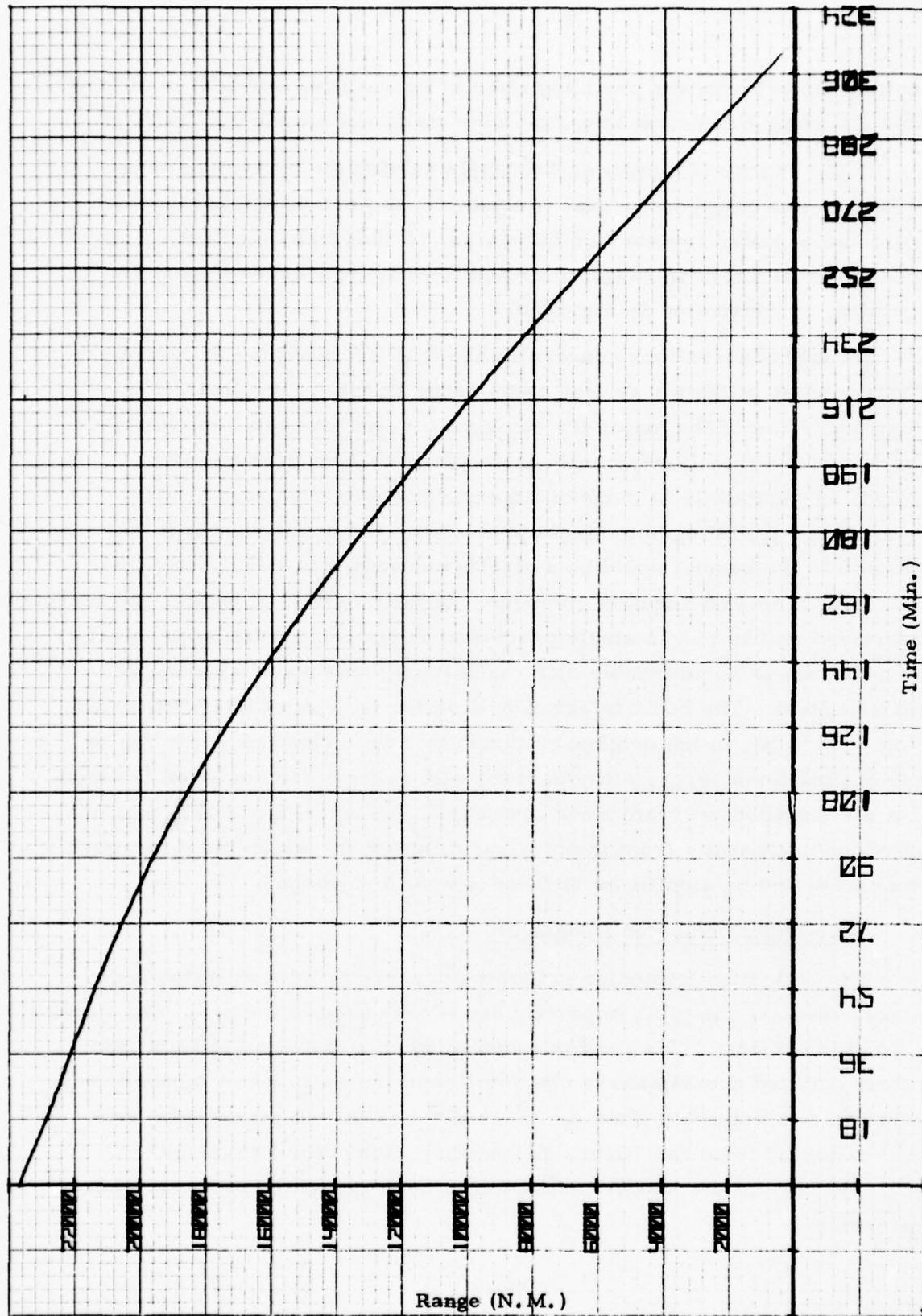


Figure II-2, Spaceborne Radar

A missile trajectory computer program developed at RADC\* had been modified to zero-in on a specific impact point. This is accomplished by utilizing the position and velocity vectors at the actual impact point as new initial conditions. Then the actual impact point is moved to the desired impact point and run backwards to burnout, which is time zero. Thus, a new set of initial burnout conditions is obtained for the third trajectory which zeros in on the desired impact point. This is of particular interest for reentry radars. Additional trajectories can be run which are perturbed from the nominal trajectory (i.e., the third trajectory); the radar differences from the nominal trajectory (3rd) are then printed out. This option is obtained by setting the FORTRAN variable KZ=0 in the Cobra Talon Program and = F in the RADC Trajectory Program.

In a study which OCSA was required to perform, the launch point and missile capability were known. Therefore, the above computer program was modified\*\* so that the launch point was not changed. The impact point was allowed to stay where the missile capability put it. This means that the first trajectory was made the nominal trajectory. The second and third trajectories were skipped and additional trajectories were perturbed from the first trajectory. This option is obtained by setting KZ=1 in the Cobra Talon Program and = T in the RADC version.

The original program\*\*\* was such that every time initial burnout conditions were changed, the computer program was changed. This computer program was changed to accept input data without changing the computer

\* See Reference 4, Page VI-2

\*\* See Reference 3, Page VI-2

\*\*\* See Reference 4, Page VI-2

program every time. This allows the time-sharing system to be used for production runs. The computer program was also modified to print-out all the input conditions for future reference.

To determine the radar coverage parameters a separate version of the trajectory computer program was utilized which prints the missile trajectory and radar coverage data every tenth of a trajectory minute. In addition, the radar slant range is printed out in nautical miles. For the case where differences are calculated, a second version of the computer programs prints out data for every trajectory minute. Also, the differences in radar slant range from the nominal trajectory are printed in feet. The original computer program was modified to calculate the total angular separation in the radar beam from the nominal trajectory.

The outputs of the computer program can be used to determine the radar systems information needed to fill in Table II-1 .

To simulate missile trajectories, burnout velocities referenced to the earth's surface are required; therefore, set the FORTRAN variable INERTL = 0. If satellite orbits are to be simulated, inertial velocities must be used; therefore, set INERTL = 1. This causes the earth's rotation ( $\omega$ ) to be subtracted from  $\lambda$ , the total longitude angle velocity component of the vehicle which is in subroutine ICERBM(P) as the FORTRAN variable XD(3). When a simulated trajectory is required for a specified inclination (INC) angle, the missile heading angle BETA measured clockwise from north has to be calculated. Figure II-3

LAUNCH AZ ° FR TRUE NO.	INIT DET RANGE NM	MIN. DET RANGE NM	MAX DET RANGE NM	FINAL DET RANGE NM	MAX EL ANGLE DEG	TOT AZ ANGLE DEG	MAX RANGE RATE NM/ SEC	MAX EL RATE DEG/ SEC	MAX AZ RATE DEG/ SEC	TOT OBS. TIME MIN
100										
120										
170										
190										
200										
230										

EXPLANATORY NOTES:

1. Unless otherwise specified, the numbers in parenthesis list time (min. after burnout) at which value would be observed.
2. The total Az Angle is the az angle required by radar to observe missile from horizon to horizon (0.5° el. angle). The numbers in parenthesis indicate initial and final detection azimuths (true North) from radar site.
3. The Total Observation Time is the time target would be within radar field-of-view. In parenthesis are cited initial and final observation times.

TABLE - II-1. Radar Systems Information Chart

Section III. B. documents the PRC version of the RADC Trajectory Program. PRC's effort was directed towards making the program run more efficiently on HIS 6180 and making the program relatively easy to use for the user. This version of the program can handle multiple trajectories for multiple radar sites. To save computer run time the trajectories of interest can be stored on disc and/or magnetic tape. Then coverage parameters for the radar sites of interest can be handled. Since the trajectory simulation requires the greatest amount of computer time this is more efficient and allows other radar sites which may come into consideration at a later date to be easily included.

Appendix A discusses the ejection velocity geometry used for multiple trajectories. Other appendices discuss procedures for determining burn-out velocity input parameters for the missile case. The inertial velocity for orbital cases is determined from\*

$$VI = \sqrt{\frac{\mu}{a}} \quad (\text{circular orbit})$$

$$VI = \sqrt{\mu \left( \frac{2}{r} - \frac{1}{a} \right)} \quad (\text{elliptical orbit})$$

$$\text{where } r = \frac{a(1-e)^2}{1+e \cos\theta}$$

$\theta$  = true anomaly = angular position along orbit referenced to perigee

$$\mu = 5.0675004 \times 10^{19} \text{ ft}^3/\text{min}^2$$

\* See "Radar Handbook" by Skolnik

$\mu = 1.407639 \times 10^{16} \text{ ft}^3/\text{sec}^2$

$R_E = 2.0925640 \times 10^7 \text{ ft}$  (earth's equatorial radius)

$e$  = orbit eccentricity ( $e = 0$  for circular orbit)

$a$  = semi-major axis

$r$  = distance from earth's center to satellite/missile position

Section III. C. documents the Cobra Talon version of the RADC Trajectory Program. This version has the capability of handling multiple targets ejected from the nominal trajectory for a single radar site.

### III. Description of Trajectory Computer Programs

#### A. Introduction

This section provides a description for four (4) simulation-type computer programs which have been written in FORTRAN Y to execute under the Honeywell 6180 GCOS operating system. These programs, basically, generate trajectories for missiles and satellites and determine radar coverage parameters and are the following:

1. RADC Trajectory Program
2. Cobra Talon Trajectory Program
3. Nodal Crossing Prediction Program
4. Orbit Prediction Program

Program 1 is a second modification of the general perturbation program of George A. Ellis, the initial modification of which was done under Contract F30602-72-C-0136. Program 2 is essentially the version of Mr. Ellis' program which was used in conjunction with the Cobra Talon radar study by John C. Cleary and Leonard C. Gratch. Refer to sections III. B and III. C for documentation and further references on these programs. Programs 3 and 4 were developed under the direction of Mr. Cleary for predicting the path of an earth-orbiting satellite and determining radar look-angles for it. Sections III. D and III. E document these programs and mention a reference for them. All the programs have been put in the appropriate time-sharing CARDIN format by PRC/ISC so that they are executable by means of the RADC Interactive Radar Simulator.

B. RADC Trajectory Program

1. Introduction

This computer program is a second modification of the general perturbation program (PROGRAM TRAJ) of George A. Ellis, previously modified under Contract F30602-72-C-0136. The previous modification retained much of the mathematics and basic processing methodology of the Ellis program but differed primarily in its input/output capabilities and increased modularity. More input flexibility and capacity for generating trajectory data (relative to a radar site) for use with an off-line plotter were major characteristics of the first modified version. This second refinement of the program brought the modification of the RADC Trajectory Program to completion. The capacity for accommodating multiple DSSR sites and multiple targets has been added to the program, while still maintaining the capabilities of the first modification.

The basic function of the program is to generate the trajectory of a ballistic missile or an earth-orbiting satellite. It predicts the position, velocity, and acceleration of the vehicle and can compute radar parameters (range, azimuth, elevation, etc.) relative to a number of radar sites. The user has the option of producing just trajectory data and no radar data, or both trajectory and radar data, or just radar data from trajectory data stored during a previous run. The reader is referred to a number of documents describing prior versions of the program. Several of these are: "Missile/Satellite Trajectory Program" April 1974, a user's guide by R. Conti, PRC; "Simulation Program for Three Degrees of Freedom Trajectories", Technical Memorandum No. EMA-TM-66-5, Sept. 1966, by George A. Ellis, et al; "Cobra Talon Study Computer Programs", Technical Memorandum RADC/OC-TM-71-4, May 1971, by John C. Cleary and Leonard C. Gratch. Also, refer to the analytical description in Volume I, Part 2 of this report.

2. Computer Program Operating Environment

a. Computer

Honeywell 6180.

b. Source Language

FORTRAN Y under GCOS.

c. Memory Requirement

40K words.

d. Typical Processing Time Required

0.12 hours (432 seconds)

e. Peripheral Equipment Requirement

One disc file (file code: 08)

Three disc or tape files (file codes: 09, 10, 11)

f. Non-system Subroutines Required

ATMOSP	Atmospheric model.
BALCOF	Ballistic coefficient subroutine.
CONVER	Conversion to radar coordinates.
EQTNX	Computation of acceleration components.
ICERBM	Computation of geocentric spherical components.
INITAL	Initialization subroutine.
INTRAJ	Input trajectory and radar data stored on files for computations.
INPUT	Input subroutine.
OUTPUT	Output subroutine.
RKG	4th Order Runge-Kutta-Gill.

g. Program Limitations

The program can accommodate no more than 20 perturbed trajectories.

The maximum number of trajectories which can be generated will vary with the selection of the nominal trajectory. When the nominal trajectory for the trajectory perturbations is the first trajectory,

the first trajectory and up to 20 perturbed trajectories can be generated, for a total of 21. When the nominal trajectory is the third trajectory, there will be generated the first, backward, and third trajectories, and up to 20 perturbed trajectories, for a total of 23.

The program can accommodate no more than 20 different radar sites.

For the radar parameter difference calculations, no more than 10 different trajectories, 10 different radar sites, and 5 different sightings of a trajectory by a site are allowed.

### 3. Inputs

The following two sets of inputs (INPUT1 and INPUT2) are for the program controls.

#### NAMELIST INPUT 1

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NTRAJ	None	Total number of trajectories simulated. If KZ = T, the actual number of trajectories simulated will be NTRAJ-2. NTRAJ cannot exceed 23.
TM	Min.	Maximum time allowed for any trajectory from start to finish.
NSWTCH		Main processing switch for the program.
0		Produce trajectory data only. The data for each trajectory generated will be placed on a file for later access.
1		Produce both trajectory and radar data. The trajectory data will be placed on a file.
2		Produce radar data only.

#### NAMELIST INPUT 2

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
IOUT1		Printout option No. 1.
T		Print out the 13 trajectory parameters from the radius of the missile (or satellite) trajectory to the acceleration in longitude for each time point of each trajectory. The time points are spaced by OUTINC, and each trajectory is considered relative to a geocentric coordinate system.

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
	F	Print out the 7 trajectory parameters from the radius to atmospheric density for each time point of each trajectory generated.
IPLOT1		Plotting option 1.
	T	Produce a plot file of the 8 radar parameters from slant range to inertial phi for each time point of each detected trajectory. This plot file consists of data produced from all input radar sites.
	F	Do not produce this plot file.
IPLOT2		Plotting option 2.
	T	Produce a plot file of the 13 radar parameters (calculated for each site) from slant range to heading angle for each time point of each detected trajectory.
	F	Do not produce this plot file.
IOUT2		Printout option 2.
	T	Print out the 13 radar parameters from slant range to heading angle for each time point of each detected trajectory. The radar parameters of each trajectory are computed relative to the input radar site coordinates.
	F	Print out the 8 radar parameters from slant range to the inertial phi angle for each time point of each detected trajectory.
KAT		Atmospheric model option.
	T	Use the atmospheric model. Atmospheric effects will be considered in the generation of the trajectories.

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
	F	Do not use the atmospheric model.
KZ		Nominal trajectory selection switch.
	T	Select the 1st trajectory as the nominal trajectory for the trajectory perturbations.
	F	Select the 3rd trajectory as the nominal trajectory.
SPHERE		Spherical earth model option.
	T	Use the spherical model of the earth.
	F	Do not use the spherical model.
IOUT3		Printout option for radar parameter differences.
	T	Print out the radar parameter differences.
	F	Do not print out the differences.
OUTINC	Min.	Increment between time points for printout.
INERTL		Inertial velocity option.
	T	The initial missile velocity input is the inertial velocity.
	F	The initial velocity is the burnout velocity.

Note: The spherical model of the earth is the only one currently present in the program, so that the value of SPHERE has no effect on a program run. Also, IPLOT1 and IPLOT2 cannot be simultaneously true. Only one can be true and the other false, or both can be false.

The following set of inputs are for the initial state vector of the interceptor and the subsatellite parameters.

NAMELIST INPUT3

<u>Symbol Name</u>	<u>Unit</u>	<u>Description</u>
GAM	Deg.	Re-entry angle of the missile with respect to the vertical.
BETA	Deg.	Heading angle of missile w. r. t. relative north.
VO	Ft. /Sec.	Velocity of the missile relative to burnout at epoch or inertial velocity of the missile.
HX	Ft.	Height of missile at burnout or initialization of trajectory.
THE	Deg.	Geocentric latitude at burnout, + north and - south of equator.
GLAM	Deg.	Geocentric longitude at burnout, east of Greenwich.
THES	Deg.	Geocentric latitude of the target (subsatellite), + north and - south of equator.
GLAMS	Deg.	Geocentric longitude, east of Greenwich, of the target.

Note: The inputs GAM through GLAM above could also be interpreted as parameters for an orbiting satellite, rather than a missile.

The following set of inputs describes the radar sites for which computations are to be made. INPUT4 is not read if NSWTCH = 0.

NAMELIST INPUT4

<u>Symbol Name</u>	<u>Unit</u>	<u>Description</u>
NSITE	None	The number of radar sites to be simulated. NSITE cannot exceed 20.

<u>Symbol Name</u>	<u>Unit</u>	<u>Description</u>
SLAT	Deg.	Geocentric latitudes of the radar sites, + north and - south of equator. SLAT is an array.
SLONG	Deg.	Geocentric longitudes of the radar sites, west of Greenwich. SLONG is an array.
SALT	Ft.	Altitudes of the radar sites above sea level. SALT is an array.
ELIM	Deg.	Maximum co-latitude of the elevation angle for which objects are detected by all the radar sites.

If NTRAJ > 3, the velocity perturbations are input:

#### NAMELIST INPUT5

<u>Symbol Name</u>	<u>Unit</u>	<u>Description</u>
A	Ft. /Sec.	Out of trajectory plane perturbation, + ejected to the left of the nominal trajectory. A is an array.
B	Ft. /Sec.	In plane perturbation, + ejected backwards from nominal trajectory. B is an array.
C	Ft. /Sec.	In plane perturbation, + ejected backwards from nominal trajectory. C is an array.

#### 4. Output

The output from the RADC Trajectory Program is a variable depending upon the selection of the program options. First, a printout of the input parameters for the program run is produced, this printout and the input parameters, themselves, varying according to the values of the options. Then follows the printout of the results of the program execution. The main processing switch for the program (NSWTCH) has a great deal of control over the type of output coming from the program. If NSWTCH=0, only trajectory data will be printed out. If NSWTCH=1, both trajectory and radar data will be produced. And if NSWTCH=2, only radar data will be outputted. The following lists indicate what printout is produced with what option values.

When NSWTCH=0 or 1 and IOUT1=.FALSE., the following printout of trajectory parameters for every trajectory generated is produced:

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NTRJ	None	Number of trajectory. When KZ=T, the second trajectory will be numbered 4.
TIME1+(I/IO) *OUTINC	Min.	Formula for the calculation of a trajectory time point for printout. The value calculated (and printed out) represents the time from burn-out of the missile along its trajectory or time from the initiation of the satellite orbit or missile path, if that is appropriate.
OUTTRJ(1)	Ft.	Earth-centered radius of the trajectory or the distance of the missile or satellite from the earth center at the time point above.

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
OUTTRJ(2)	Deg.	Position in latitude of the missile/satellite in its trajectory at the above time point.
OUTTRJ(3)	Deg.	Position in longitude of the missile/satellite, east of Greenwich.
OUTTRJ(4)	Ft.	Altitude above sea level of the missile.
OUTTRJ(5)	Ft. /Sec.	Inertial velocity of the missile/satellite along its trajectory.
OUTTRJ(6)	Ft. <sup>2</sup> /Slug	Ballistic coefficient at the time point.
OUTTRJ(7)	Slug/Ft. <sup>3</sup>	Atmospheric density at the trajectory time point for the missile/satellite altitude.

The trajectory parameters corresponding to the next time point to be printed out are stored in OUTTRJ(8) - OUTTRJ(14), and so on for each time point to be printed. NTRJ is printed at the top of a page of printout. The time point - OUTTRJ(7) are printed out on one line of a page, next time point - OUTTRJ(14) on the next line, etc., up to 52 lines per page. NTRJ will start the next page. Each successive time point printed out will differ by OUTINC from the previous one. This may not hold true for the very last time point as it may differ from the previous one by 0.01 min. or more.

If IOUT1 = .TRUE. and NSWTC=0 or 1, the following trajectory parameters are printed out:

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NTRJ		
TIME1+(I/IO) *OUTINC		
OUTTRJ(1)		Described for IOUT1=.FALSE.

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
OUTTRJ(2)		
OUTTRJ(3)		
OUTTRJ(4)		
OUTTRJ(5)		
OUTTRJ(6)		
OUTTRJ(7)		
OUTTRJ(8)	Ft. /Sec.	Geocentric radial velocity component of the missile/satellite at the time point.
OUTTRJ(9)	Deg. /Sec.	Geocentric latitude velocity component of the missile/satellite.
OUTTRJ(10)	Deg. /Sec.	Geocentric longitude component of velocity of the missile/satellite.
OUTTRJ(11)	Ft. /Sec. <sup>2</sup>	Geocentric radial acceleration component of the missile/satellite.
OUTTRJ(12)	Deg. /Sec. <sup>2</sup>	Geocentric latitude component of acceleration of the missile.
OUTTRJ(13)	Deg. /Sec. <sup>2</sup>	Geocentric longitude component of acceleration of the missile.

What was said above for the printout when IOUT1 = .FALSE. essentially holds for IOUT1 = .TRUE. The difference is that storage of the trajectory parameters is not the same. The trajectory parameters corresponding to the next time point to be printed out are stored in OUTTRJ(14)-OUTTRJ(26), and so on for each time point to be printed out.

The number and types of trajectories generated are basically controlled by the input variables NTRAJ and KZ. If only one trajectory is desired, NTRAJ would be set equal to one. If perturbed trajectories are desired with the nominal trajectory as the first trajectory, NTRAJ would be set  $\geq 4$  and KZ = .TRUE. The trajectories on the printout would be

numbered in the order 1, 4, 5, \_\_\_, number 4 representing the first perturbed trajectory. If perturbed trajectories are desired with the nominal trajectory as the third trajectory, NTRAJ would be set  $\geq$  4 and KZ = .FALSE. In this case the trajectories would be numbered 1, 2, 3, 4, \_\_\_. Trajectory 2 is the so called "backwards" trajectory, with time going in descending order.

Now if NSWTCH = 1 or 2, the following set of radar parameters will be printed out for each radar site and each trajectory detected by the sites. For NSWTCH=1, the radar data will follow the appropriate trajectory data printout. For NSWTCH=2, there will be no trajectory data printout, only radar data. There will be no radar data printout for the second trajectory and if a trajectory is not visible to a radar site, a message to that effect will be produced. For IOUT2 = .FALSE., the radar parameters printed out are:

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NTRJ	None	Trajectory number.
ISITE	None	Radar site number.
SC1	Deg.	Position in latitude of the radar site.
SC2	Deg.	Position in longitude of the radar site.
TIME2+(I/I01) *OUTINC	Min.	Trajectory time point. See description for IOUT1 = .FALSE. under trajectory data output.
OUTRAD(1)	N. M.	Radar slant range to the missile/satellite for the time point.
OUTRAD(2)	Ft. /Sec.	Slant range rate for the time point.
OUTRAD(3)	Deg.	Radar elevation angle for the missile/satellite at the time point.
OUTRAD(4)	Deg. /Sec.	Elevation angle rate.

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
OUTRAD(5)	Deg.	Radar azimuth angle, measured clockwise from north.
OUTRAD(6)	Deg. /Sec.	Azimuth angle rate.
OUTRAD(7)	e. r. u.	Trajectory radius in earth radii units.
OUTRAD(8)	Deg.	Inertial phi angle.

The radar parameters corresponding to the next time point to be printed out are stored in OUTRAD(9)-OUTRAD(16), and so on for each time point to be printed. NTRJ, ISITE, SC1, SC2 are printed at the top of a page of printout. The time - OUTRAD(8) are printed out on one line of a page, next time point - OUTRAD(16) on the next line, etc., up to 52 lines per page. NTRJ, ISITE, SC1, SC2 will start the next page. Each successive time point printed out will differ by OUTINC from the previous one, except that the difference between the first and second time points and the next-to-last and last could be less than OUTINC.

What was said in the previous paragraph applies to one sighting of the missile/satellite by a radar site. Each sighting of the missile/satellite by a site will have a group of printouts similar to what is described above. The first time printed out for a group represents the initial time of sighting by the radar for the current sighting (or current period in which the missile/satellite is in the radar coverage). The last time represents the time at which the missile was last visible to the radar for the current sighting. The printout of radar parameters, in this way, can reflect when a missile moves in and out of the radar coverage.

When IOUT2 = .TRUE. and NSWTCH=1 or 2, the following radar parameters are printed out:

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NTRJ		
ISITE		
SC1		
SC2		

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
TIME2+(I/IO1) *OUTINC		Described under IOUT2 = . FALSE.
OUTRAD(1)		
OUTRAD(2)		
OUTRAD(3)		
OUTRAD(4)		
OUTRAD(5)		
OUTRAD(6)		
OUTRAD(7)		
OUTRAD(8)		
OUTRAD(9)	Ft. /Sec. <sup>2</sup>	Radar slant range acceleration of the missile/satellite.
OUTRAD(10)	Deg. /Sec. <sup>2</sup>	Radar elevation angle acceleration.
OUTRAD(11)	Deg. /Sec. <sup>2</sup>	Radar azimuth angle acceleration.
OUTRAD(12)	Deg.	Missile re-entry angle.
OUTRAD(13)	Deg.	Missile heading angle.

Essentially what was said for the printout for IOUT2 = . FALSE. holds true for IOUT2 = . TRUE., except that the storage of data is different. For example, time point - OUTRAD(13) is printed on one line, next time point - OUTRAD(26) printed on the next line, etc.

#### Radar Parameter Differences

The radar parameter difference calculations, as of this writing, have not been fully implemented. The following discussion will describe the output as it will be produced from the calculations.

If IOUT3 = . TRUE., the program will compute radar parameter differences and print them out, after the last set of trajectory and/or radar data printed out. The differences will be out-putted for each radar site and for each perturbed trajectory when NTRAJ > 4 in a manner basically

similar to the printout of the radar parameters discussed previously. The differences represent the values obtained by subtracting the radar parameters for the perturbed trajectories from the corresponding parameters for the nominal trajectory (trajectory #1 or #3).

Radar data required for the computations must be stored on the plot file and is identical to the data that is placed on the file for producing plots. Normally, this data would be stored on the file as the result of the execution of the parts of the program preceding the parameter difference portion. This data could also be stored from a prior execution of the program and used in the difference computations. However, this latter procedure is not recommended since all program inputs required by the computations should be identical to the corresponding ones that were used when the plot file was created. When IOUT3 = true, therefore, IPLOT1 or IPLOT2 should be set = true and NSWTCH = 1 or 2. It should be pointed out that the input variable KZ will determine which trajectory will be the nominal trajectory for the computations. With KZ = true, the nominal trajectory would be the first trajectory; with KZ = false, it will be the third trajectory.

The following list defines the output parameters when IOUT2 = false.

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
NTRJ	None	Trajectory number.
ISITE	None	Radar site number.
SC1	Deg.	Position in latitude of the radar site.
SC2	Deg.	Position in longitude of the radar site.
Time	Min.	Time from burnout or from initiation of the trajectory of the target (or missile/satellite). Each time printed out will be a time at which both the nominal trajectory and the current perturbed trajectory were detected by the current site.
Slant Range	N.M.	Difference in radar slant (nominal trajectory slant range - perturbed trajectory slant range) for time.

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
Sl Range Rate	Ft. /Sec.	Difference in radar slant range rate.
Elevation	Deg.	Difference in the radar elevation look-angles to the trajectories (nominal-perturbed) or targets.
Elevation Rate	Deg. /Sec.	Difference in radar elevation angle rate.
Azimuth	Deg.	Difference in radar azimuth angle, measured clockwise from north.
Azimuth Rate	Deg. /Sec.	Difference in radar azimuth angle rate.

If IOUT2 = true, the following list of output parameters is produced.

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
NTRJ		Described in the previous list.
ISITE		
SC1		
SC2		
Time		
Slant Range		
Sl Range Rate		
Elevation		
Elevation Rate		
Azimuth		
Azimuth Rate		
Sl Range Rate Dot	Ft. /Sec. <sup>2</sup>	Difference in radar slant range acceleration.
Elevation Rate Dot	Deg. /Sec. <sup>2</sup>	Difference in radar elevation angle acceleration.
Azimuth Rate Dot	Deg. /Sec. <sup>2</sup>	Difference in radar azimuth angle acceleration.
Angular Separation in Radar Beam	Deg.	Total angular separation in the radar beam.

### Plot File

The previous paragraphs under Output have dealt with the printout on listing paper from a program execution. The following paragraphs will describe the plot file which can be created on disc or tape if the user exercises the appropriate input options. By setting either IPLOT1 or IPLOT2 = .TRUE. (when NSWTCH = 1, 2) data will be placed on the file so that off-line plots of radar parameters (range, azimuth, elevation, etc.) can be produced. The plots can be drawn, from data cards punched out from the file, on the Hewlett-Packard 9820A calculator/plotter through the use of the Generalized Data Entry and Plot Program. See Volume II for a detailed description of this program. The Plot Program XYNETICS Plotter, developed for the first modified version of the trajectory program, can handle the case of one trajectory and one radar site, only. The format of the file for each generated trajectory which is subject to a radar search and detected by the radar is given below. Logical records nos. 1 through 7, ..., n contain the data for one sighting of the trajectory (or target) by a radar site. They will be repeated for each additional sighting by the site; they will also be repeated for each sighting of the trajectory by each additional radar site, if multiple sites are to be processed. Refer to Figure III-1 which illustrates the layout of the file.

#### Logical Record No. 1

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
TIME3	Min.	Initial time of sighting missile trajectory at the radar site.
IPLOT2	T	Plotting option 2. Plots for 13 different radar trajectory parameters can be produced. A total of 12 plots can be drawn.
	F	Plots for 8 radar trajectory parameters can be produced. A total of 7 plots can be drawn.
IO2	None	Number of radar parameters which can be plotted. IO2=8 if IPLOT2 if false, 13 for IPLOT2 true.

Radar Site 1, 1st Sighting:

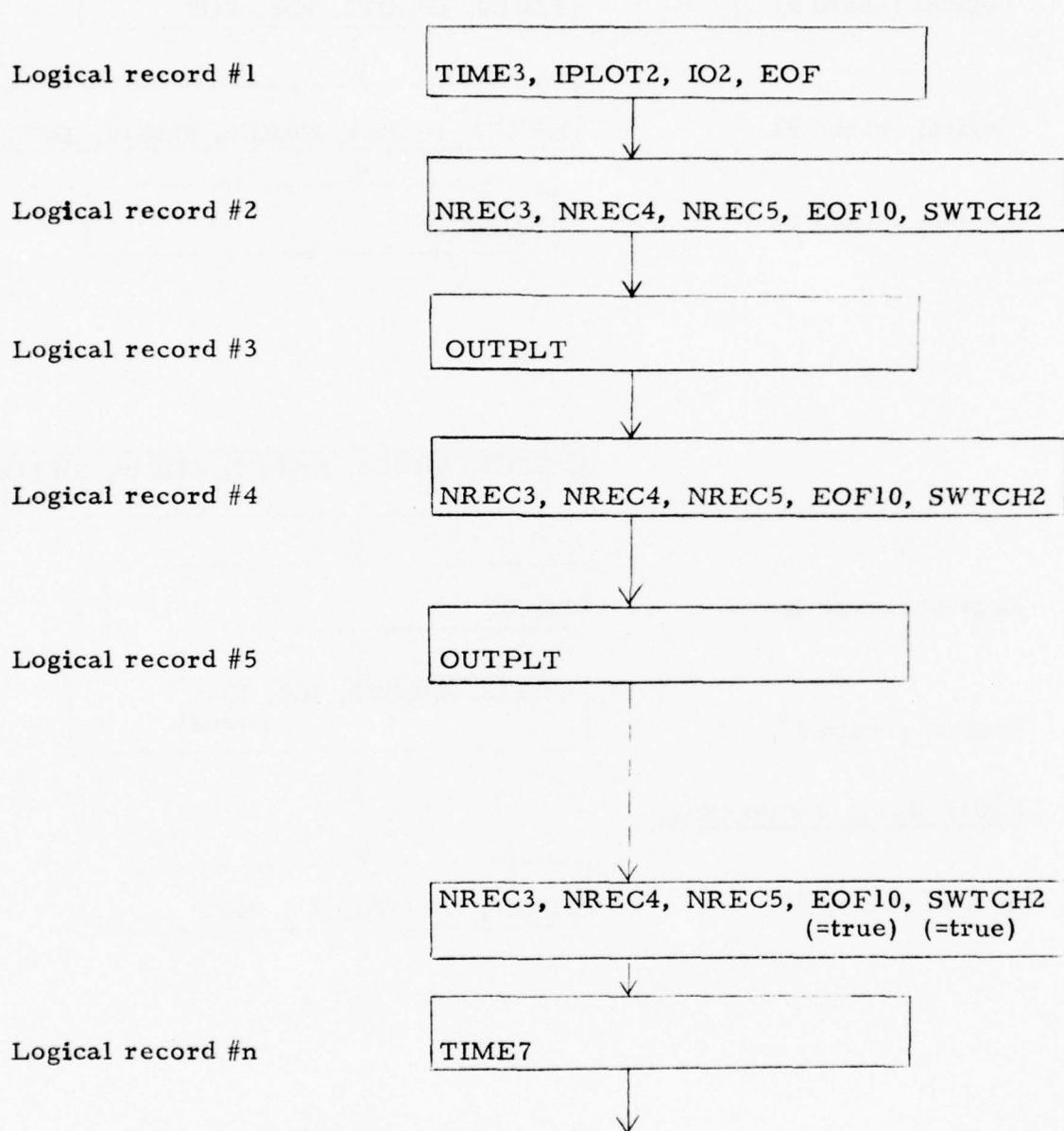


Figure III-1. Plot File Format for Each Trajectory. (1 of 2)

Radar Site 1, 2nd Sighting:

Logical record #1

TIME3, IPLOT2, IO2, EOF

Logical record #2

NREC3, NREC4, NREC5, EOF10, SWTCH2

Logical record #3

OUTPLT

Logical record #n

TIME7

Logical record #1

TIME3, IPLOT2, IO2, EOF  
(=true)

Radar Site 2, 1st Sighting:

Logical record #1

TIME3, IPLOT2, IO2, EOF

Last record on file

TIME3, IPLOT2, IO2, EOF  
(=true)

Figure III-1. Plot File Format for Each Trajectory (2 of 2)

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
EOF		Switch variable to denote the end of data for the current radar site and the current trajectory.
	T	There is no more data on the file for the current site and trajectory.
	F	Radar data follows for the current site and trajectory.

Note that the description of IPLOT2 above is somewhat different from that given under Inputs. The description above is given mainly from the standpoint of a plot program.

Logical Record No. 2, 4, 6, ---

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
NREC3	None	Number of time points in the radar trajectory data on the following record.
NREC4	None	Total number of time points in the following record of radar data and all previously input records of data for the current sighting of the missile trajectory by the radar.
NREC5	None	Number of the following record of radar data for the current sighting.
EOF10		Switch variable to signal the end of the set of data for the current missile sighting.
	T	No more radar data follows for the current sighting.
	F	More data follows for the current sighting.
SWTCH2		Switch variable for plot program to read last time missile is visible to the radar for the current sighting.
	T	Read in this last time from the file.
	F	Do not read in this last time from the file.

Note: In the current version of the program, NREC4 and NREC5 are not used, and the last time of missile visibility to the radar is not written on the plot file. This means SWTCH2 will always be false, and when EOF10 is true, logical record no. 2, 4, 6, --- will be the last record on the file for one sighting of the missile by the radar. The very last record on the file will be logical record no. 1 with EOF true following data for the last trajectory and final sighting by the last radar site.

Logical record no. 3, 5, 7, ---

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
OUTPLT		Output array for outputting the data on this record. There are NREC3*IO2 data words on this record. The contents of OUTPLT are:
OUTPLT(1)	N.M.	Radar slant range for 1st timepoint of this record.
OUTPLT(2)	Ft. /Sec.	Radar slant range rate for 1st timepoint.
OUTPLT(3)	Deg.	Radar elevation angle.
OUTPLT(4)	Deg/Sec.	Radar elevation angle rate.
OUTPLT(5)	Deg.	Radar azimuth angle.
OUTPLT(6)	Deg/Sec.	Radar azimuth angle rate.
OUTPLT(7)	eru	Trajectory radius in eru.
OUTPLT(8)	Deg.	Trajectory inertial phi angle.

If IPLOT2 = .TRUE., the following parameters will also be on this logical record:

OUTPLT(9)	Ft. /Sec. <sup>2</sup>	Slant range acceleration.
OUTPLT(10)	Deg. /Sec. <sup>2</sup>	Elevation angle acceleration.
OUTPLT(11)	Deg. /Sec. <sup>2</sup>	Azimuth angle acceleration.
OUTPLT(12)	Deg.	Missile reentry angle.
OUTPLT(13)	Deg.	Missile heading angle.

Note: If IPLOT2 is false, there are only 8 different radar trajectory parameters on this record for each time point; if IPLOT2 is true there will be 13. Each parameter will be repeated every IO2+1 word of OUTPLT; e.g., OUTPLT (IO2+1) contains the slant range for the 2nd time point of the record, OUTPLT (IO2+2) contains the range rate for the 2nd time point, etc. Any pair of consecutive time points for any records containing radar parameter data are separated by the same increment in time. That is, the time increment between consecutive time points has been set at 0.1 min. for all radar data on the plot file.

If SWITCH2 is true (not currently allowed), the following record will be written on the file. It will be the last record on the file for one sighting of the missile by the radar site and is used mainly in the computation of radar parameter differences.

Logical record no. n

<u>Symbol Name</u>	<u>Units</u>	<u>Description</u>
TIME7	Min.	Last time of sighting (or detection) by the radar site for the current missile sighting.

#### 5. Main Logic Flow

Figure III-2 is a flow chart of the main logic of the program. It is basically a flow chart for the executive (main program) of the program.

#### 6. Sample Job Stream

The sample job stream following Figure III-2 illustrates the program setup for a 1 radar site and 8 trajectory run. The nominal trajectory for the perturbations was chosen as the 1st trajectory. The job stream is setup to place radar data on the plot file so that plots may be produced later if so desired. In the job stream, file 09 stores trajectory data and file 10 stores the radar data to be plotted. The sample output and sample plots included in this document were produced by executing this sample job stream. The output and plots herein included are for the first 3 trajectories only. Note that the second trajectory is labeled number 4. Also, the input data of the job stream causes circular orbit trajectories to be generated.

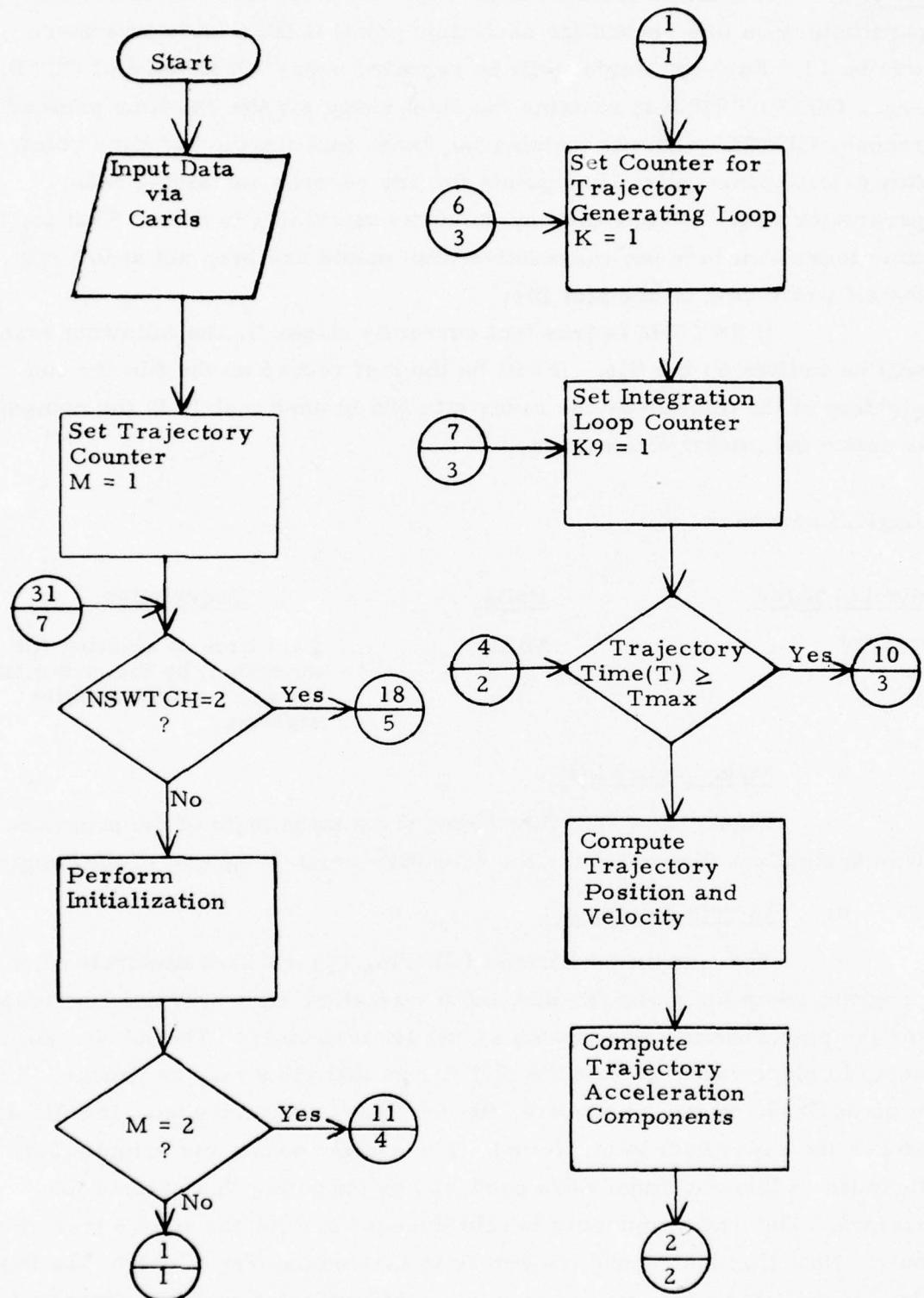


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (1 of 9)

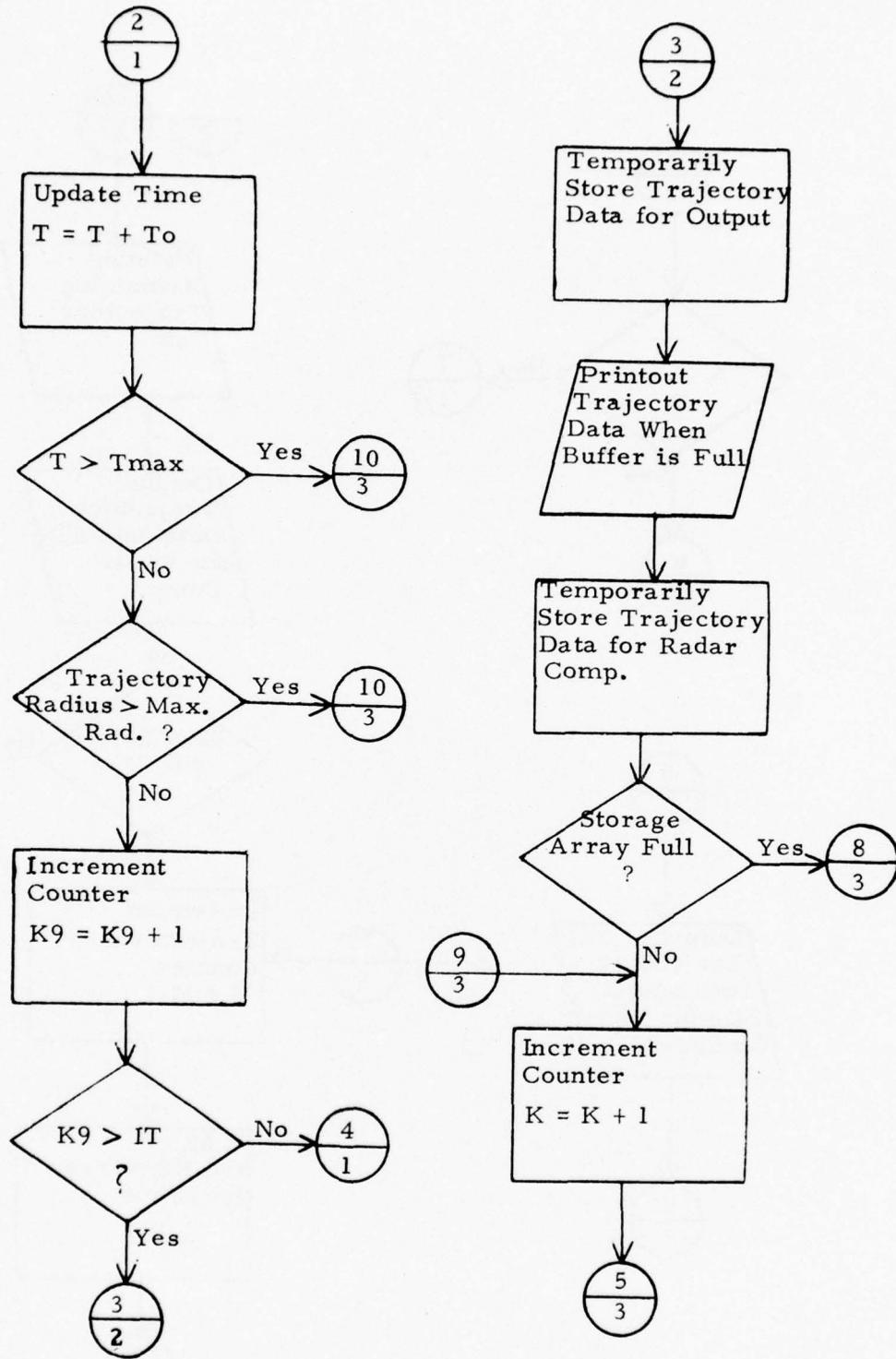


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (2 of 9)

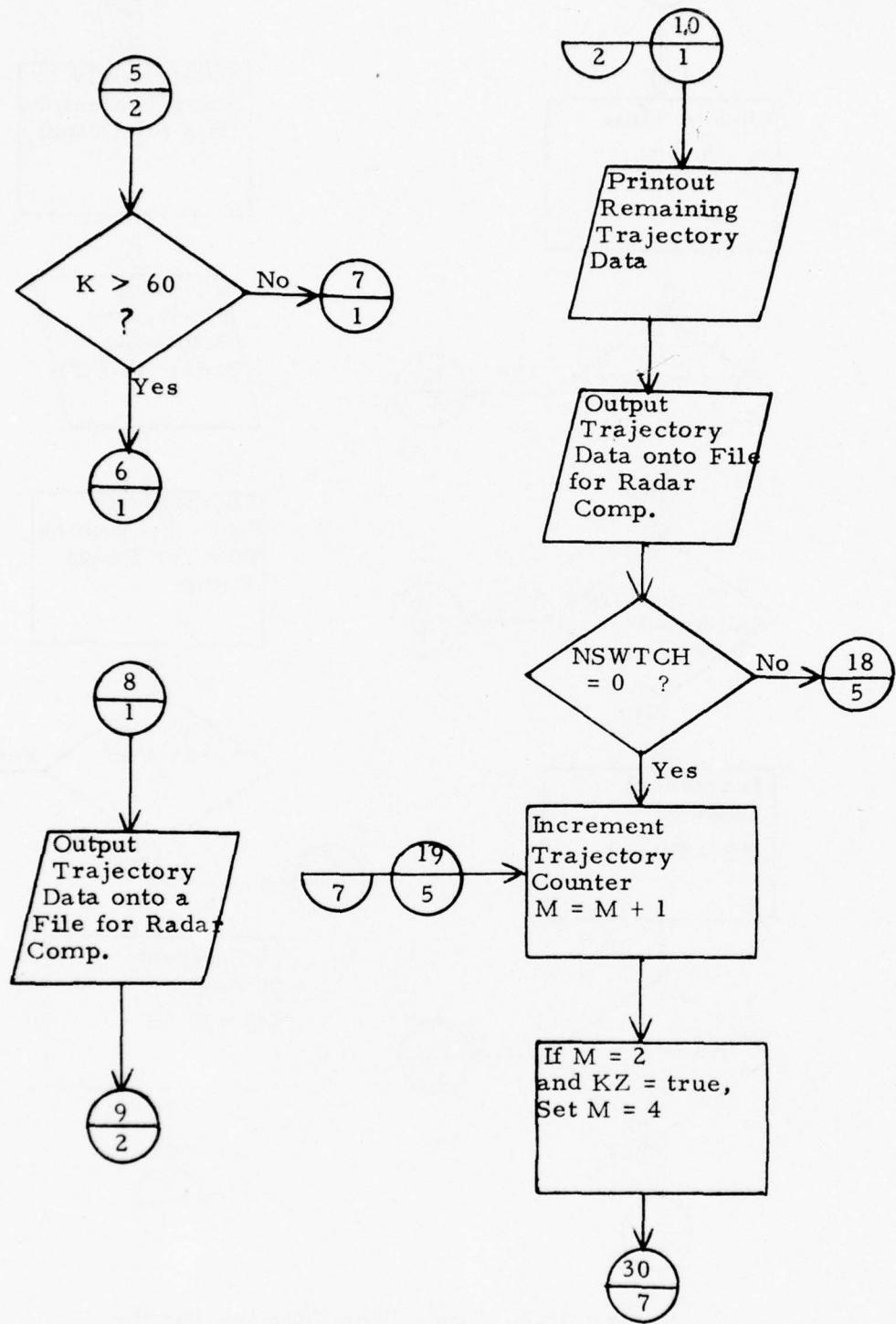


Figure III-2. Logic Flow Diagram for the  
RADC Trajectory Program (3 of 9)

$M = 2$  Trajectory

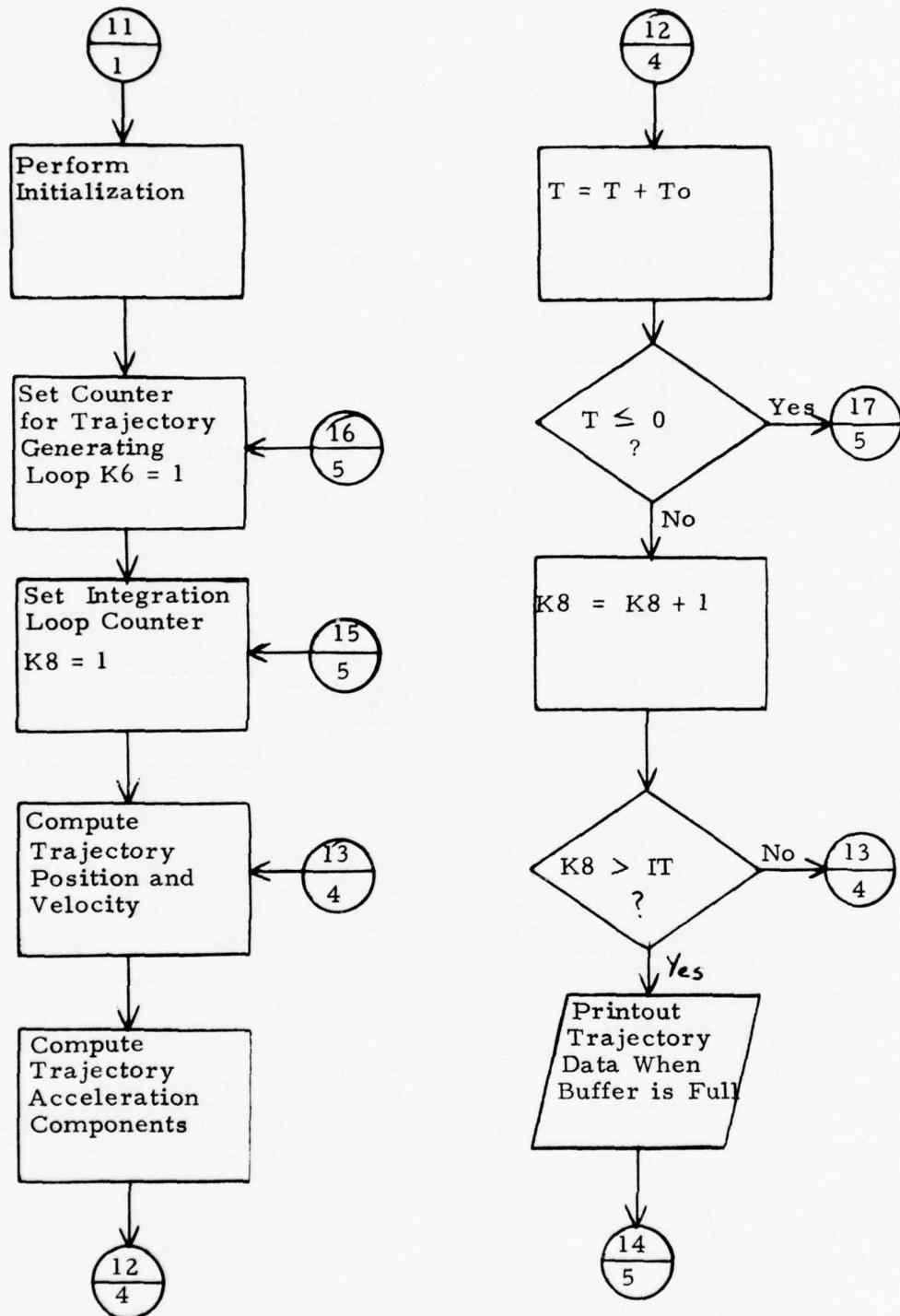


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (4 of 9)

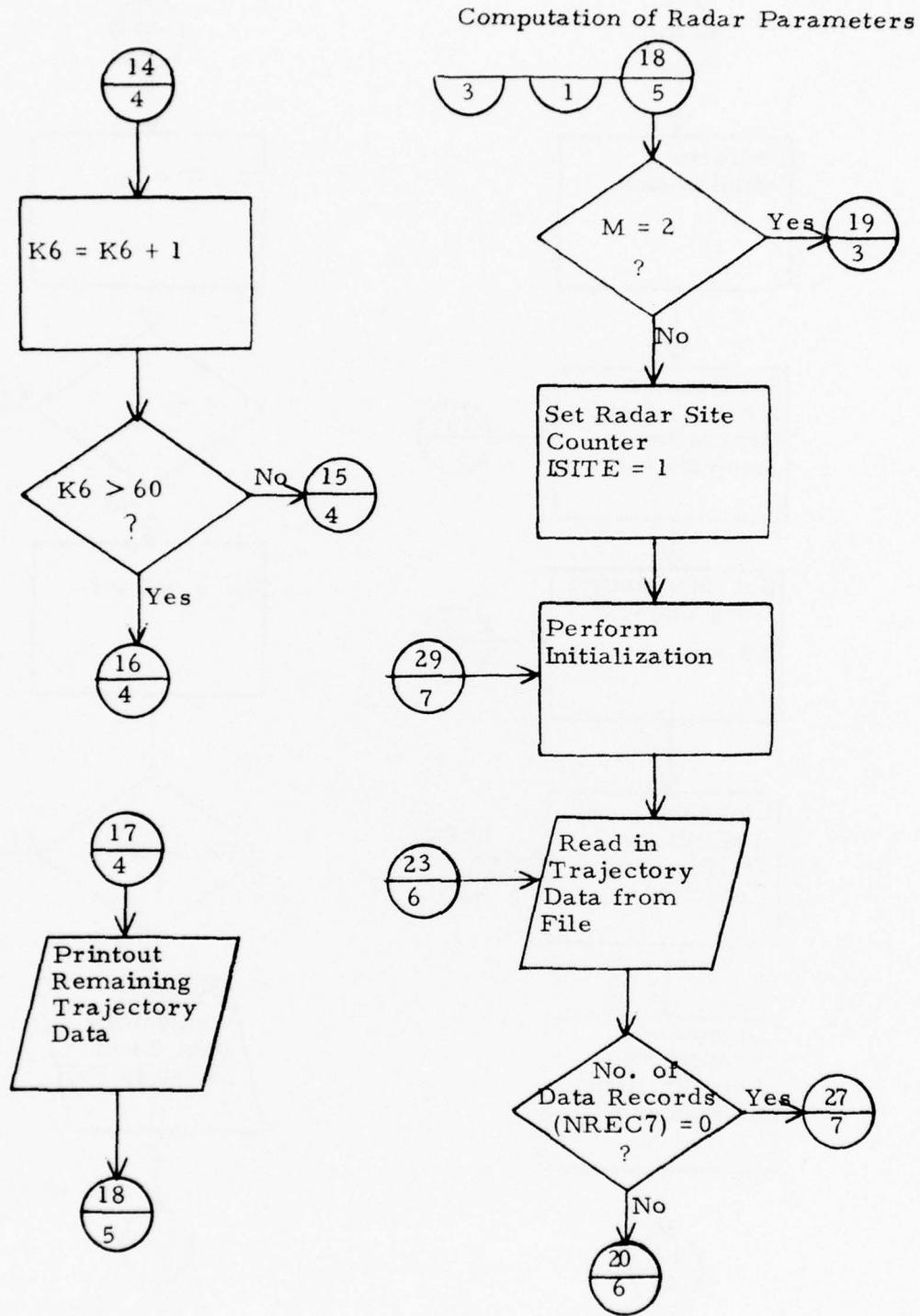


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (5 of 9)

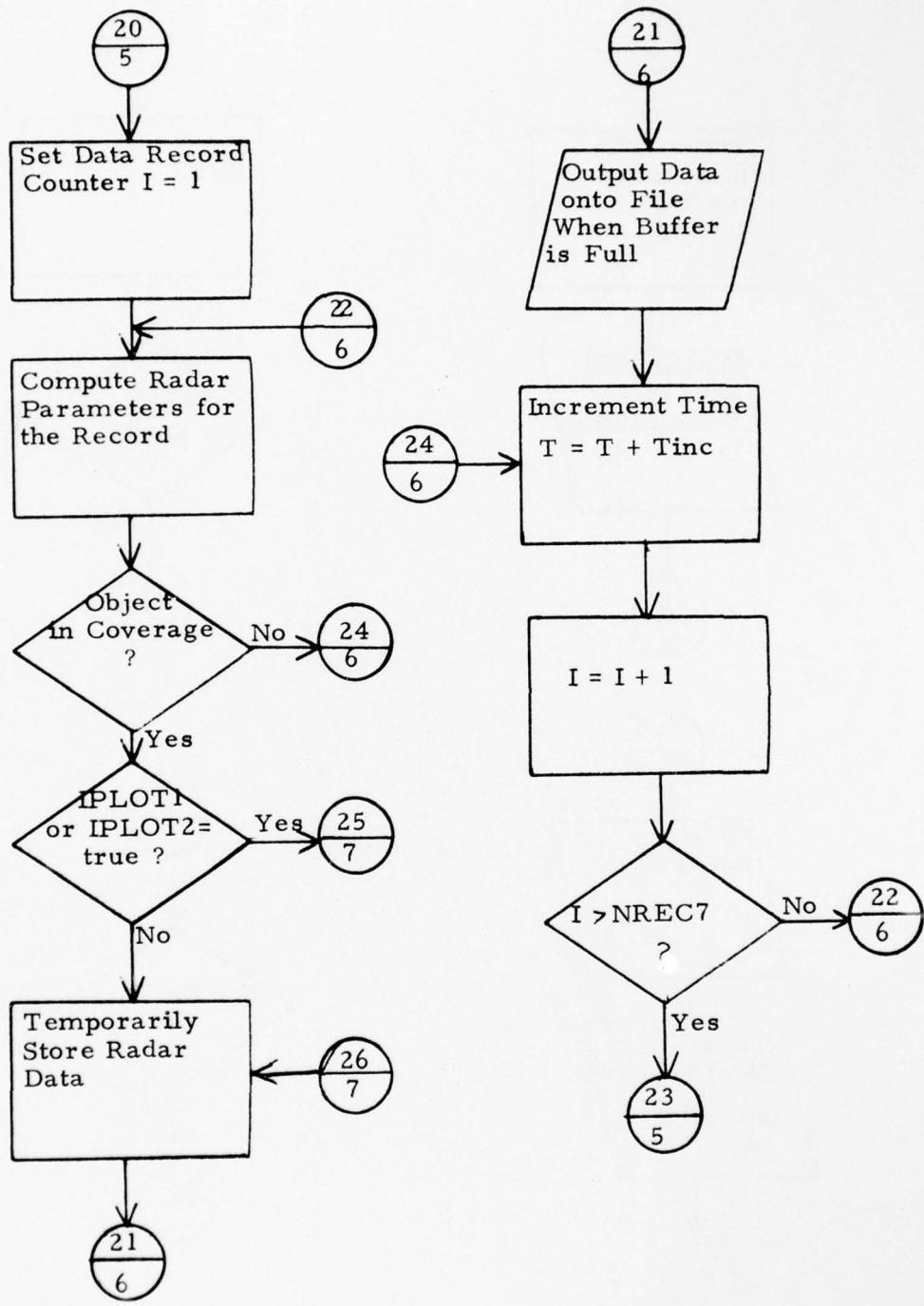


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (6 of 9)

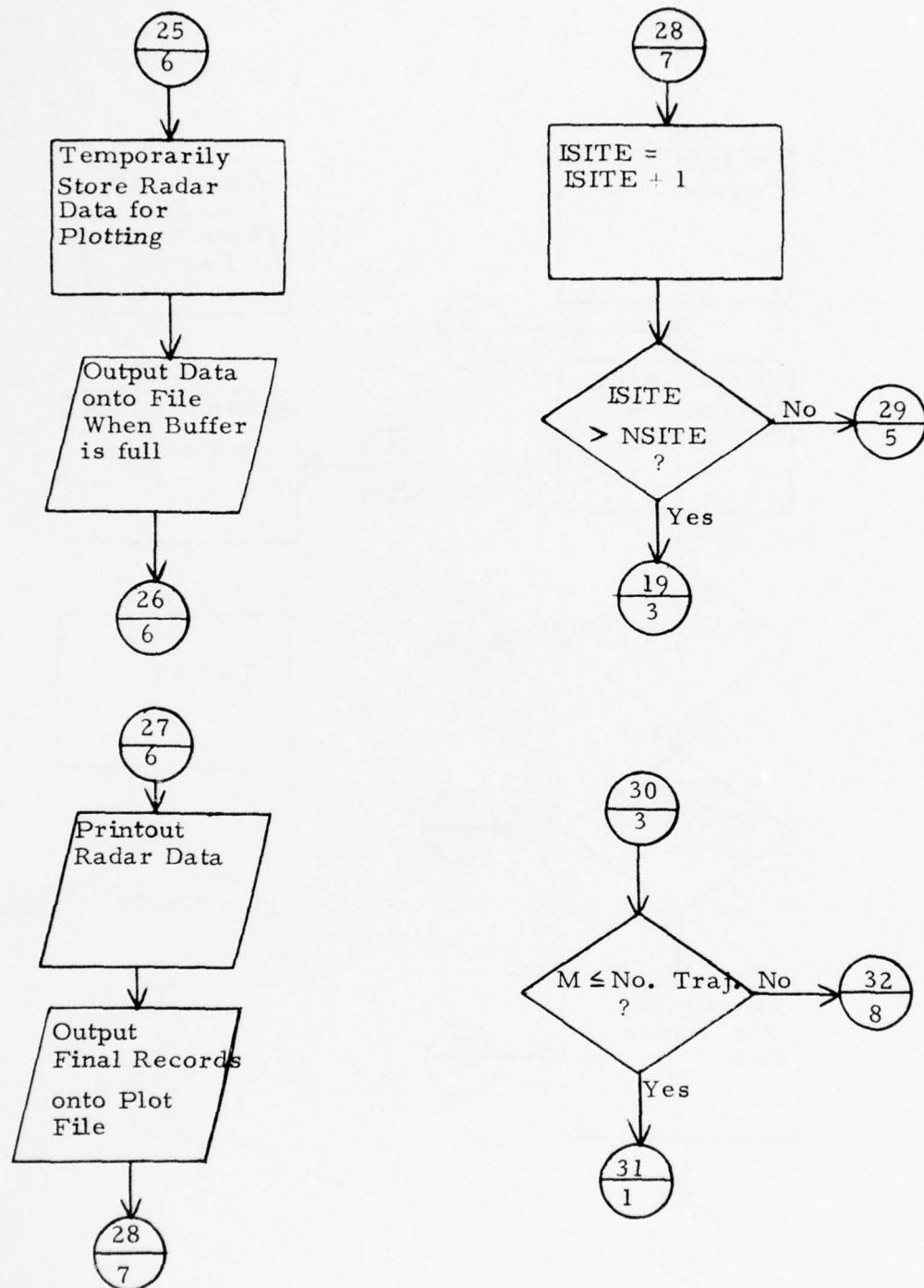


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (7 of 9)

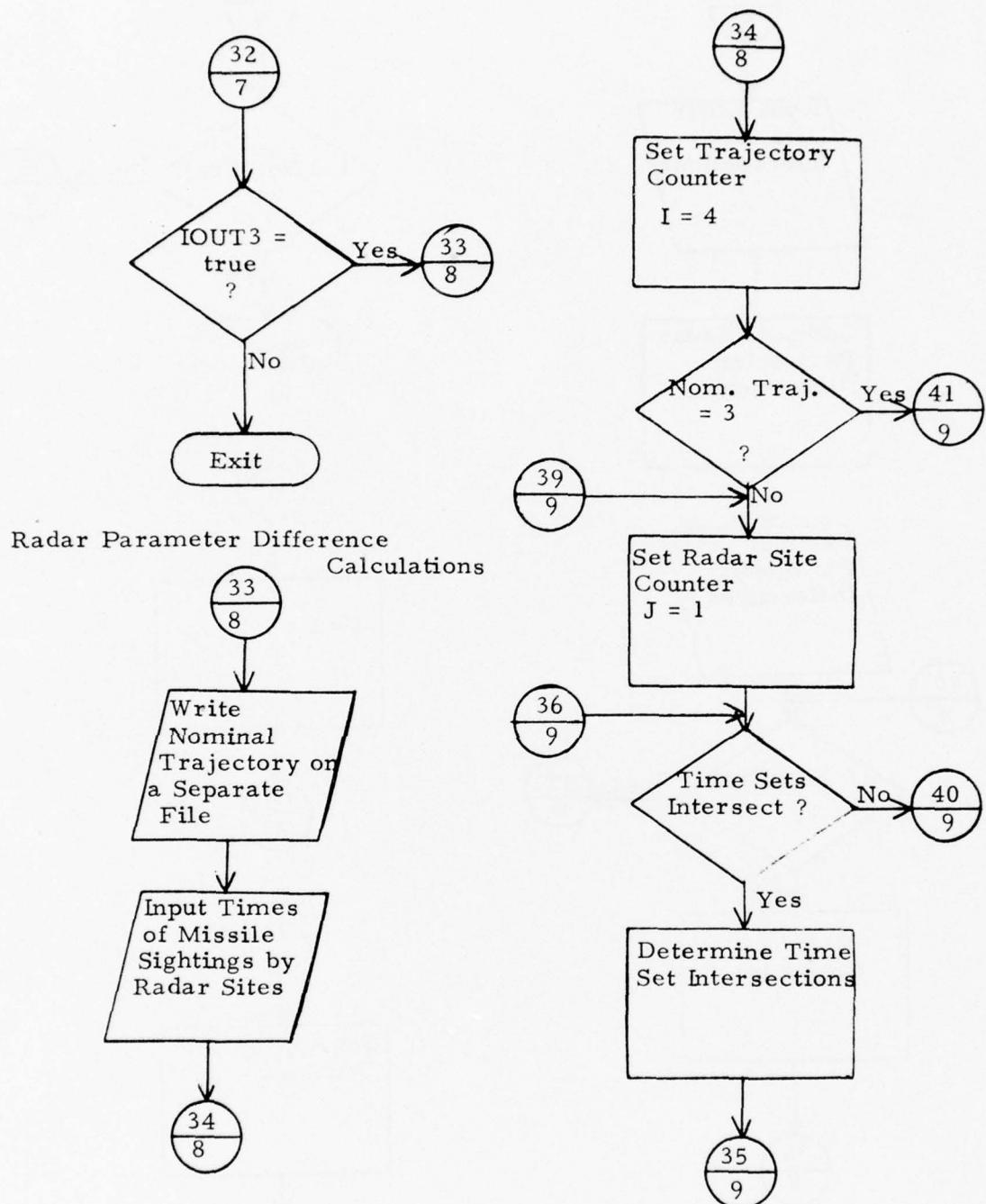


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (8 of 9)

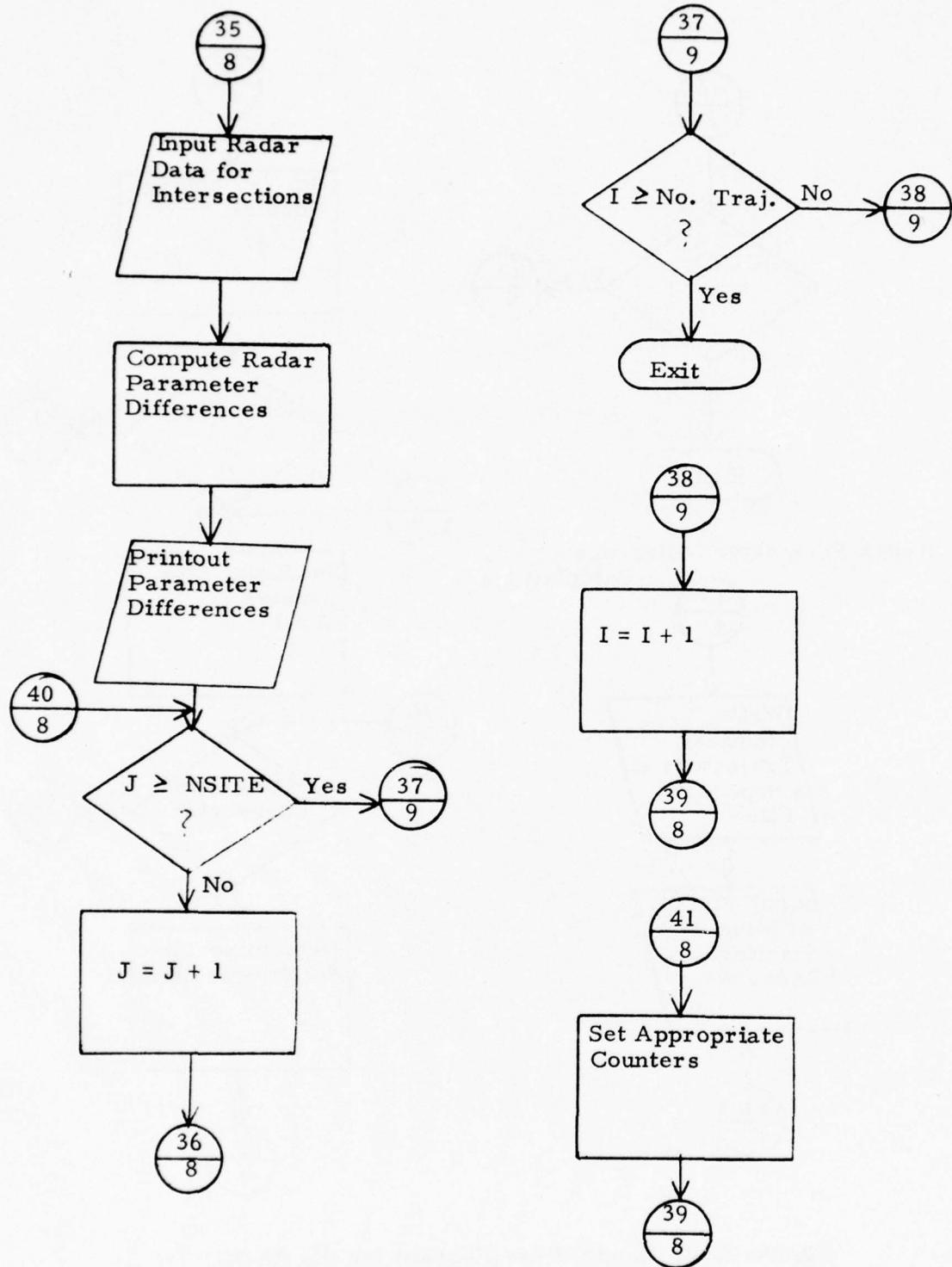


Figure III-2. Logic Flow Diagram for the RADC Trajectory Program (9 of 9)

```

10$:IDENT:CLEARY,CONTI      ,65121104RADC,DSSR
20$:USERID:CLEARYSTHREE
30$:OPTION:FORTRAN
40$:SELECT:CLEARY/ZOMISSATC
50$:SELECT:CLEARY/ZOSIPC
60$:SELECT:CLEARY/ZDOUTUTC
70$:SELECT:CLEARY/ZINTRAJIC
75$:SELECT:CLEARY/ZATMOSC
77$:SELECT:CLEARY/ZEOFTRXC
80$:EXECUTE
90$:LIMITS:40,40K,,12000
100$:DISC:08,01P,10L
110$:PRMFEL:09,R/V,L,CLEARY/ZSTOR4
115$:PRMFEL:10,R/V,L,CLEARY/ZSTOR8
120$:DATA:05
130 $INPUT1 NTRAJ=10, TM=90.0DC, NSITCH=1 $
140 $INPUT2 IOUT1=F, IOUT2=F, IOUT3=F, OUTINC=0.1, KAT=F, KZ=1,
150 SPHERE=T, IPLOT1=T, IPLOT2=F, INFTL=T $
160 $INPUT3 GAM=90.0DD, PETA=31.82638DD, V0=2.556742D4,
170 HX=6.98098D5, THE=62.7D0, GLAM=42.35D0, THES=-40.0D0, GLAM2=64.0DD $
180 $INPUT4 NSITE=1,
190 SLAT(1)=35.0DD, SLONG(1)=933.333DD, SALT(1)=6.0DD, FLIM=89.0DD $
200 $INPUT5 A(1)=4*0.0DD, 5.0DD, 2*3.533DD,
210 B(1)=0.0DD, 5.0DD, 3.533DD, -3.533DD, 0.0DD, 3.533DD, -3.533DD,
220 C(1)=5.0DD, 0.0DD, 2*3.533DD, 3*0.0DD $
225:ENDJOB
226***EOF

```

Sample Job Stream for the RADC Trajectory Program

## HIS 6000 Batch Submittal Form

**Source Listing of the RADC Trajectory Program**

CMISSAT MISSILE/SATELLITE TRAJECTORY PROGRAM  
 C INPUT/OUTPUT MOD 2, MULTIPLE SITE/TRAJECTORY VERSION

---

C THIS IS A GENERAL PERTURBATION PROGRAM THAT PREDICTS THE POSITION, 00000010  
 C VELOCITY AND ACCELERATION OF A VEHICLE WHETHER AS AN EARTH 00000020  
 C ORBITING SATELLITE OR BALLISTIC MISSILE. THE FORMULATION IS BASED 00000030  
 C UPON THE NUMERICAL INTEGRATION OF THE SPHERICAL FORM OF THE EARTH. 00000040  
 C THE 1959 ARDC ATMOSPHERIC MODEL AND 00000050  
 C THE EARTH WIND ARE INCLUDED. 00000060  
 C

---

C THIS ROUTINE DRIVES THE PROGRAM. 00000120  
 C THE MAIN SUBROUTINE GROUPINGS CALLED ARE 00000130  
 C 1. EQTNX - COMPUTES ACCELERATION COMPONENTS 00000140  
 C 2. CONVER - COMPUTES SENSOR PARAMETERS 00000150  
 C 3. RKG - USING A 4TH ORDER RUNGE KUTTA-GILL, NUMERICALLY 00000160  
 C INTEGRATES THE EQUATIONS OF MOTION 00000170  
 C

---

C ALL DATA ASSOCIATED WITH THE MATHEMATICAL MODEL OF THE EARTH ARE 00000180  
 C FROM MAKEMSON, B., BAKER, R.L.M., AND WESTRON, G.B., ANALYSIS AND 00000190  
 C STANDARDIZATION OF ASTRODYNAMIC CONSTANTS. 00000200  
 C

---

DOUBLE PRECISION X, XD, XDD, ITO, TM 00000210  
 DOUBLE PRECISION TC, TI, XK, TX 00000220  
 \*, T, H, XYZ, RSL, PZ, R, W 00000230  
 DOUBLE PRECISION TN, STN 00000240  
 DOUBLE PRECISION P1, ZK, B1, GEO 00000250  
 DOUBLE PRECISION GAM, BETA, HX, VO, THE, GLAM, SC1, SC2, AH, THES, GLAMS 00000260  
 \*, E, ELIM, SLAT, SLONG, SALT 00000270  
 COMMON/E/E/ELIM/ELIM/IJJJ/INOM,I,J,JSIGHT,TSTART,TEND 00000280  
 COMMON/MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS 00000290  
 COMMON/TS/T,H,XYZ,RSL,PZ 00000300  
 \*7A/R,W/JX/JX/TIME2/TIME2 00000310  
 COMMON/BS/X(3), XD(3), XDD(3) 00000320  
 \*7GEOXK/GEO,XK 00000330  
 \*7SWSW/SWTC1,SWTC2/SW10/SWCH10 00000340  
 \*7SW3SW4/SWTC1,SWTC4 00000350  
 \*7SW5SW6/SWTC5,SWTC6 00000360  
 \*7SW7/SWTC7/SW8/SWTC8/SW9/SWTC9/NSWTC/NSWTC 00000370  
 \*7TIMES5/TIMES5 00000380  
 \*7TSIGHT/TIMESI(10,10,5),TIMESY(10,10,5),NSIGHT(10,10) 00000390  
 \*7OPTION/IOUT1,IOUT2,KZ,IPILOT1,IPILOT2,KAT,SPHERE,OUTINC,IOUT3 00000400  
 \*7OUTRJ/OUTTRJ(5000),OUTRAD(5000),OUTPLT(5000) 00000410  
 \*7NTRAJ/ITM 00000420  
 COMMON/GE/ZK,B1,P1 00000430  
 COMMON/AX/TM,M 00000440  
 COMMON/INOUT/INOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA 00000450  
 \*7TO/TO/IT2/IT2,IT 00000460  
 COMMON/NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC 00000470  
 \*7IO/IO,IO1,IO2 00000480  
 COMMON/NR7/NREC7,NOFF4 00000490  
 \*7ISITE/ISITE/SITES/NSITE,SLAT(20),SLONG(20),SALT(20) 00000500  
 00000510  
 00000520  
 00000530

LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE	00000540
* ,IOUT3,SWTCH1,SWTCH2,SWTCH10	00000550
LOGICAL SWTCH3,SWTCH4	00000560
LOGICAL SWTCH5,SWTCH6	00000570
* ,SWTCH7,SWTCH8,SWTCH9	00000580
 C INPUT DATA	00000600
CALL INPUT	00000610
M=1	00000620
 C SET INTEGRATION STEP SIZE AND NUMBER OF INTEGRATION STEPS	00000630
260 T0=0.1D-1	00000640
IT=10	00000650
TINC=T0*IT	00000660
IF(NSWTCH.EQ.2)GO TO 250	00000670
 C INITIALIZATION	00000680
CALL INITAL	00000690
 C INITIALIZE MISSILE/SATELLITE TRAJECTORY	00000700
CALL ICERBM	00000710
IF(M.EQ.2)GO TO 15	00000720
CALL EQTNX	00000730
105 CALL OUTPUT	00000740
IF(M.EQ.2)GO TO 6	00000750
CALL STORTR	00000760
 C MAIN PROCESSING LOOP FOR TRAJECTORY GENERATION	00000770
20 DO 16 K=1,60	00000780
 C INTEGRATION LOOP	00000790
DO 1 K9=1,IT	00000800
IF(T.GE.TM-1,D-5)GO TO 21	00000810
 C PERFORM RUNGE-KUTTA INTEGRATION	00000820
CALL RKG	00000830
 C COMPUTE ACCELERATION COMPONENTS	00000840
CALL EQTNX	00000850
T=T+TO	00000860
IF(T.GT.(TM+1.0D-5).OR.,V(1),GT,GEO)GO TO 21	00000870
CONTINUE	00000880
IOUT = IOUT + IT	00000890

C	STORE TRAJECTORY DATA FOR OUTPUT	00001100
	IF(IOUT.GE.INCOUT)CALL STORTJ	00001110
C	PRINT OUT TRAJECTORY DATA	00001120
	IF(NREC1.GE.NOFF1)CALL PRINTT	00001130
		00001140
		00001150
		00001160
		00001170
		00001180
		00001190
C	STORE TRAJECTORY DATA FOR RADAR COMPUTATIONS	00001200
	CALL STORTR	00001210
	IF(NREC7.GE.NOFF4)GO TO 150	00001220
	GO TO 16	00001230
		00001240
		00001250
C	OUTPUT TRAJECTORY DATA ON A FILE	00001260
	150 IF(SWTC9)CALL OUTTRI	00001270
	SWTC9=.FALSE.	00001280
	CALL OUTTR	00001290
16	CONTINUE	00001300
	GO TO 20	00001310
21	IF(X(1).GT.GEQ)GO TO 2	00001320
	SWTC3=.TRUE.	00001325
2	CONTINUE	00001330
		00001340
		00001350
C	PRINT OUT TRAJECTORY DATA	00001360
	CALL PRINTT	00001370
C	OUTPUT TRAJECTORY DATA ON A FILE	00001380
	IF(SWTC9)CALL OUTTRI	00001390
	IF(NREC7.NE.0)CALL OUTTR	00001400
	CALL OUTTR	00001410
	IF(ITM.GE.2)CALL STORT2	00001415
	IF(NSWTC9.EQ.1)GO TO 17	00001420
	GO TO 250	00001430
60	CONTINUE	00001431
C	M = 2 TRAJECTORY	00001432
C	SET INTEGRATION STEP SIZE AND NUMBER OF STEPS	00001435
C	TO=-0.01DC	00001440
	IT=10	00001450
	IF(SWCH10)IT=IT2	00001460
	DO 41 K8=1,IT	00001470
	CALL RKG	00001480
	CALL EQTNX	00001490
	T=T+TO	00001500
		00001510
		00001520
		00001530
		00001540
		00001550
		00001560

```

        IF(T.LE.1.0D-5)GO TO 86          00001570
41 CONTINUE          00001580
        TIME2=T          00001585
        CALL STORTJ      00001590
        IF(SWCH10)IT=10      00001600
C     MAIN PROCESSING LOOP,M=2 TRAJECTORY      00001610
C
70 DO 18 K6=1,60          00001620
    DO 40 K8=1,IT          00001630
    CALL RKG          00001640
    CALL EQTNX          00001650
    T=T+TO          00001660
    IF(T.LE.1.,D-5)GO TO 86          00001670
40 CONTINUE          00001680
    IOUT=IOUT+IT          00001690
    IF(IOUT.GE.INCOUT)CALL STORTJ      00001700
    IF(NREC1.GE.NOFF1)CALL PRINTT      00001710
18 CONTINUE          00001720
    GO TO 70          00001730
86 SWTCH3=.TRUE.          00001740
    CALL PRINTT          00001750
C     COMPUTE RADAR PARAMETERS          00001760
C
250 IF(M.EQ.2)GO TO 17          00001770
    DO 500 ISITE=1,NSITE          00001780
    CALL INITAL          00001790
C     INPUT TRAJECTORY DATA          00001800
C
    CALL INTRAJ          00001810
100 CALL TRAJIN          00001820
    IF(NREC7.EQ.0)GO TO 200          00001830
    JX=1          00001840
    DO 300 I=1,NREC7          00001850
    CALL TRAJX          00001860
    CALL CONVER          00001870
    SWTCH5=.TRUE.          00001880
    IF(E.GT.ELEM)GO TO 120          00001890
    SWTCH5=.FALSE.          00001900
    SWTCH6=.FALSE.          00001910
    IOUTA=IOUTA+IT          00001920
    IF(SWTCH1)GO TO 115          00001930
    IF(SWTCH4)CALL STRAD2          00001940
130 IF(IPLOT1.OR.IPLOT2)GO TO 135          00001950
C     STORE RADAR DATA FOR OUTPUT          00001960
C
110 IF(SWTCH4)GO TO 120          00001970
    IF(IOUTA.GE.INCOUT)CALL STORD1      00001980
    IF(NREC2.GE.NOFF2)CALL OUTRDR      00001990

```

C	120 IF(SWTCHE)GO TO 125	00002310
	IF(.NOT.SWTCH1,AUD,SWTCHE)GO TO 140	00002320
	GO TO 125	00002330
C	STORE,OUTPUT DATA FOR LAST VISIBLE POINT	00002340
C		00002350
C	140 SWTCHE,TRUE.	00002360
	CALL STRADL	00002370
	IF(NREC2,NE,.)CALL OUTRDR	00002380
	CALL OUTEOF	00002390
C	RE-INITIALIZE SWITCHES	00002400
C	SWTCH1=.TRUE.	00002410
	SWTCH4=.TRUE.	00002420
	IF(IPLOT1.OR.IPLOT2)GO TO 145	00002430
	GO TO 125	00002440
C	OUTPUT DATA ON PLOT FILE UP TO LAST VISIBLE POINT	00002450
C		00002460
C	145 SWTCH2=.TRUE.	00002470
	IF(NREC3,NE,.)CALL PLTAP1	00002480
	CALL PLTAP2	00002490
	GO TO 125	00002500
C	135 IF(SWTCH2)CALL PLTAPE	00002510
	SWTCH2=.FALSE.	00002520
	SWTCH7=.FALSE.	00002530
C	STORE RADAR DATA FOR PLOTTING	00002540
C		00002550
C	CALL STORTP	00002560
C	OUTPUT DATA ON PLOT TAPE/FILE	00002570
C		00002580
C	IF(NREC3.GE.NOFF3)CALL PLTAP1	00002590
	GO TO 110	00002600
C	115 SWTCH1=.FALSE.	00002610
	SWTCH8=.FALSE.	00002620
	CALL STORAD	00002630
	GO TO 130	00002640
C	125 CONTINUE	00002650
	T=T+TINC	00002660
C	300 CONTINUE	00002670
	GO TO 100	00002680
C	PRINT OUT RADAR DATA	00002690
C		00002700
C	200 CONTINUE	00002710
	IF(NREC7,EQ,.)T=T-TINC	00002720
	IF(.NOT.SWTCHE)GO TO 23	00002730
		00002740
		00002750
		00002760
		00002770
		00002780
		00002790
		00002800
		00002810
		00002820

```

24 IF(NREC2,NE,0)CALL OUTRDR          00002830
    CALL OUTADR                         00002840
    CALL PRINTR                          00002850
    IF(SWTCH8)CALL NOTVIS               00002860
    IF(SWTCH7)GO TO 500                 00002870
C
C     OUTPUT LAST RECORDS ON PLOT TAPE/FILE 00002880
C
C
IF(SWTCH2)GO TO 22                  00002910
IF(NREC3,NE,0)CALL PLTAP1            00002920
    CALL PLTAP2                          00002930
    CALL PLTAP3                          00002940
    GO TO 500                           00002950
22 CONTINUE                         00002960
    CALL PLTAP3                        00002970
    GO TO 500                           00002980
23 IF(T.LT.TIME5+0.01)GO TO 24      00002990
    CALL CONVER                         00003000
    IF(E.GT.ELEM)GO TO 24              00003010
    CALL STRALL                         00003020
    GO TO 24                           00003030
500 CONTINUE                         00003040
    17 M=M+1                           00003045
    IF(M.EQ.2,AND,KZ)M=4               00003046
    IF(M.LE.17)GO TO 25                00003047
    IF(IOUT3)GO TO 10                  00003050
1010 STOP                            00003060
C
C     COMPUTE RADAR PARAMETER DIFFERENCES 00003070
C
C     WRITE NOMINAL TRAJECTORY ON A SEPARATE FILE 00003080
C
1000 CALL OUTNOM                     00003090
C
C     READ AND STORE TIMES OF SIGHTING 00003095
C
C     CALL TIMEST                        00003096
C
C     MAIN PROCESSING LOOP PARAMETER DIFFERENCES 00003100
C
    INOM = 1                           00003106
    I=4                                00003110
    IPASS=1                            00003120
    IF(.NOT.KZ)I=1                      00003130
    IF (.NOT.KZ)INOM=3                  00003135
C
C     LOOP ON SITES                     00003140
C
1060 J=1                            00003150
1040 II=NSIGHT(INOM,J)               00003160
    IF(TIMESI(I,J,1).GT.TIMESF(INOM,J,II))GO TO 1020 00003170
    II=NSIGHT(I,J)                      00003180
                                                00003190
                                                00003200
                                                00003214
                                                00003205
                                                00003216
                                                00003210
                                                00003220
                                                00003230
                                                00003240

```

```

C IF(TIMESI(INOM,J,1),GT,TIMESF(I,J,II))GO TO 1020      00003250
C DETERMINE THE INTERSECTIONS OF TIME SETS                 00003260
C CALL INTER                                                00003270
C INPUT RADAR DATA CORRESPONDING TO TIME SET INTERSECTIONS 00003280
C
C CALL INTDAT                                              00003290
1020 IF(J,GE,NSITE)GO TO 1030                           00003300
J=J+1
GO TO 1040
1030 IF(I,GE,ITM)STOP
IF(INOM,EQ,1)GO TO 1050
IF(IPASS,NE,1)GO TO 1050
IPASS=2
I=3
1050 I=I+1
GO TO 1060
END
***EOF

```

-76 17.491

ATMOSPHERIC MODEL

LAB

```
1      CATMOSP      ATMOSPHERIC MODEL
2      SUBROUTINE ATMOSF
3      C      THIS ROUTINE COMPUTES THE ATMOSPHERIC DENSITY(IN SLUGS PER FEET
4      C      CUBED) FROM THE 1959 ARDC MODEL ATMOSPHERE, ABOVE 105 KILOMETERS
5      C      THE DENSITY IS SET EQUAL TO ZERO. BELOW THIS VALUE, THE LAYERS
6      C      ASSUME AN ISOTHERMAL OR LINEAR TEMPERATURE LAPSE RATE SECTION.
7
8      DOUBLE PRECISION HP,H2P,SK3,HB,PB,SK1,SK2,CD,ST
9      DOUBLE PRECISION P1,ZK,B1
10     DOUBLE PRECISION TS,T,H,V,RSL,PZ,XYZ
11     COMMON/TS/T,H,XYZ,RSL,PZ
12     COMMON/GE/ZK,B1,P1
13     HP=.3148D0*R
14     H2P=HP/(1.0D0+HP/.6356766D7)
15     IF(HP-5.3D4)20,25,25
16     20   IF(HP-4.7D4)21,29,29
17     21   IF(HP-2.5D4)22,30,30
18     22   IF(HP-1.1D4)23,31,31
19     23   IF(HP)28,28,32
20     25   IF(HP-7.9D4)33,33,26
21     26   IF(HP-9.0D4)34,34,27
22     27   IF(HP-1.05D5)35,35,28
23     28   PZ=0.0D0
24     Q1=0.0D0
25     Q2=0.0D0
26     Q3=0.0D0
27     RETURN
28     29   SK3=.120869D-3
29     HB=4.7D4
30     PB=2.8804D-6
31     GO TO 37
32     30   SK1=.138466D-4
33     SK2=1.13883D1
34     PB=7.765D-5
35     HB=2.5D4
36     GO TO 36
37     31   SK3=.157689D-3
38     HB=1.1D4
39     PB=7.62D-4
40     GO TO 37
41     32   SK1=-.225569D-4
42     SK2=-5.25612D0
43     PB=2.37692D-3
44     HB=1.0D0
45     GO TO 36
46     33   SK1=-.159202D-4
47     SK2=-7.59218D0
48     PB=1.39468D-6
49     HB=5.3D4
50     GO TO 36
51     34   SK3=.206234D-3
52     HB=7.9D4
```

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ATMOSPHERIC MODEL

LAB

```
53      PB=4.1189D-8
54      GO TO 37
55      35 SK1=.241458D-4
56      SK2=8.9442D0
57      PH=4.261D-9
58      KB=9.0D4
59      36 CD=1.0D0+SK1*(H2P-HB)
60      ST=(1.0D0+SK2)
61      PZ= PB*(CD**ST)
62      RETURN
63      37 PZ=PB*DEXP(-8K3*(H2P-HB))
64      RETURN
65      END
```

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## BALLISTIC COEFFICIENTS

L

```

1      CBALCOF      BALLISTIC COEFFICIENTS
2      SUBROUTINE BALCOF
3      DOUBLE PRECISION Z1,Z2,Z3,Z4,Z5,B1,ZK
4      DOUBLE PRECISION HB,HB2,HB3,HB4,P1,P2,P3,P4
5      DOUBLE PRECISION XL1,XL2,XL3,XL4,XL5
6      DOUBLE PRECISION GM,TM,X,T,H,XYZ,RSL,PZ
7      DOUBLE PRECISION XD,XDD
8      DOUBLE PRECISION P5,P7,P9,P11,P13,P14,P8
9      COMMON/BS/X(3),XD(3),XDD(3)
10     COMMON/AX/TM,M/TS/T,H,XYZ,RSL,PZ
11     COMMON/GE/ZK,B1,P1
12     DATA GM/1.407639D16/
13     HB = H*1.D-3
14     IF (HB.GE.3.445D2) GO TO 90
15     HB2 = HB*HB
16     HB3 = HB2*HB
17     HB4 = HB2*HB2
18     IF(M.LE.3) GO TO 3
19     IF(M.EQ.4) GO TO 4
20
21     C      ***** M = 3    RV-9-2B    *****
22
23     3      P1 = 0.0D0
24     P2 = 9.0D1
25     P3 = 1.8D2
26     P4 = 2.7D2
27     IF(HB.GE.P4)GO TO 18
28     IF(HB.GE.P3) GO TO 20
29     IF(HB.GE.P2) GO TO 22
30     IF(HB.GE.P1) GO TO 24
31     GO TO 90
32     18    XL1 = .8473D-7
33     XL2 = .3864D-5
34     XL3 = -.4263D-1
35     XL4 = .1417D+2
36     XL5 = -.1124D+4
37     GO TO 2
38     20    XL1 = .2573D-6
39     XL2 = -.4352D-4
40     XL3 = -.4597D-1
41     XL4 = .1253D+2
42     XL5 = -.4204D+3
43     GO TO 2
44     22    XL1 = -.1944D-5
45     XL2 = .7391D-3
46     XL3 = -.1040D0
47     XL4 = .7063D+1
48     XL5 = .1649D3
49     GO TO 2
50     24    XL1 = .1835D-5
51     XL2 = -.2271D-3
52     XL3 = -.5727D-2

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24-76 19.492

## BALLISTIC COEFFICIENTS

L

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53      XL4 = .2765D1
54      XL5 = .2008D3
55      GO TO 2
56
57      C      * * * * H = 4    BOOSTER * * * *
58
59      4      P1 = 5.0D1
60      P2 = 1.40D2
61      P3 = 2.3D2
62      P5 = 3.1D2
63      IF(HB.GT.P5) GO TO 90
64      IF(HB.GE.P4) GO TO 40
65      IF(HB.GE.P2) GO TO 41
66      IF(HB.GE.P1) GO TO 42
67      GO TO 90
68      40      XL1 = .3123D-7
69      XL2 = -.6148D-5
70      XL3 = -.7003D-2
71      XL4 = .2501D2
72      XL5 = -.1995D3
73      GO TO 2
74      41      XL1 = .5097D-6
75      XL2 = -.2590D-3
76      XL3 = .3502D-1
77      XL4 = .6331D-1
78      XL5 = -.1343D3
79      GO TO 2
80      42      XL1 = -.8529D-6
81      XL2 = .4197D-3
82      XL3 = -.7661D-1
83      XL4 = .6386D1
84      XL5 = -.1654D3
85      GO TO 2
86      90      ZK = 0.0D0
87      B1 = 0.0D0
88      GO TO 100
89      2      Z1 = XL1*HB4
90      Z2 = XL2*HB3
91      Z3 = XL3*HB2
92      Z4 = XL4*HB
93      Z5 = XL5
94      B1 = Z1+Z2+Z3+Z4+Z5
95      ZK = GM/(2.0D0*X(1)*X(1)*B1)
96      5      CONTINUE
97      100     RETURN
98      END

```

22-76 15.858 CONVERT TO RADAR COORDINATES LAB

```

1      CCONVER   CONVERT TO RADAR COORDINATES
2      SUBROUTINE CONVER
3      INPUT/OUTPUT MOD 1
4      THIS ROUTINE DETERMINES WHETHER THE SENSOR UNDER CONSIDERATION IS
5      CAPABLE OF OBSERVING THE VEHICLE AT ANY TIME AND OF COMPUTING THE
6      RANGE, RANGE-RATE, RANGE-ACCELERATION, AZIMUTH, AZIMUTH-RATE, AZIMUTH
7      ACCELERATION, CO-ELEVATION, CO-ELEVATION RATE, CO-ELEVATION
8      ACCELERATION OF THE VEHICLE RELATIVE TO ANY VISIBLE SENSOR. IF THE
9      SENSOR OBSERVES THE VEHICLE, ALL DATA IS
10     PRINTED IN THE TOPOCENTRIC COORDINATE SYSTEM.
11
12     DOUBLE PRECISION COST,COSL,SINT,SINL,EX,X,Z,EXD,YD,ZD,XDP,YDP,ZDP
13     *JREQ,W2,W3,W4,W5,XS,ZS,SRS,R$,RSD,XNUM1,XNUM2,XNUM3,
14     *TWOP1,EF,AK,AHREQ
15     *,X1,X3
16     *RS1,RS01
17     DOUBLE PRECISION XNUM,XNUM1,XNUM2,S1K,W9,S2K,S3K,S1K2,$2K2,OPS,E,W6;W7
18     DOUBLE PRECISION XNUM,ED,SIG,W14,W15,SIGD,RSDD,SIGDD,EDD
19     DOUBLE PRECISION SC1,SC2,T,H,XYZ,RSL,PZ,B,W,P,Q
20     DOUBLE PRECISION X,XB,XDD
21     DOUBLE PRECISION EL,ELD,ELDD,REGAM,HDBETA
22     DOUBLE PRECISION TN,STN,TM
23     DOUBLE PRECISION PI,HALFPI,TIHAPI,ARSIN,GOSLT,GNUM,GDEM,BETA,GAM
24     DOUBLE PRECISION AH,XPUM,VPRIME,GNUM2,COSB,BNUM
25     DOUBLE PRECISION HX,VO,THE,GLAMS,THES,GLAMS
26     COMMON/TS/T,H,XYZ,RSL,PZ
27     COMMON/BS/X(3),XD(3),XDD(3)
28     COMMON/ZAX/TM,M
29     COMMON/MS/GAM,BETA,HX,VO,THE,GLAMS,SC1,SC2,AH,THES,GLAMS
30     */ELIM/ELIM
31     */CONCOM/RS,RSD,RSDD,SIG,SIGD,SIGDD,EL,ELD,ELDD,REGAM,HDBETA
32     */OUTCOM/X1,X3
33     */TIME8/TIME8
34     */OPTION/IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC
35     *,IOUT3
36     COMMON/W23459/W2,W3,W4,W5,W9
37     COMMON/E/E
38     LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE
39     *,IOUT3
40     DATA EF/57.2957795130823208/,REQ/20925640.000/,
41     *AK/D,0174532925199432957/,PI/3.14159265358979323/,
42     *HALFPI/1.570796326794896627/,TIHAPI/4771238898038468986/,
43     *TWOP1/6.28318530717958648/
44     COST=DCOS(X(2))
45     COSL=DCOS(X(3))
46     SINT=DSIN(X(2))
47     SINL=DSIN(X(3))
48     EX =X(1)*COST*COSL
49     Y =-X(1)*COST*SINT
50     Z =X(1)*SINT
51     EXD =XD(1)*COST*COSL-X(1)*XD(2)*SINT*COSL-X(1)*XD(3)*COST*SINT
52     YD =-XD(1)*COST*SINT+X(1)*XD(2)*SINT*SINT-X(1)*XD(3)*COST*COSL

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2-76 15.898

## CONVERT TO RADAR COORDINATES

LA

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53      ZD = X(0) + SINT * X(1) * XD(2) * COST
54      XDP = (X(0) - X(1) * XD(2) * XD(2)) - X(1) * (XD(2) * XD(3)) * COST * COSL
55      1   + (2,0D0 * XD(1) * XD(2) * X(1) * XD(2)) * SINT * COSL
56      2   + (2,0D0 * XD(1) * XD(3) * X(1) * XD(3)) * COSY * SINAL
57      3   + 2,0D0 * X(1) * XD(2) * XD(3) * SINT * SINAL
58      YDP = (XD(1) * X(1) * XD(2) * XD(2)) - X(1) * (XD(3) * XD(3)) * COST * SING
59      1   + (2,0D0 * XD(1) * XD(2) * X(1) * XD(2)) * SINT * SINAL
60      2   - (X(1) * XD(3) * 2 * XD0 * XD(1) * XD(3)) * COSY * COSL
61      3   + 2,0D0 * X(1) * XD(2) * XD(3) * SINT * COSL
62      ZDP = (X(0) - X(1) * XD(2) * XD(2)) * SINT
63      1   + (2,0D0 * XD(1) * XD(2) * X(1) * XD(2)) * COSY
64      AHREQ = AH + REQ
65      XS = AHREQ * H3 * H5
66      YS = AHREQ * H3 * H4
67      ZS = AHREQ * H2
68      SRS = DSQRT(XS**2 + YS**2 + ZS**2)
69      S1K = ((EX - XS) * H2 * H3 * (Y - YS) * H2 * H4 * (Z - ZS) * H3)
70      S2K = X(1) * COSY * DSINT * X(3) * H9
71      S3K = (EX - XS) * H3 * H9 * (Y - YS) * H3 * H4 * (Z - ZS) * H2
72      S1K2 = S1K * * 2
73      S2K2 = S2K * * 2
74      S3K2 = S3K * * 2
75      RS1 = DSQRT(S1K2 + S2K2 + S3K2)
76      RSD1 = (EXD * (EX - XS) + YD * (Y - YS) + ZD * (Z - ZS)) / RS1
77      XNUM1 = ((EX - XS) * X0) / RS1
78      XNUM2 = ((Y - YS) * Y0) / RS1
79      XNUM3 = ((Z - ZS) * Z0) / RS1
80      XNUM = (XNUM1 + XNUM2 + XNUM3) / SR8
81      XMUM = (XNUM1 * XNUM2 * XNUM3) / RS1
82      OPS = DSQRT(S1K2 + S2K2)
83      C ELEVATION ANGLE CONSTRAINT ON H01 TRAJECTORY SIMULATION
84      E = DATAN2(10PS, S3K)
85      IF(E > GT, BLIM) GO TO 200
86      47 EL = HALFPI - E
87      RS = RS1
88      RSD = RSD1
89      TIME8 = T
90      X1 = X(1)
91      X3 = X(3)
92      45 W6 = DSIN(E)
93      W7 = DCOS(E)
94      XNLM = XS * EXD + YS * YD + ZS * ZD
95      ED = (-RS * XNLM + XMUM * RSD) / (SR8 * (RS * 21 * W6))
96      ELD = -ED
97      65 SIG = DATAN2(S2K, S1K)
98      IF(SIG, GE, 0, 0D0) GO TO 90
99      SIG = SIG + THOP1
100     90 W14 = DSIN(SIG)
101     W15 = DCOS(SIG)
102     IF(DABS(W14), GE, 1, 0D-16, AND, W6, GT, 0, 0D0) GO TO 105
103     100 SIGD = 0, 0D0
104     GO TO 110

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2-76 15,858 CONVERT TO RADAR COORDINATES LAF

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105      105 SIGD = (EXD*W2*W5 + YD*W2*W4-ZD*W3 + (RSD*W6+RS*ED*W7)*W15)
106          17(RS*W6*W14)
107      110 XpUM1=(X5/RS)*(YDR/RS)
108          XpUM2=(Y5/RS)*(YDR/RS)
109          XpUM3=(Z5/RS)*(ZDR/RS)
110          XpUM = (XpUM1+XpUM2+XpUM3)/W6
111          RSDD=((EX-XS)*XDP+(Y-YS)*YDP+(Z-ZS)*ZDP)
112          1 +(EXD*EXD+YD*YD+ZD*ZD-RSD*RSD))/RS
113          EDD = -XpUM + (XNUM/W6)*(RSDD/RS) = (ED*ED*W7)/W6 - 2.000*ED*RS
114          ./RS
115          EDD=EDD
116          IF(DABS(W14),GE,1.0D-16,AND,W6,GT,0.0D0)GO TO 108
117          SIGDD=0.0D0
118          GO TO 109
119      108 SIGDD=(XDP*W2*W5+YDP*W2*W4-ZDP*W3-2.0D0*RSD*W6*W14+SIGD
120          1 -2.000*RS*W7*W14*ED+SIGD=2.0D0*RS*W8*W15*SIGD
121          2 +2.000*RSDD*W7*W15*ED+RSDD*W6*W18*RS*EDD*W7*W15)/(RS*W6*W14)
122          109 CONTINUE
123          IF(.NOT.IOUT2)RETURN
124
125          C CALCULATION OF HEADING ANGLE(CLOCKWISE 0 TO 2PI)
126
127          COSLT = XD(3)*COST/XD(2)
128          BNUM = XD(3)*COST
129          IF (XD(2)) 1,2,3
130          C ZERO XD(2)
131          2 IF(BNUM) 4,5,6
132          C NEGATIVE BNUM
133          4 BETA = THAP
134          GO TO 60
135          C ZERO BNUM
136          5 BETA = 1.0D1*PI
137          GO TO 60
138          C POSITIVE BNUM
139          6 BETA = HALFPI
140          GO TO 60
141          C NEGATIVE XD(2)
142          1 IF(BNUM) 7,8,9
143          C NEGATIVE OR POSITIVE BNUM
144          7 BETA = PI + DATAN(COSLT)
145          GO TO 60
146          9 BETA = PI + DATAN(COSLT)
147          GO TO 60
148          C ZERO BNUM
149          8 BETA = PI
150          GO TO 60
151          C POSITIVE XD(2)
152          3 IF(BNUM) 10,11,12
153          C NEGATIVE BNUM
154          10 BETA = TWOPI + DATAN(COSLT)
155          GO TO 60
156          C ZERO BNUM

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2-76 15.858 CONVERT TO RADAR COORDINATES

LA

```
157      11 BETA = 0.00000
158      GO TO 60
159      C POSITIVE GNUM
160      12 BETA = DATAN(COS(LT))
161      C CALCULATION OF RE/ENTRY ANGLE(CLOCKWISE 0 TO 2PI)
162      60 COSB = DCOS(BETA)
163      GNUM = X(1)*XD(2) / E0SB
164      GDEM = XD(1)
165      IF(GDEM) 13,14,18
166      C ZERO GDEM
167      14 IF (GNUM) 16,17,18
168      C NEGATIVE GNUM
169      16 ARSIN = TIWARI
170      GO TO 62
171      C ZERO GNUM
172      17 ARSIN = 1.0D1*PI
173      GO TO 62
174      C POSITIVE GNUM
175      18 ARSIN = HALFPI
176      GO TO 62
177      C NEGATIVE GDEM
178      19 IF(GNUM) 19,20,24
179      C NEGATIVE OR POSITIVE GNUM
180      20 ARSIN = TWOPI + DATAN2(GNUM,GDEM)
181      GO TO 62
182      24 ARSIN = DATAN2(GNUM,GDEM)
183      GO TO 62
184      C ZERO GNUM
185      20 ARSIN = PI
186      GO TO 62
187      C POSITIVE GDEM
188      15 IF (GNUM) 21,22,23
189      C NEGATIVE GNUM
190      21 ARSIN = TWOPI + DATAN2 (GNUM,GDEM)
191      GO TO 62
192      C ZERO GNUM
193      22 ARSIN = 0.000
194      GO TO 62
195      C POSITIVE GNUM
196      23 ARSIN = DATAN2 ( GNUM,GDEM)
197      GO TO 62
198      62 GAM = ARSIN
199      REGAM = GAM
200      HDBETA = BETA
201      200 RETURN
202      END
```

MEMORY EXPANDED. USE SLIMITS OR COREM OPTION FOR NEXT RUN

2-76 15.889 COMPUTE ACCELERATION COMPONENTS LA

```

1      CEQTNX      COMPUTE ACCELERATION COMPONENTS
2          SUBROUTINE EQTNX
3          C THIS ROUTINE COMPUTES THE VEHICLE'S ACCELERATION COMPONENTS
4          C REQUIRING VARIABLE BALLISTIC COEFFICIENTS AND DENSITY FROM
5          C ROUTINES BALCOF AND ATMOSPHE, RESPECTIVELY
6
7          DOUBLE PRECISION H,RSL,PZ,T
8          DOUBLE PRECISION V6,EL2,EL3,EL4,EL5,EL6,BA
9          DOUBLE PRECISION DV,XYZ,ZK,S1,S2,S3,S4,S8,VA,VDD,VD,S23,Q1,Q2,Q3
10         DOUBLE PRECISION X,XB,XDD
11         DOUBLE PRECISION A,R,W,TM,B1
12         DOUBLE PRECISION P1
13         LOGICAL IOUT1,IOUT2,IOUT3,KZ,KAT,SPHERE,IPL0T1,IPL0T2
14         DIMENSION DV(5)
15         COMMON/B8/X(3),XD(3),XDD(3)
16         COMMON/TS/T,H,XYZ,RSL,PZ
17         COMMON/A/R,W
18         COMMON/GE/ZK,B1,P1
19         /*OPTION/IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,OUTINC,IOUT3
20         DATA DV/2.4216704D12,4D0,0D0/
21         * ,S6/2.0D0/
22         S1=DCOS(X(2))
23         S2=DSIN(X(2))
24         S3=DSIN(S6*X(2))
25         S4=DCOS(S6*X(2))
26         RSL = R
27         H= X(1)-RSL
28
29         IF(.NOT.KAT)GO TO 31
30         CALL BALCOF
31         CALL ATMOSP
32
33         VA = (XD(1)*XD(1))/(X(1)*X(1)+XD(2)*XD(2)+(S1*(XD(3)+W))**2
34         C VEHICLE'S INERTIAL SPEED (COMPUTED OUTPUT)
35         XYZ=X(1)*DSQRT(VA)
36         VDD= XD(1)*XD(1)+ X(1)*XD(2)*X(1)*XD(2)+(X(1)*(XD(3)-W)*S1)**2
37         C VEHICLE SPEED WRT THE ATMOSPHERIC WIND
38         VD=DSQRT(VDD)
39         S23=-PZ*ZK*VD
40         C DRAG FORCES CONJUGATE TO GEO,RADIUS,LATITUDE,LONGITUDE(FT/MIN/MIN)
41         Q1= S23*XD(1)
42         Q2= S23*XD(2)
43         Q3= S23*(XD(3)-W)
44         V6 = R/X(1)
45         EL2=X(1)*XD(2)*XD(2)+0.5D0*(1,0D0+S4)*(W*XD(3))*(W*XD(3))+X(1)
46         EL3=DV(1)/X(1)+V6+DV(2)/X(1)+V6+3*(3,0D0+S4-1.0D0)
47         EL4=DV(3)/X(1)+V6+5*(35,0D0+S4*S4-10,0D0+S4-13,0D0)
48         C GEOCENTRIC RADIAL ACCELERATION (FT/MIN/MIN)
49         XDD(1)= EL2-EL3+EL4+Q1
50         EL5=(-S6*XD(2)*XD(1))/X(1)-0.5D0*S3*(W*XD(3))*(W*XD(3))
51         EL6=-DV(4)/(X(1)*X(1))*V6+3*S3+DV(5)/(X(1)*X(1))+V6+5*S3*(1,0D0-
52         17,-D0*S4)

```

2-76 15.889 COMPUTE ACCELERATION COMPONENTS LA

53 C GEOCENTRIC LATITUDE ANGULAR ACCELERATION (RAD/MIN/MIN)  
54 XDD(2),EL5.EL6.02  
55 AA=-1.000\*(W\*XD(3))  
56 C GEOCENTRIC LONGITUDE ANGULAR ACCELERATION(RAD/MIN/MIN)  
57 XDD(3),AA= -(S0\*XD(1)/X(1))-AA\*(S0\*XD(2)\*S2)/S1\*03  
58 RETURN  
59 END

2-76 15.896 GEOCENTRIC SPHERICAL COMPONENTS LA

```

1 CICERBM GEOCENTRIC SPHERICAL COMPONENTS
2          SUBROUTINE ICERBM
3
4 C INPUT/OUTPUT MOD 2;MULTIPLE SITE/TRAJECTORY VERSION
5
6 C THIS ROUTINE ACCEPTS BOUNDARY CONDITIONS OF VEHICLE AND COMPUTES
7 C GEOCENTRIC SPHERICAL COMPONENTS OF POSITION AND VELOCITY VECTORS.
8 C IN ADDITION, PERTURBATION TECHNIQUE IS INCORPORATED TO COMPUTE
9 C THE RESULTANT EFFECT OF SINGULAR OR MULTIPLE PERTURBATIONS OF
10 C NOMINAL COMPONENTS OF VELOCITY.
11
12 DOUBLE PRECISION VO,RAT,XX,ZK,B1,P1
13 DOUBLE PRECISION RDP,RTDP,RLDP,C13,GMU,CA,GAM,BETA,GLAM,HX,THE,RO
14 DOUBLE PRECISION XIXB,XDD
15 DOUBLE PRECISION SC1,SC2,T,H,XYZ,RBL,PZ,B,W
16 DOUBLE PRECISION XM, XDN,XN1(20),XDN$(20)
17 DOUBLE PRECISION COSGAM,COSBET,SINGAM,SINBET,V2,A,B,C
18 DOUBLE PRECISION SN1,V80DR,VBO
19 DOUBLE PRECISION RATN
20 DOUBLE PRECISION TN,STN,TM
21 DOUBLE PRECISION THES,GLAMS,AH
22 COMMON/B5/X(3),XD(3),XDD(3)
23 COMMON/TS/T,H,XYZ,RSL,PZ
24 COMMON/AYR,W/M2TRAJ/XX(11)
25 COMMON/AX/TM,MT/GE/ZK,B1,P1
26 COMMON/H5/GAM,BETA,RX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS
27 /*ABC/A(20),B1(20),C(20)
28 */OPTION/IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,IOUT3
29 /*OPT1/INERTL
30 DIMENSION RDP(20),RTDP(20),RLDP(20),XN(3),XDN(3)
31 LOGICAL IOUT1,IOUT2,KZ,IPL0T1,IPL0T2,KAT,SPHERE,IOUT3,INERTL
32 DATA C13/0.0174532925199432957/,GMU/3.0675004019/
33 IF(MT-2)6,10,16
34
6 CONTINUE
35 RO = R + HX
36 XD(1)=VO*DCOS(GAM*C13)
37 IF(GAM.EQ.90.0D0)XD(1)=0.0D0
38 XD(2)=VO/RO*DSIN(GAM*C13)*DCOS(BETA*C13)
39 RAT=RO*DCOS(THE*C13)
40 XD(3)=VO*DSIN(GAM*C13)*DSIN(BETA*C13)/RAY
41 IF(INERTL)XD(3)=XD(3)=W
42 X(1)=RO
43 X(2)=THE*C13
44 X(3)=GLAM*C13
45 IF(.NOT.KZ)GO TO 30
46 DO 15 I=1,3
47 XN1(I) = X(I)
48 15 XDN1(I) = XD(I)
49
50
51 C INITIAL BOUNDARY CONDITIONS TO SIMULATE TIMEWISE BACKWARD TRAJECTORY
52

```

2-76 15.896 GEOCENTRIC SPHERICAL COMPONENTS LAS

```
53      10 R0 = 1.383337301D8
54      X(1) = XM(1)
55      X(2) = TMES*C13
56      X(3) = GLAMS*C13
57      XD(1) = XX(4)
58      XD(2) = MX(5)
59      XD(3) = MX(6)
60      XDD(1) = XX(7)
61      XDD(2) = XX(8)
62      XDD(3) = XX(9)
63      ZK = XX(10)
64      PZ = XX(11)
65      RETURN
66      IF(MT.GT.3)GO TO 35
67      DO 10 I = 1,3
68      XN(I) = X(I)
69      XDN(I) = XD(I)
70      10 CONTINUE
71      RETURN
72      35 IF(.NOT.KZ)GO TO 20
73      DO 40 I=1,3
74      X(I) = XN1(I)
75      XD(I) = XDN1(I)
76      XN(I) = XN1(I)
77      40 XDN(I) = XDN1(I)
78      GO TO 45
79      20 DO 25 I = 1,3
80      X(I) = XN(I)
81      25 CONTINUE
82      45 SN1 = DCOS(XN(2)*C13)
83      VBD0R = DSQRT((XDN(1)/XN(1))**2 + XDN(2)*XDN(2)+(SN1*XD(3))**2)
84      V0 = XN(1) * VBD0R
85      BETA = DATAN2(XDN(3)*SN1 , XDN(2))
86      COSBET = DCOS(BETA)
87      SINBET = DSIN(BETA)
88      COSGAM = XDN(1) / V0
89      SINGAM = XDN(2) / (VBD0R * COSBET)
90      M = MT-3
91      V2 = B(M)*SINGAM*C(M)*COSGAM
92      RDPM(M) = (-B(M)*COSGAM*C(M)*SINGAM)*60.0D0
93      RTDP(M) = (-V2*COSBET*A(M)*SINBET)*60.0D0
94      RLDP(M) = (-V2*SINBET*A(M)*COSBET)*60.0D0
95      XD(1) = XDN(1) + RDPM(M)
96      XD(2) = XDN(2) + RTDP(M)/XN(1)
97      RATN = XN(1)* DCOS(XN(2)*C13)
98      XD(3) = XDN(3) + RLDP(M)/RATN
99      RETURN
100     END
```

QUALITY OR NON-EQUALITY COMPARISON MAY NOT BE MEANINGFUL IN LOGICAL IF EXPRESSIONS

```

CINIT      INITIALIZATION SUBROUTINE          000000010
          SUBROUTINE INITIAL                   000000020
C           INPUT/OUTPUT MOD 2,MULTIPLE SITE/TRAJECTORY VERSION 000000030
C           THIS SUBROUTINE PERFORMS SOME OF THE INITIALIZATION NEEDED FOR THE 000000040
C           PROGRAM, ESPECIALLY FOR PRODUCING OUTPUT. 000000050
C
COMMON/INOUT/INCOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA 000000060
*#TO/TO/TS/T,H,XYZ,RSL,PZ 000000070
*OPTION/IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC,IOUT3 000000080
*RTD/RTD,RTD6,RTD36,F36,F6080,FERU 000000090
COMMON/W23459/W2,W3,W4,W5,W9 00000100
*MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS 00000110
COMMON/GE/ZK,B1,P1/A/H,W/ST/P(3),Q(3) 00000120
*GEOXX/GEO,XK/AX7TM,M 00000130
*SWSW/SWTC1,SWTC2/SW10/SWCH10 00000140
*SW3SW4/SWTC3,SWTC4 00000150
*SW5SW6/SWTC5,SWTC6 00000160
*SW7/SWTC7/SW8/SWTC8/SW9/SWTC9 00000170
*NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC 00000180
*NR6/NREC6/IT2/IT2,IT 00000190
*TIME5/TIME5/TIMEL/TIMEL,TIMES 00000200
COMMON/NR7/NREC7,NOFF4 00000210
*SITES/NSITE,SLAT(20),SLONG(2),SALT(20) 00000220
*ISITE/ISITE 00000230
LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,IOUT3 00000240
LOGICAL SWTC1,SWTC2,SWCH10 00000250
LOGICAL SWTC3,SWTC4 00000260
LOGICAL SWTC5,SWTC6 00000270
LOGICAL SWTC7,SWTC8,SWTC9 00000280
DOUBLE PRECISION ZK,B1,P1,R,W,GEO,XK,P,Q 00000290
DOUBLE PRECISION W2,W3,W4,W5,W9,GAM,BETA,HX,VO,THE,GLAM,SC1,SC2, 00000300
AH,THES,GLAMS,AH,W10,TO,T;H,XYZ,RSL,PZ,TM 00000310
*,SLAT,SLONG,SALT,TIMEL,TIMES 00000320
DATA AH/0.0174532925199432957/ 00000330
RTD = 57.295780 00000340
RTD60 = RTD/6. 00000350
RTD36 = RTD/360. 00000360
F36= 1.0/360.0 00000370
F6080 = 1.0/6080.0 00000380
FERU = 1.0/20925640. 00000390
T = 0.0D0 00000400
PZ = 0.0D0 00000410
ZK = 0.0D0 00000420
DO 11 I=1,3 00000430
P(I)=0.0D0 00000440
11 Q(I)=0.0D0 00000450
IF(M.NE.2)GO TO 2 00000460
T = TIMEL 00000470
SWCH10 = .FALSE. 00000480
IF(T.LT.TIMES+TO)GO TO 2 00000490
                                         00000500
                                         00000510
                                         00000520

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      BWTCH10 = .TRUE.
      ET2 = (T-TIMES+1)D-5)/T0
20  ENCOUT = (OUTINC + 1.0E-03)/T0
      EOUT = 0
      EOUTA = 0
      NOFF1 = 676
      IF(IOUT1)NOFF1=364
      NOFF2 = 624
      NOFF3 = NOFF2
      IF(IOUT2)NOFF2=364
      IF(IPLOT2)NOFF3=364
      NOFF4= 554
      IF(ISITE,EQ,0)GO TO 10
      SC1 = SLAT(ISITE)
      SC2 = SLONG(ISITE)
      RH = SALT(ISITE)
      W9=SC2*AK
      W10 = SC1*AK
      W2 = DSIN(W10)
      W3 = DCOS(W10)
      W4 = DSIN(W9)
      W5 = DCOS(W9)
10   TIME5 = 0.0
      REC1 = 0
      REC2 = 0
      REC3 = 0
      REC4 = 0
      REC5 = 0
      REC6 = 0
      REC7=0

C PHYSICAL CONSTANTS OF THE EARTH MODEL, EQUATORIAL RADIUS AND ANGULAR
C SPEED
      R = 20925640.00
      W=0.437526948D-2
      RK=5.72961D-1

C UPPER VALUE OF THE TARGET'S GEOCENTRIC RADIAL DISTANCE(FT)
      GEO = 1.383337801D8
      P1 = 0.0D0
      BWTCH1 = .TRUE.
      BWTCH2 = .TRUE.
      BWTCH3 = .FALSE.
      BWTCH4 = .TRUE.
      BWTCH6 = .TRUE.
      BWTCH7 = .TRUE.
      BWTCH8=.TRUE.
      BWTCH9 = .TRUE.
      RETURN
      END

```

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CINPUT	INPUT SUBROUTINE	00001050
	SUBROUTINE INPUT	00001060
C	THIS ROUTINE PERFORMS THE INPUT FUNCTION THRU CARDS FOR THE #PROGRAM.	00001070
	COMMON/AX/TM,M/NTRAJ/ITM	00001080
	*#MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS	00001090
	*#ELIM/ELIM/NSWTCH/NSWTCH	00001100
	*#OPTION/IOUT1,ZOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC,IOUT3	00001110
	*#OPT1/INERTL	00001120
	*#ABC/A(20),B(20),C(2)	00001130
	COMMON/SITES/NSITE,SLAT(20),SLONG(20),SALT(20)	00001140
	DOUBLE PRECISION GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS,TM,	00001150
	*#LIM,A,B,C,SLAT,SLONG,SALT	00001160
	LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,IOUT3,IEOFFP,INERTL	00001170
	DATA DTR/.117453293/	00001180
	#AMELIST/INPUT1/NTRAJ,TM,NSWTCH	00001190
	*#INPUT2/IOUT1,IPLOT1,IPLOT2,IOUT2,KAT,KZ,SPHERE,OUTINC,IOUT3	00001200
	*#INERTL	00001210
	*#INPUT3/GAM,BETA,HX,VO,THE,GLAM,THES,GLAMS	00001220
	*#INPUT4/NSITE,SLAT,SLONG,SALT,ELIM	00001230
	*#INPUT5/A,B,C	00001240
	CALL FLGEOF (~5,TEOFFP)	00001250
C	INPUT TRAJECTORY NUMBER,TIME LIMIT,MAIN PROCESSING SWITCH	00001260
	READ(5,INPUT1)	00001270
	IF(IEOFFP)STOP	00001280
	ITM = NTRAJ	00001290
	WRITE(6,10)NTRAJ,TM,NSWTCH	00001300
10	FORMAT(1H1//5x,"MISSILE TRAJECTORY PROGRAM(MULTIPLE SITE/TRAJECTOR")	00001310
	*# MOD) INPUTS"/>714x,"PROGRAM CONTROLS"//10x,"NUMBER OF TRAJECTORY",I6	00001320
	*#ES SIMULATED(NTRAJ)",I6/710x,"MAXIMUM TIME FOR A TRAJECTORY(TM)",I6	00001330
	*#15.5," MIN."//10x,"MAIN PROCESSING SWITCH(NSWTCH)",I6	00001340
C	INPUT OTHER PROGRAM CONTROLS	00001350
	READ(5,INPUT2)	00001360
	WRITE(6,60)IOUT1,IOUT2,OUTINC,IOUT3,KZ,IPLOT1,IPLOT2,KAT,SPHERE	00001370
60	FORMAT(/>10x,25HPRINT-OUT OPTION 1(IOUT1),L6,10x,25HPRINT-OUT OPTION 2(IOUT2),L6/>1 X,51HINCREMENT BETWEEN TIME POINTS FOR PRINT-OUT	00001380
	*#ON 2(IOUT2),L6/>1 X,51HINCREMENT BETWEEN TIME POINTS FOR PRINT-OUT	00001390
	*#OUTINC,F1 .3.5H MIN./>1 X,54HPRINTOUT OPTION FOR RADAR PARAMETER	00001400
	*# DIFFERENCES(IOUT3),L6,1 X,39HNOMINAL TRAJECTORY SELECTION SWITCH(KZ),L6//>10x,25HPLOTTING OPTION 1(IPLOT1),L6,10x,25HPLOTTING OPTION 2(IPLOT2),L6/>1 X,29HATMOSPHERIC MODEL OPTION(KAT),L6//>10x,29HSP	00001410
	*#HERICAL EARTH MODEL(SPHERE),L6	00001420
	WRITE(6,65)INERTL	00001430
65	FORMAT(/>10x,32HINERTIAL VELOCITY OPTION(INERTL),L6)	00001440
		00001450
		00001460
		00001470
		00001480
		00001490
		00001500
		00001510
		00001520
		00001530
		00001540
		00001550
		00001560



```
      WRITE(6,B )(B(I),I=1,NT)          JCUC2090
80  FORMAT(//1 X,80HIN PLANE PERTURBATION, +EJECTED BACKWARDS FROM NOMIN0002100
*FINAL TRAJECTORY(B) IN FT./SEC.//(5X,5D17.5))    000 2110
      WRITE(6,C )(C(I),I=1,NT)          000 2120
100 FORMAT(//1 X,78HIN PLANE PERTURBATION, +EJECTED UPWARDS FROM NOMIN0002130
*AL TRAJECTORY(C) IN FT./SEC.//(5X,5D17.5))    000 2140
      RETURN                           000 2150
      END                             000 2160
```

```

CINTRAJ      INPUT TRAJECTORY DATA FROM FILE
C
C      SUBROUTINE INTRAJ
C
C      THIS ROUTINE READS THE TRAJECTORY DATA PLACED ON A FILE
C      SO THAT RADAR COVERAGE PARAMETERS MAY BE COMPUTED.
C      IT WILL ALSO READ AND STORE RADAR DATA NEEDED FOR CALCULATING
C      RADAR PARAMETER DIFFERENCES.
C
C      COMMON/NR7/NREC7,NOFF4/AX/TM,NTRJ/ISITE/ISITE
C      /OUTT/OUTTJ(57)/NSWTCH/NSWTCH
C      /JX/JX/TIME1/TIME1/BS/TE(2)
C      /SITES/NSITE,SLAT(2),SLONG(20),SALT(20)
C      /TSIGHT/TIMESI(1),10,5),TIMESF(10,10,5),NSIGHT(10,10)
C      /NTRAJ/NTRAJ/IJJ/TNOM,I,JSITE,JSIGHT,TSTART,TEND
C      /OPTION/IOUT1,IOUT2,KZ,IPLQT1,IPLQT2,KAT,SPHERE,OUTINC,
C      IOUT3
C      DOUBLE PRECISION TM,SLAT,SLONG,SALT
C      LOGICAL IPLQT2,EOF,SWTCH2,EOF10,
C      IOUT1,IOUT2,KZ,IPLQT1,IPLQT2,KAT,SPHERE,IOUT3
C      IF(NTRJ.GT.2)GO TO 20
C      REWIND 9
C      50 READ(9)IREC,TIME1
C      RETURN
C      20 IF(NSWTCH.EQ.2)GO TO 25
C      IF(ISITE.NE.1)GO TO 3
C      35 BACKSPACE 9
C      READ(9)IREC,NREC7
C      IBACK=IREC
C      IF(NREC7.EQ.0.AND.IREC.EQ.2)RETURN
C      30 DO 40 IB=1,IBACK
C      40 BACKSPACE 9
C      GO TO 50
C      25 IF(ISITE.EQ.1)GO TO 50
C      IF(ISITE.EQ.2)GO TO 35
C      GO TO 30
C
C      ENTRY TRAJIN
C      READ(9)IREC,NREC7
C      IF(NREC7.EQ.0)RETURN
C      NDATA = NREC7*9
C      READ(9)IREC,(OUTTJ(I),I=1,NDATA)
C      RETURN
C
C      ENTRY TRAJX
C
C      STORE TRAJECTORY DATA FROM INPUT BUFFER IN TRAJECTORY
C      ARRAYS
C
C      II=1
C      DO 10 JJ=JX,JX+2
C      TR{II}=OUTTJ(JJ)
C
C      00000050
C      00000055
C      00000060
C      00000065
C      00000070
C      00000080
C      00000085
C      00000086
C      00000087
C      00000090
C      00000100
C      00000110
C      00000115
C      00000116
C      00000117
C      00000118
C      00000119
C      00000120
C      00000125
C      00000126
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C      00000140
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C      00000340
C      00000350
C      00000360
C      00000370
C      00000380
C      00000390
C      00000400

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II=II+1          00000410
10 CONTINUE      00000420
JX=JX+9          00000430
RETURN           00000440
C               00000450
C               00000460
C               00000470
C               00000480
C               00000490
C               00000500
C               00000510
C               00000520
C               00000530
C               00000540
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C               00000840
C               00000850
C               00000860
C               00000870
C               00000880
C               00000890

II=II+1          00000410
10 CONTINUE      00000420
JX=JX+9          00000430
RETURN           00000440
C               00000450
C               00000460
C               00000470
C               00000480
C               00000490
C               00000500
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C               00000790
C               00000795
C               00000800
C               00000810
C               00000820
C               00000830
C               00000840
C               00000850
C               00000860
C               00000870
C               00000880
C               00000890

C               ENTRY TIMEST
C               READ IN AND STORE TIMES OF SIGHTING FOR COMPUTATION OF
C               RADAR PARAMETER DIFFERENCES.
C               READ IN AND STORE TIMES OF SIGHTING OF NOMINAL TRAJECTORY
C               BY ALL RADAR SITES.
C               REWIND 11
INOM=1
IF(.NOT.KZ)INOM=3
JJ=1
II=0
130 READ(11)TIME3,IPL0T2,IC2,EOF
IF(EOF)GO TO 10
II=II+1
TIMESI(INOM,JJ,II)=TIME3
120 READ(11)NREC3,ITR,IS,EOF1,SWTCH2
IF(EOF10)GO TO 11
READ(11)DUMMY
GO TO 120
110 READ(11)TIME7
TIMESF(INOM,JJ,II)=TIME7
GO TO 130
100 NSIGHT(INOM,JJ)=II
IF(JJ.EQ.NSITE)GO TO 140
JJ=JJ+1
II=0
GO TO 130
C               READ IN AND STORE TIMES OF SIGHTING OF ALL OTHER TRAJECTORIES
C               BY ALL SITES.
C               140 REWIND 11
REWIND 1
IF(.NOT.KZ)GO TO 15
195 JJ=1
190 READ(10)DUM,DUM,DUM,EOF
IF(EOF)GO TO 160
180 READ(10)DUM,DUM,DUM,EOF10,DUM
IF(EOF10)GO TO 170
READ(10)DUM
GO TO 180
170 READ(10)DUM
GO TO 190
160 IF(JJ.EQ.NSITE)GO TO 200

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JJ=JJ+1	00000900
GO TO 190	00000910
150 ITRAJ=1	00000915
GO TO 270	00000917
200 ITRAJ=4	00000920
270 JJ=1	00000930
II=0	00000950
220 READ(10)TIME3,DUM,DUM,EOF	00000960
IF(EOF)GO TO 230	00000970
II=II+1	00000980
TIMESI(ITRAJ,JJ,II)=TIME3	00000990
240 READ(10)NRECG,ITR,IS,EOF1,SWTCH2	00001000
IF.EOF1)GO TO 25	00001010
READ(10)DUMMY	00001020
GO TO 240	00001030
250 READ(10)TIME7	00001040
TIMESF(ITRAJ,JJ,IT)=TIME7	00001050
GO TO 220	00001060
230 NSIGHT(ITRAJ,JJ)=FI	00001070
IF(JJ.EQ.NSITE)GO TO 260	00001080
JJ=JJ+1	00001090
II=0	00001100
GO TO 220	00001110
260 IF(ITRAJ.EQ.1)GO TO 195	00001115
IF(ITRAJ.EQ.NTRAJ)GO TO 280	00001120
ITRAJ=ITRAJ+1	00001130
GO TO 270	00001140
280REWIND 10	00001150
RETURN	00001160
C ENTRY INTER	00001170
C DETERMINE THE INTERSECTIONS OF THE TIME SETS	00001180
C JSIGHT=1	00001190
IF(TIMESI(INOM,JSITE,JSIGHT).GE.TIMESI(I,JSITE,JSIGHT))	00001200
8 GO TO 290	00001210
IF(TIMESF(INOM,JSITE,JSIGHT),LE,TIMESF(I,JSITE,JSIGHT))	00001220
8 GO TO 300	00001230
TSTART=TIMESI(I,JSITE,JSIGHT)	00001240
TEND=TIMESF(I,JSITE,JSIGHT)	00001250
310 RETURN	00001260
300 TSTART=TIMESI(I,JSITE,JSIGHT)	00001270
TEND=TIMESF(INOM,JSITE,JSIGHT)	00001280
GO TO 310	00001290
290 IF(TIMESF(INOM,JSITE,JSIGHT).GE.TIMESF(I,JSITE,JSIGHT))	00001300
8 GO TO 320	00001310
TSTART=TIMESI(INOM,JSITE,JSIGHT)	00001320
TEND=TIMESF(INOM,JSITE,JSIGHT)	00001330
GO TO 310	00001340
320 TSTART=TIMESI(INOM,JSITE,JSIGHT)	00001350
TEND=TIMESF(I,JSITE,JSIGHT)	00001360
	00001370
	00001380
	00001390

GO TO 310  
END

00001400  
00001410

C OUTPUT	OUTPUT SUBROUTINE	
	SUBROUTINE OUTPUT	00000010
C	INPUT/OUTPUT MOD 2, MULTIPLE SITE/TRAJECTORY VERSION	00000020
C	THIS SUBROUTINE PRODUCES THE PRINT-OUT OF THE RESULTS OF A PROGRAM	00000030
C	RUN. MISSILE/SATELLITE TRAJECTORY PARAMETERS(POSITION, VELOCITY, ETC)	00000040
C	) ARE PRINTED-OUT. AS ARE THE TRAJECTORIES AS SEEN BY VARIOUS	00000045
C	RADAR SITES.	00000050
C	THIS ROUTINE ALSO IS USED FOR TEMPORARY STORAGE OF	00000060
C	TRAJECTORY AND RADAR DATA AND CAN WRITE A FILE	00000070
C	FOR LATER USE IN PLOTTING.	00000080
C	COMMON/TS/T,H,XYZ,RSL,PZ	00000085
C	*7CONCOM/RS,RSDD,SIG,SIGD,SIGDD,EL,ELD,ELDD,REGAM,HDBETA	00000090
C	*7OUTCOM/X1,X3/TIME2/TIME2	00000100
C	*7TIME8/TIME8/ISITE/ISITE	00000110
C	*7BS/X(3),XD(3),XDD(3)	00000120
C	*7MS/GAM,BETA,HX,VO,THE,GLAM,SC1,SC2,AH,THES,GLAMS	00000130
C	*7GE/ZK,B1,P1	00000140
C	*7OPTION/IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE,OUTINC,IOUT3	00000150
C	*7RTD/RTD,RTD6,RTD36,F36,F608,FERU	00000160
C	*7SWSW/SWTC1,SWTC2	00000170
C	*7SW3SW4/SWTC3,SWTC4	00000180
C	*7SWSSW6/SWTC5,SWTC6	00000190
C	*7TIME5/TIME5/TIMEL,TIMES	00000200
C	*7AX/TM,NTRJ/M2TRAJ/XX(11)	00000210
C	COMMON/NR/NREC1,NREC2,NREC3,NREC4,NREC5,NREC	00000220
C	*7NR6/NREC6/SW10/SWCH10	00000230
C	*7IO/IO,IO1,IO2	00000240
C	*7INOUT/INCOUT,IOUT,NOFF1,NOFF2,NOFF3,IOUTA	00000250
C	COMMON/NR7/NREC7,NOFF4	00000260
C	*7OUTT/OUTTBJ(5000),OUTTRJ(5000),OUTRAD(5000),OUTPLT(5000)	00000270
C	*7SITES/NSITE,SLAT(20),SLONG(20),SALT(20)	00000280
C	DOUBLE PRECISION T,H,XYZ,RSL,PZ,X,XD,XDD,ZK,B1,P1,GAM,BETA,HX,VO,	00000285
C	*THE,GLAM,SC1,SC2,AH,THES,GLAMS,RS,RSDD,SIG,SIGD,SIGDD,EL,ELD,	00000290
C	*ELDD,REGAM,HDBETA,TM,X1,X3,TIMEL,TIMES	00000300
C	,XX,SLAT,SLONG,SALT	00000310
C	LOGICAL IOUT1,IOUT2,KZ,IPLOT1,IPLOT2,KAT,SPHERE	00000320
C	,IOUT3	00000330
C	LOGICAL SWITCH,SWTC1,SWTC2,SWTC3,SWTC4,SWTC5,SWTC6	00000340
C	,EOF8,EOF10,EOF,SWCH10	00000350
C	TIME1 = T	00000360
C	ISTOR1 = 1	00000370
C	IO = 7	00000380
C	IF(IOUT1)IO=13	00000390
C	NREC1 = 0	00000400
C	ISTOR4=1	00000410
C	IF(NTRJ.NE.2)GO TO 120	00000420
C	OUTINC=OUTINC	00000430
C	SWITCH=.FALSE.,	00000440
C	SWTC1=.FALSE.,	00000450
C		00000460
C		00000470
C		00000480
C		00000490
C		00000500
C		00000505
C		00000510
C		00000512
C		00000515
C		00000517

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120 IF(NTRJ.EQ.3)OUTINC=-OUTINC          00000518
                                              00000520
ENTRY STORJ                                00000530
                                              00000540
C   STORE DATA FROM MISSILE/SATELLITE TRAJECTORY FOR PRINT-OUT 00000550
                                              00000560
IOUT = 0                                     00000570
TIMES = T                                     00000577
OUTTRJ(ISTOR1) = X(1)                         00000580
OUTTRJ(ISTOR1+1) = X(2)*RTD                00000590
OUTTRJ(ISTOR1+2) = X(3)*RTD                00000600
OUTTRJ(ISTOR1+3) = H                         00000610
OUTTRJ(ISTOR1+4) = XYZ*0. 16666667          00000620
OUTTRJ(ISTOR1+5) = ZK                        00000630
OUTTRJ(ISTOR1+6) = PZ                        00000640
ISTOR1 = ISTOR1 + 7                          00000650
NREC1 = NREC1 + 1                            00000660
IF(.NOT.IOUT1)RETURN                         00000670
OUTTRJ(ISTOR1) = XD(1)*0. 16666667          00000680
OUTTRJ(ISTOR1+1) = XD(2)*RTD6               00000690
OUTTRJ(ISTOR1+2) = XD(3)*RTD6               00000700
OUTTRJ(ISTOR1+3) = XDD(1)*F36              00000710
OUTTRJ(ISTOR1+4) = XDD(2)*RTD36             00000720
OUTTRJ(ISTOR1+5) = XDD(3)*RTD26             00000730
ISTOR1 = ISTOR1 + 6                          00000740
RETURN                                         00000750
                                              00000760
ENTRY STORTR                                00000770
                                              00000780
C   STORE TRAJECTORY DATA FOR RADAR COMPUTATIONS 00000790
                                              00000800
NREC7 = NREC7+1                             00000810
OUTTJ(ISTOR4)=X(1)                          00000820
OUTTJ(ISTOR4+1)=X(2)                        00000830
OUTTJ(ISTOR4+2)=X(3)                        00000840
OUTTJ(ISTOR4+3)=XD(1)                        00000850
OUTTJ(ISTOR4+4)=XD(2)                        00000860
OUTTJ(ISTOR4+5)=XD(3)                        00000870
OUTTJ(ISTOR4+6)=XDD(1)                       00000880
OUTTJ(ISTOR4+7)=XDD(2)                       00000890
OUTTJ(ISTOR4+8)=XDD(3)                       00000900
ISTOR4= ISTOR4+9                           00000910
RETURN                                         00000920
                                              00000930
ENTRY OUTTRI                                00000940
                                              00000950
IREC=1                                     00000955
WRITE(9)IREC,TIME1                         00000960
RETURN                                         00000970
                                              00000980
ENTRY OUTTR                                00000990
                                              00001000

```

```

C OUTPUT TRAJECTORY DATA ON A FILE          00001010
                                            00001020
IREC=IREC+1                                00001025
WRITE(9)IREC,NREC7                          00001030
IF(NREC7.EQ.0)RETURN                         00001040
NDATA = NREC7*9                             00001050
IREC=IREC+1                                00001055
WRITE(9)IREC,(OUTTJ(I),I=1,NDATA)           00001060
NREC7 = 0                                    00001070
ISTOR4=1                                     00001080
RETURN                                         00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001220
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500

C COMPUTE SECOND RADAR TIME POINT TO BE PRINTED OUT      00001130
TIME4 = T/OUTINC                               00001140
ITIME = TIME4                                 00001150
IF(TIME4>FLOAT(ITIME).LT.1.0E-5)GO TO 80    00001160
RETURN                                         00001170
80 SWTCH4 = .FALSE.
IOUTA = INCOUT                                00001180
TIME4 = T                                      00001190
NREC6 = 2                                     00001200
RETURN                                         00001210
00001220
00001230
00001240
00001250
00001260
00001270
00001280
00001290
00001300
00001310
00001320
00001330
00001340
00001350
00001360
00001370
00001380
00001390
00001400
00001410
00001420
00001430
00001440
00001450
00001460
00001470
00001480
00001490
00001500

C STORE RADAR DATA FROM MISSILE/SATELLITE      00001330
90 IOUTA = 0                                    00001340
TIMES = T                                      00001350
OUTRAD(ISTOR2) = RS*F609                      00001360
OUTRAD(ISTOR2+1) = RSD*0.16666667              00001370
OUTRAD(ISTOR2+2) = ELD*RTD                     00001380
OUTRAD(ISTOR2+3) = ELD*RTD60                  00001390
OUTRAD(ISTOR2+4) = SIG*RTD                     00001400
OUTRAD(ISTOR2+5) = SIGD*RTD60                 00001410
OUTRAD(ISTOR2+6) = X1*FERU                     00001420
OUTRAD(ISTOR2+7) = X3*RTD - GLAMS             00001430
ISTOR2 = ISTOR2 + 8                           00001440
NREC2 = NREC2 + 1                            00001450
IF(.NOT.IOUT2)RETURN                         00001460
OUTRAD(ISTOR2) = RSDD*F36                     00001470
OUTRAD(ISTOR2+1) = ELD2*RTD36                 00001480
OUTRAD(ISTOR2+2) = SIGD*RTD36                 00001490
OUTRAD(ISTOR2+3) = RGAM1*RTD                  00001500

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OUTRAD(ISTOR2+4) = HDBETA*RTD          00001510
ISTOR2 = ISTAR2 + 5                     00001520
RETURN                                   00001530
ENTRY STRADL                            00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
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00001721
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00001750
00001760
00001770
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00001790
00001800
00001810
00001820
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00001860
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00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960

```

C DETERMINE LAST RADAR TIME POINT FOR STORAGE AND PRINT-OUT

IF(TIME8.LT.TIME5+0.01)RETURN

TIME6 = TIME8

NREC6 = 3

GO TO 90

ENTRY PRINTT

C OUTPUT TRAJECTORY DATA

IF(NREC1.EQ.0)GO TO 5

I011 = IO - 1

MOD52 = MOD(NREC1,52)\*IO

NPAGE = NREC1/52 + 1

IF(MOD52.EQ.0)NPAGE=NPAGE-1

K52 = 52\*IO

IF(NTRJ.NE.2)GO TO 85

IF(SWITCH)GO TO 85

SWITCH=.TRUE.

IF(TIME2-TIME1.EQ.OUTINC)GO TO 85

SWITCH=.TRUE.

25 DO 40 NP=1,NPAGE

IEND = NP\*K52

ISTART = (NP-1)\*K52 + 1

IF(SWTCHR)GO TO 18

IF(NP.NE.NPAGE)GO TO 30

IF(MOD52.EQ.0)GO TO 30

IF(NPAGE.EQ.1)GO TO 50

IEND = ISTART - 1 + MOD52

30 IF(IOUT1)GO TO 35

WRITE(6,1)NTRJ,(TIME1+(I/IO)\*OUTINC,(OUTTRJ(J),J=I,I+IO-1),I=ISTART,\*,RT,IEND,IO)

10 FORMAT(1H1,1X,41HTRAJECTORY PARAMETERS , TRAJECTORY NUMBER,I4//5X00001830

\*, 9HTIME(MIN),2X,1HRADIUS(FT),2X,13HLATITUDE(DEG),2X,14HLONGITUDE00001840

\* (DEG),2X,1HHHEIGHT(FT),2X,14HVELOCITY(FT/S),2X,21HBAL.COEFF.(FT\*\*200001850

\*/SLG),2X,22HATMOS.DENS.(SLG/FT\*\*3)/(6X,F7.2,1X,E12.5,3X,F7.2,8X,F800001860

\*.2,5X,E12.5,3X,E13.6,4X,E12.5,12X,E12.5))

GO TO 40

50 IEND = MOD52

GO TO 30

35 WRITE(6,15)NTRJ,(TIME1+(I/IO)\*OUTINC,(OUTTRJ(J),J=I,I+IO-1),I=ISTART,\*,RT,IEND,IO)

15 FORMAT(1H1,1X,41HTRAJECTORY PARAMETERS , TRAJECTORY NUMBER,I4//3X00001930

\*,4HTIME,4X,6HRADIUS,1X,8HLATITUDE,1X,9HLONGITUDE,4X,6HHEIGHT,3X,8H0000194

\*VELOCITY,2X,6HBALCOF,2X,5HATDEN,5X,5HR-DOT,1X,7HLAT-DOT,1X,6HLONG-0000195

\*DOT,2X,8HR-DOTDOT,1X,10HLAT-DOTDOT,1X,11HLONG-DOTDOT/2X,5H(MIN),5X00001960

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*,4H(FT),4X,5H(DEG),4X,5M(DEG),7X,4H{FT},5X,6H(FT/S),4X,7H(F2/S),100001872
*X,7H(SG/F3),4X,6H(FT/S),4X,7H(DEG/S),2X,1DEG/S),4X,9H(FT/S),100001982
*X,10H(DEG/S)**2,2X,1H(DEG/S**2)/(1X,F6,2,1X,E9,3,2X,F7,2,2X,F8,2,00001990
*X,E9,3,1X,E11,3,1X,F5,2,E9,2,E12,3,1X,F7,4,1X,F8,5,2X,F8,4,1X,00002000
*E10,3,2X,E11,31)00002010
GO TO 400002020
00002030
C PRINT OUT 1ST,2ND,& FOLLOWING TIME POINTS FOR 2ND TRAJECTORY00002040
C 180 SWTCHE=.FALSE.00002050
IF(NPAGE,NE,1)GO TO 24000002060
IF(MOD52,EQ,.)GO TO 24000002070
IEND=MOD52000002080
240 IF(IOUT1)GO TO 24500002090
WRITE(6,10)NTRJ,TIME1,(OUTTRJ(J),J=1,IO)00002100
ISTART=ISTART+IO00002110
WRITE(6,60)(TIME2+((I-IO)/IO)*OUTINC,(OUTTRJ(J),J=I,
*I+IO11),I=ISTART,IEND,IO)00002120
255 TIME1=TIME2-OUTINC00002130
GO TO 4000002140
00002150
245 WRITE(6,15)NTRJ,TIME1,(OUTTRJ(J),J=1,IO)00002160
ISTART=ISTART+IO00002170
WRITE(6,75)(TIME2+((I-IO)/IO)*OUTINC,(OUTTRJ(J),J=I,
*I+IO11),I=ISTART,IEND,IO)00002180
GO TO 25500002190
00002202
40 CONTINUE00002210
TIME1 = TIME1 + (IEND/IO)*OUTINC00003000
5 IF(SWTCHE3)GO TO 2000003010
ISTOR1 = 100003020
NREC1 = 000003030
65 TIMEL=T000003040
RETURN000003050
000003060
000003070
C PRINT OUT LAST TIME POINT000003080
000003090
20 IF(NTRJ,NE,21)GO TO 2100003100
IF(T.GT.TIMES-0.01D0)GO TO 6500003110
GO TO 2200003120
21 IF(T.LT.TIMES+0.01D0)GO TO 6500003130
22 OUTTRJ(1) = X(1)00003140
OUTTRJ(2) = X(2)*RTD00003150
OUTTRJ(3) = X(3)*RTD00003160
OUTTRJ(4) = H00003170
OUTTRJ(5) = XYZ*.J., 1666666700003180
OUTTRJ(6) = ZK00003190
OUTTRJ(7) = PZ00003200
IF(.NOT.IOUT1)GO TO 2500003210
OUTTRJ(8) = XD(1)*. 1666666700003220
OUTTRJ(9) = XD(2)*RTD6000003230
OUTTRJ(10) = XD(3)*RTD6000003240
OUTTRJ(11) = XD(1)*F3600003250
OUTTRJ(12) = XD(2)*RTD3600003260

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        OUTTRJ(13) = XDD(3)*RTD36          00003270
        GO TO 45                           00003280
25 IF(MOD52.EQ. )GO TO 55             00003290
        WRITE(6,6 )T,(OUTTRJ(J),J=1,IO)    00003300
60 FORMAT(6X,F7.2,1X,E12.5,3X,F7.2,8X,F8.2,5X,E12.5,3X,E13.6,4X,E12.5) 00003310
        *,12X,E12.5)                   00003320
        GO TO 65                           00003330
55 WRITE(6,10)NTRJ,T,(OUTTRJ(J),J=1,IO) 00003340
        GO TO 65                           00003350
45 IF(MOD52.EQ. )GO TO 70             00003360
        WRITE(6,75)T,(OUTTRJ(J),J=1,IO)    00003370
75 FORMAT(1X,F6.2,1X,E9.3,2X,F7.2,2X,F8.2,1X,E9.3,1X,E10.3,1X,F5.2, 00003380
        *,E9.2,E10.3,1X,F7.4,1X,F8.5,2X,F8.4,1X,E10.3,2X,E10.3) 00003390
        GO TO 65                           00003400
70 WRITE(6,15)NTRJ,T,(OUTTRJ(J),J=1,IO) 00003410
        GO TO 65                           00003420
        00003430
        ENTRY OUTRDR                    00003440
C      OUTPUT RADAR DATA ON FILE       00003450
EOF8 = .FALSE.                         00003460
WRITE(08)NREC2,NREC6,EOF8              00003470
IF(NREC2.EQ. )RETURN                  00003480
IF(NREC6.EQ.1.OR.NREC6.EQ.2)WRITE(08)TIME2,TIME4 00003490
IF(NREC6.EQ. )GO TO 95                00003500
IF(NREC6.EQ.3)WRITE( 8)TIME2,TIME4,TIME6 00003510
95 NREC = NREC2*I01                   00003520
WRITE(08)(OUTRAD(I),I=1,NREC)         00003530
ISTOR2 = 1                            00003540
NPEC2 = 0                            00003550
NREC6 = 0                            00003560
RETURN                                00003570
ENTRY OUTEOF                        00003580
EOF8 = .TRUE.                          00003590
WRITE(08)NREC2,NREC6,EOF8              00003600
RETURN                                00003610
ENTRY PRINTR                         00003620
C      OUTPUT RADAR DATA ON PRINTER   00003630
REWIND 8                            00003640
I011 = I01 - 1                      00003650
140 SWITCH = .TRUE.                  00003660
SWTCHR = .FALSE.                     00003670
8 READ(08)NREC2,NREC6,EOF8            00003680
IF(EOF8)GO TO 14                     00003690
IF(NREC2.EQ. )GO TO 300               00003700
NREC = NREC2*I01                     00003710
IF(NREC6.EQ.1.OR.NREC6.EQ.2)READ(08)TIME2,TIME4 00003720
IF(NREC6.EQ. )GO TO 130               00003730
IF(NREC6.EQ.3,AND.SWITCH)READ(08)TIME2,TIME4,TIME6 00003740
IF(NREC6.EQ.3,AND.(.NOT.SWITCH))READ(08)DUM,DUM,TIME6 00003750
130 READ(08)(OUTRAD(I),I=1,NREC)     00003760
MOD52 = MOD(NREC2,52)*I01           00003770
NPAGE = NPEC2/52 + 1                 00003780

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IF(MOD52.EQ.0)NPAGE=NPAGE-1          00003790
K52 = 52*I01                         00003800
DO 110 NP=1,NPAGE                   00003810
IEND = NP*K52                       00003820
ISTART = (NP-1)*K52 + 1              00003830
IF(NP.EQ.1)GO TO 150                00003840
160 IF(NP.EQ.NPAGE)GO TO 155         00003850
IF(NP.NE.NPAGE)GO TO 105            00003860
200 IF(MOD52.EQ.0)GO TO 105         00003870
IF(NPAGE.EQ.1)GO TO 115             00003880
IEND = ISTART + MOD52               00003890
105 IF(IOUT2)GO TO 10               00003900
WRITE(6,125)NTRJ,ISITE,SC1,SC2,(TIME2+(I/I01)*OUTINC, 00003910
*OUTRAD(J),J=I,I+I011),I=ISTART,IEND,I01           00003920
125 FORMAT(1H1,10X,36HRADAR PARAMETERS, TRAJECTORY NUMBER,I4,3X,10HRA 00003930
*DAR SITE,I4,F12.3," DEG,LAT.",F12.3," DEG,LONG." //5X,"TIME",7X,8H00003940
*SL RANGE,4X,13HSL RANGE-RATE,3X,9HELEVATION,7X,7HEL RATE,4X,7HAZIM00003950
*UTH,6X,7HAZ RATE,4X,6HRADIUS,4X,12HINERTIAL PHI/4X,5H(MIN),10X,4H(00003960
*NH,8X,6H(FT/S),9X,5H(DEG),9X,7H(DEG/S),5X,5H(DEG),7X,7H(DEG/S),4X00003970
*5H(ERU),9X,5H(DEG)/(12X,F7.2,2X,E13.6,4X,E13.6,5X,F7.2,3X,E11.4,4X00003980
*,F7.2,2X,E11.4,3X,F7.3,9X,F7.2))                 00003990
GO TO 110                           00004000
115 IEND = MOD52                     00004010
GO TO 105                          00004020
100 WRITE(6,135)NTRJ,ISITE,SC1,SC2,(TIME2+(I/I01)*OUTINC, 00004030
*OUTRAD(J),J=I,I+I011),I=ISTART,IEND,I01           00004040
135 FORMAT(1H1,10X,36HRADAR PARAMETERS, TRAJECTORY NUMBER,I4,3X,10HRA 00004050
*DAR SITE,I4,F12.3," DEG,LAT.",F12.3," DEG,LONG." //3X,"TIME",2X,8H00004060
*SL-RANGE,1X,11HSL-RANGE-RT,1X,9HELEVATION,4X,7HEL-RATE,1X,7HAZIMUT00004070
*M,5X,7HAZ-RATE,2X,6HRADIUS,1X,7HINR-PHI,1X,7HSL-RTRT,4X,7HEL-RTRT,00004080
*4X,7HAZ-RTRT,1X,7HREENTRY,1X,7HHEADING/2X,5H(MIN),5X,4H(NM),5X,6H(00004090
*FT/S),5X,5H(DEG),6X,7H(DEG/S),2X,5H(DEG),6X,7H(DEG/S),3X,5H(ERU),200004100
*X,5H(DEG),1X,8H(FT/S/S),2X,9H(DEG/S/S),2X,9H(DEG/S/S),2X,5H(DEG),300004110
*X,5H(DEG)/(1X,F6.2,1X,E9.3,1X,E11.4,3X,F7.2,1X,E10.3,1X,F7.2,1X,E10.3,1X,F7.2,1X,F7.2)) 00004120
*1.4,1X,F7.3,1X,F7.2,1X,F7.3,1X,E10.3,1X,E10.3,1X,F7.2,1X,F7.2) 00004130
GO TO 110                           00004140
00004150
C PRINT OUT FIRST,SECOND AND FOLLOWING TIME POINTS 00004160
150 IF(SWITCH)GO TO 145             00004170
GO TO 160                          00004180
145 IF(NPAGE.EQ.1)GO TO 165         00004190
195 IF(IOUT2)GO TO 17               00004200
WRITE(6,125)NTRJ,ISITE,SC1,SC2,TIME2,(OUTRAD(J),J=1,I01) 00004210
ISTR = ISTART + I01                 00004220
WRITE(6,175)(TIME4+((I-I01)/I01)*OUTINC,(OUTRAD(J),J=I,I+I011),I= 00004230
*ISTR,IEND,I01)                   00004240
175 FORMAT(2X,F7.2,2X,E13.6,4X,E13.6,5X,F7.2,3X,E11.4,4X,F7.2,2X,E11.4,400004250
*,3X,F7.3,9X,F7.2)                 00004260
IF(SWTCHR)WRITE(6,175)TIME6,(OUTRAD(J),J=IEND+1,IEND+I01) 00004270
190 TIME2 = TIME4 - OUTINC        00004280
GO TO 110                           00004290
00004300

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170 WRITE(6,135)NTRJ,ISITE,SC1,SC2,TIME2,(OUTRAD(J),J=1,I01) 00004310
  ISTART = ISTART + I01 00004320
  WRITE(6,185)(TIME2+(I-I01)/I01)*OUTINC,(OUTRAD(J),J=I,I+I01),I= 00004330
  *ISTART,IEND,I01) 00004340
185 FORMAT(1X,F6.2,1X,E9.3,1X,E11.4,3X,F7.2,1X,E10.3,1X,F7.2,1X,E11.4) 00004350
  *1X,F7.3,1X,F7.2,1X,E10.3,1X,E10.3,1X,F7.2,1X,F7.2) 00004360
  IF(SWTCR)WRITE(6,185)TIME6,(OUTRAD(J),J=IEND+1,IEND+I01) 00004370
  GO TO 190 00004380
165 IF(NREC6.NE.3)GO TO 196 00004390
  SWTCR = .TRUE. 00004400
  IEND = IEND - I01 00004410
  IF(MOD52.NE.0)IEND=MOD52-I01 00004420
  GO TO 195 00004430
196 IF(MOD52.NE.0)IEND=MOD52 00004432
  GO TO 195 00004434
  00004440
C   PRINT OUT LAST TIME POINT 00004450
155 IF(NREC6.NE.3)GO TO 200 00004460
  IF(MOD52.EQ.0)GO TO 205 00004470
  IF(NPAGE.EQ.1)GO TO 210 00004480
  IEND = ISTART + 1 + MOD52 - I01 00004490
230 IF(IOUT2)GO TO 22 00004500
  IF(IEND.LE.ISTART)GO TO 215 00004510
  WRITE(6,125)NTRJ,ISITE,SC1,SC2,(TIME2+(I/I01)*OUTINC, 00004520
  *(OUTRAD(J),J=I,I+I01),I=ISTART,IEND,I01) 00004530
  WRITE(6,175)TIME6,(OUTRAD(J),J=IEND+1,IEND+I01) 00004540
  GO TO 110 00004550
215 WRITE(6,125)NTRJ,ISITE,SC1,SC2,TIME6,(OUTRAD(J),J= 00004560
  *ISTART,ISTART+I01) 00004570
  GO TO 110 00004580
220 IF(IEND.LE.ISTART)GO TO 225 00004590
  WRITE(6,135)NTRJ,ISITE,SC1,SC2,(TIME2+(I/I01)*OUTINC, 00004600
  *(OUTRAD(J),J=I,I+I01),I=ISTART,IEND,I01) 00004610
  WRITE(6,185)TIME6,(OUTRAD(J),J=IEND+1,IEND+I01) 00004620
  GO TO 110 00004630
225 WRITE(6,135)NTRJ,ISITE,SC1,SC2,TIME6,(OUTRAD(J),J= 00004640
  *ISTART,ISTART+I01) 00004650
  GO TO 110 00004660
205 IEND = IEND - I01 00004670
  GO TO 230 00004680
210 IEND = MOD52 - I01 00004690
  GO TO 230 00004700
110 CONTINUE 00004710
  SWTCR = .FALSE. 00004720
  SWTCR = .FALSE. 00004730
  TIME2 = TIME2 + (IEND/I01)*OUTINC 00004740
  GO TO 8 00004750
300 REWIND 8 00004760
  RETURN 00004770
  ENTRY NOTVIS 00004780
  WRITE(6,25)NTRJ,ISITE,SC1,SC2 00004790
250 FORMAT(1H1///10X,"OBJECT NOT VISIBLE TO RADAR"//10X, 00004800

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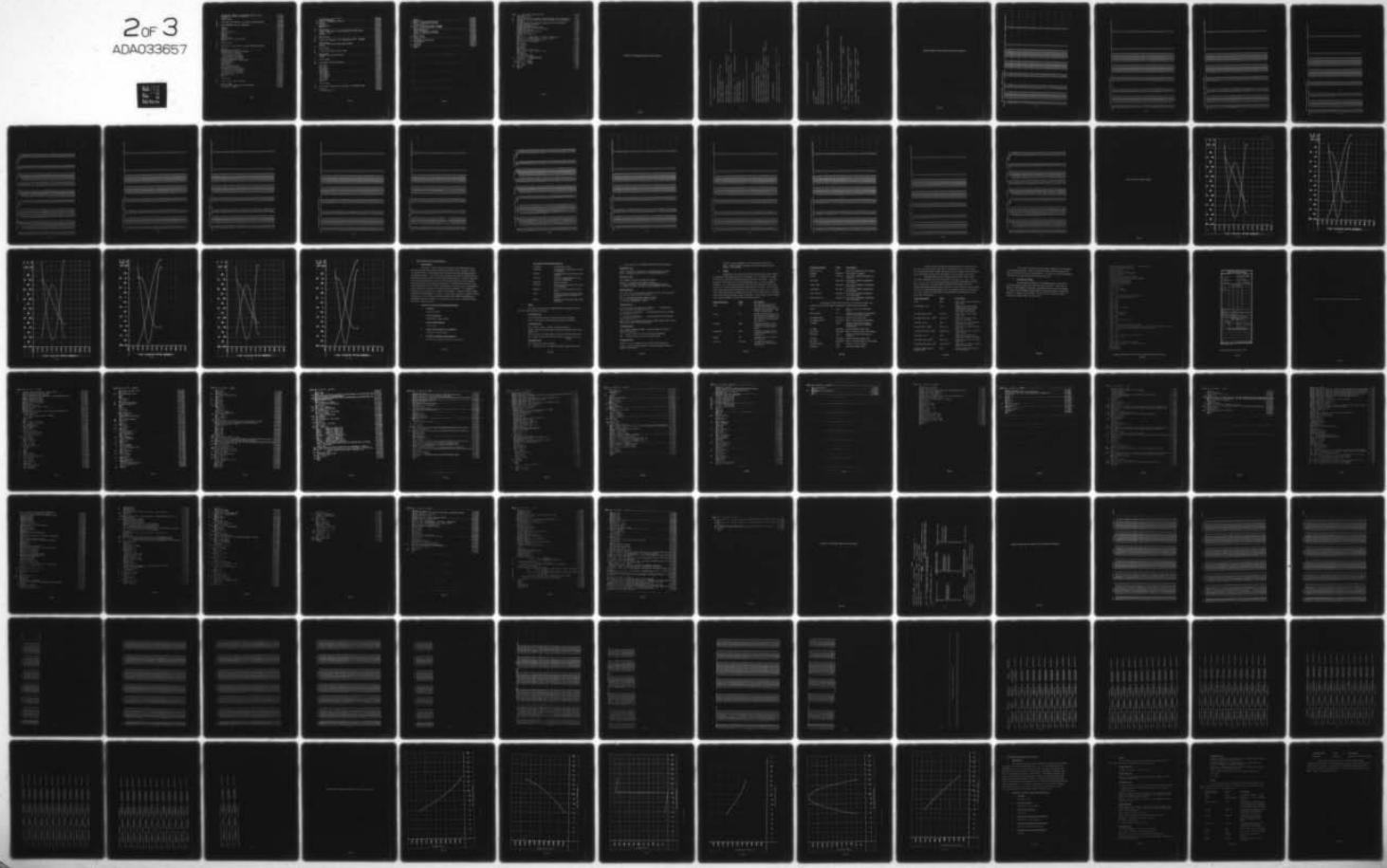
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SPACE SURVEILLANCE SOFTWARE SUPPORT. VOLUME 1, PART 1, BOOK 1, --ETC(U)  
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2 OF 3  
AD-A033657



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*TRAJECTORY NUMBER",I4,SX,"RADAR SITE",I4,F12.3,          00004810
* DEG.LAT.,I12.3, DEG.LONG. ) 00004820
  RETURN 00004830
  ENTRY PLTAP 00004840
C   GENERATE DATA TAPE/FILE FOR INPUT TO PLOT PROGRAMS 00004850
C   INITIALIZE FOR PLOT TAPE/FILE 00004860
C
C   TIME3=T 00004870
C   ISTORE3=1 00004880
C   IO2=8 00004890
C   IF(IPLOT2)IO2=13 00004900
C   NREC3=0 00004910
C   NREC4=0 00004920
C   NREC5=0 00004930
C   EOF=.FALSE. 00004940
C   WRITE(10)TIME3,IPLOT2,IO2,EOF 00004950
C   RETURN 00004960
C
C   ENTRY STORTP 00004970
C   TEMPORARILY STORE RADAR DATA FROM MISSILE/SATELLITE 00004980
C
C   TIME7=T 00004990
C   OUTPLT(ISTORE3)=RS*F6.80 00005000
C   OUTPLT(ISTORE3+1)=RSD*0.016666667 00005010
C   OUTPLT(ISTORE3+2)=EL*RTD 00005020
C   OUTPLT(ISTORE3+3)=ELD*RTD6 00005030
C   OUTPLT(ISTORE3+4)=SIG*RTD 00005040
C   OUTPLT(ISTORE3+5)=SIGD*RTD6 00005050
C   OUTPLT(ISTORE3+6)=X(1)*PERU 00005060
C   OUTPLT(ISTORE3+7)=X(3)*RTD-GLAMS 00005070
C   ISTORE3=ISTORE3+8 00005080
C   NREC3=NREC3+1 00005090
C   NREC4=NREC4+1 00005100
C   IF(.NOT.IPLOT2)RETURN 00005110
C   OUTPLT(ISTORE3)=RSD2*F36 00005120
C   OUTPLT(ISTORE3+1)=ELDD*RTD36 00005130
C   OUTPLT(ISTORE3+2)=SIGDD*RTD36 00005140
C   OUTPLT(ISTORE3+3)=REGAM*RTD 00005150
C   OUTPLT(ISTORE3+4)=HDBETA*RTD 00005160
C   ISTORE3=ISTORE3+5 00005170
C   RETURN 00005180
C
C   ENTRY PLTAP1 00005190
C   OUTPUT DATA ON PLOT TAPE/FILE 00005200
C
C   EOF10=.FALSE. 00005210
C   WRITE(10)NREC3,NREC4,NREC5,EOF10,SWTCM2 00005220
C   IF(NREC3,EQ,0)RETURN 00005230
C                                         00005240
C                                         00005250
C                                         00005260
C                                         00005270
C                                         00005280
C                                         00005290
C                                         00005300
C                                         00005310
C                                         00005320

```

```

IF(NREC3.EQ.(-1))GO TO 235          00005330
NDATA = NREC3*IO2                    00005340
WRITE(10)(OUTPLT(I),I=1,NDATA)      00005350
235 NREC3=0                          00005360
ESTOR3=1                           00005370
NREC5=NREC5+1                      00005380
RETURN                               00005390
00005400
C                                     00005410
ENTRY PLTEND                         00005420
OUTPUT LAST TIME OF MISSILE SIGHTING BY RADAR SITE 00005430
WRITE(10)TIME7                      00005440
RETURN                               00005450
00005460
C                                     00005470
ENTRY PLTAP2                         00005480
00005490
C                                     00005500
OUTPUT LAST RECORD ON PLOT TAPE/FILE FOR ONE SIGHTING 00005510
C                                     00005520
EOF10=.TRUE.                         00005530
WRITE(10)NREC3,NREC4,NREC5,EOF10,SWTCH2 00005540
RETURN                               00005550
00005560
C                                     00005570
ENTRY PLTAP3                         00005580
00005590
C                                     00005600
OUTPUT FINAL RECORD ON PLOT FILE    00005610
00005620
C                                     00005630
ENTRY STORT2                         00005640
00005650
C                                     00005660
STORE DATA FOR 2ND TRAJECTORY     00005670
00005680
XX(1)=X(1)                           00005690
XX(2)=X(2)                           00005700
XX(3)=X(3)                           00005710
XX(4)=XD(1)                          00005720
XX(5)=XD(2)                          00005730
XX(6)=XD(3)                          00005740
XX(7)=XDD(1)                         00005742
XX(8)=XDD(2)                         00005744
XX(9)=XDD(3)                         00005750
XX(10)=ZK                            00005760
XX(11)=PZ                            00005770
RETURN                               00005780
00005790
C                                     00005800
ENTRY OUTNOM                         00005810
00005820
C                                     00005830
PLACE NOMINAL TRAJECTORY RADAR DATA ON A SEPARATE FILE 00005840
C                                     00005850
ISITE =1                            00005860
IF(.NOT.KZ)GO TO 40                 00005870

```

REWIND 10	00005830
REWIND 11	00005840
440 READ(10)TIME3,IPIOT3,IO2,EOF	00005850
WRITE(11)TIME3,IPIOT2,IO2,EOF	00005860
IF(EOF)GO TO 41	00005870
430 READ(10)NREC3,ITR,IS,EOF1,SWTCN2	00005880
WRITE(11)NREC3,ITR,IS,EOF10,SWTCN2	00005890
IF(EOF10)GO TO 42	00005900
MDATA = NREC3*IO2	00005910
READ(10)(OUTPLT(I),I=1,MDATA)	00005920
WRITE(11)(OUTPLT(I),I=1,MDATA)	00005930
GO TO 430	00005940
420 READ(10)TIME7	00005950
WRITE(11)TIME7	00005960
GO TO 440	00005970
410 IF(ISITE.EQ.NSITE)RETURN	00005980
ISITE=ISITE+1	00005990
GO TO 440	00006000
400 CONTINUE	00006010
RETURN	00006015
END	00006020

```

CRKG      4TH ORDER RUNGE-KUTTA-GILL          00002170
          SUBROUTINE RKG                      00002180
C         INPUT/OUTPUT MOD 1                  00002190
C         THIS ROUTINE IS A 4TH ORDER RUNGE-KUTTA-GILL WHICH NUMERICALLY 00002200
C         INTEGRATES THE 2ND ORDER NON-LINEAR DIFFERENTIAL EQUATIONS OF 00002210
C         MOTION.                                00002220
          DOUBLE PRECISION C,F,D,A,B,DEG,DXN,DXDX,DL,SAD,ABLE,BAKER 00002230
          DOUBLE PRECISION X,XD,XDD                     00002240
          DOUBLE PRECISION P,Q                      00002250
          DOUBLE PRECISION P1,ZK,B1,TWOP1            00002260
          DIMENSION C(4), F(4), D(4), A(3),B(3)        00002270
          DOUBLE PRECISION TO                      00002280
          COMMON /BS/ X(3),XD(3),XDD(3)             00002290
          COMMON/GE/ZK,B1,P1                      00002300
          COMMON /ST/ P(3), Q(3)                   00002310
*#TO/TO
          DATA C/0.5D0,.2928932188,1.707106781,.1666666667/ 00002320
          DATA D/0.5D0,.2928932188,-.707106781,0.5D0/ 00002330
          DATA F/2.0D0,1.0D0,1.0D0,2.0D0/, 00002340
*TWOP1/6.2831853 717958648/
          DO 10 J=1,4                         00002350
          CALL EQTNX                         00002360
          DO 10 I=1,3                         00002370
          A(I)=XD(I)                         00002380
          B(I)=XDD(I)                        00002390
          BXN =(A(I)-F(J)*Q(I))*C(J)        00002400
          BXDX = (B(I) - F(J) * P(I)) * C(J) 00002410
          DL=TO*DXN                         00002420
          R(I)=X(I)+DL                      00002430
          RD(I)=XD(I)+TO*D'DX              00002440
          Q(I)=Q(I)+3. DO*DXN-D(J)*A(I)    00002450
          P(I)=P(I)+3. DO*B'DX-D(J)*B(I)   00002460
          IF(X(3)) 13,14,14                00002470
13       K(3) = X(3) +TWOP1            00002480
14       SAD = X(3) - TWOP1           00002490
          IF ( SAD ) 12,11,11           00002500
11       K(3) = SAD                 00002510
12       RETURN                         00002520
          END                               00002530
                                         00002540
                                         00002550

```

**Listing of the Sample Input for the Program**

MISSILE TRAJECTORY PROGRAM (MULTIPLE STATE/TRAJECTORY MOD) INPUTS

PROGRAM CONTROLS

NUMBER OF TRAJECTORIES SIMULATED(NTRAJ) 10

MAXIMUM TIME FOR A TRAJECTORY(TMX) 0.2000D 02 MIN.

MAIN PROCESSING SWITCH(NSWITCH) 1

PRINT-OUT OPTION 1(IOUT1) F PRINT-OUT OPTION 2(IOUT2) F

INCREMENT BETWEEN TIME POINTS FOR PRINT-OUT(TOUTINC) 0.100 MIN.

PRINT/OUT OPTION FOR RADAR PARAMETER DIFFERENCES(IOUT3) F

NOMINAL TRAJECTORY SELECTION SWITCH(KZ) T

PLOTTING OPTION 1(IPLOT1) T PLOTTING OPTION 2(IPLOT2) F

ATMOSPHERIC MODEL OPTION(KAT) F

SPHERICAL EARTH MODEL(SPHERE) T

INERTIAL VELOCITY OPTION(INERTL) T

\*\*\*\*\*

INITIAL STATE VECTOR OF THE INTERCEPT(R)

RE-ENTRY ANGLE WRT THE VERTICAL(GAM) 0.9000D 02 DEG.

HEADING ANGLE WRT RELATIVE NORTH(BETA) 0.81826D 02 DEG.

HEIGHT OF MISSILE AT BURNOUT(HX) 0.6083D 06 FT.

VELOCITY OF MISSILE RELATIVE TO BURNOUT AT EPOCH(V0) 0.2556742000D 05 FT./SEC.

GEOCENTRIC LATITUDE AT BURNOUT, +NORTH AND -SOUTH OF EQUATOR(THB)

GEOCENTRIC LONGITUDE, EAST OF GREENWICH(GLB) 0.40350D 02 DEG.

SUBSATELLITE PARAMETERS

GEOCENTRIC LATITUDE, +NORTH AND -SOUTH OF EQUATOR(THSS) -0.40350D 02 DEG.

GEOCENTRIC LONGITUDE, EAST OF GREENWICH(GLSS) 0.6000D 02 DEG.

RADAR PARAMETERS

SITE NUMBER 1

GEOCENTRIC LATITUDE OF RADAR. +NORTH AND -SOUTH OF EQUATOR(SLAT) 0.35900D 02 DEG;

GEOCENTRIC LONGITUDE OF RADAR, WEST OF GREENWICH(SLONG) 0.23333D 03 DEG.

ALTITUDE OF RADAR ABOVE SEA LEVEL(SALT) 0. FT.

MAXIMUM CO-LATITUDE OF ELEVATION ANGLE FOR WHICH COVERAGE PARAMETERS ARE DETERMINED(LIM) 0.89900D 02 DEG.

VELOCITY PERTURBATIONS

OUT OF TRAJECTORY PLANE PERTURBATION, +EJECTED TO THE LEFT OF NOMINAL TRAJECTORY(A) IN FT./SEC.

0. 0.  
0.3533 D 01 0.3533 D 01 0. 0.  
0. 0.

0.50000D 01 0.35330D 01 -0.35330D 01 0.

0.50000D 01 0.35330D 01 0.35330D 01 0.

**Sample Output for the RADC Trajectory Program**

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER I

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(FT)	VELOCITY(FT/S)	BAL. COEFF.(FT*2/SLG)	ATMOS. DENS.(SLG/FT**3)
0.	6.215342 0.8	62.75	40.35	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.10	6.215342 0.8	62.75	41.21	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.20	6.215342 0.8	62.66	42.07	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.30	6.215342 0.8	62.55	42.93	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.40	6.215342 0.8	62.44	43.80	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.50	6.215342 0.8	62.32	44.67	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.60	6.215342 0.8	62.19	45.54	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.70	6.215342 0.8	62.07	46.41	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.80	6.215342 0.8	62.95	47.28	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
0.90	6.215342 0.8	63.00	48.15	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.00	6.215342 0.8	63.0	49.93	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.10	6.215342 0.8	63.00	50.90	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.20	6.215342 0.8	62.99	50.77	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.30	6.215342 0.8	62.98	51.65	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.40	6.215342 0.8	62.96	52.52	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.50	6.215342 0.8	62.94	53.39	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.60	6.215342 0.8	62.91	54.26	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.70	6.215342 0.8	62.87	55.13	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.80	6.215342 0.8	62.83	55.99	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
1.90	6.215342 0.8	62.78	56.85	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.00	6.215342 0.8	62.73	57.71	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.10	6.215342 0.8	62.67	58.57	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.20	6.215342 0.8	62.61	59.42	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.30	6.215342 0.8	62.54	60.27	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.40	6.215342 0.8	62.47	61.12	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.50	6.215342 0.8	62.39	61.96	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.60	6.215342 0.8	62.3	62.79	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.70	6.215342 0.8	62.21	63.62	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.80	6.215342 0.8	62.12	64.45	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
2.90	6.215342 0.8	62.02	65.27	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.00	6.215342 0.8	61.91	66.08	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.10	6.215342 0.8	61.80	66.89	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.20	6.215342 0.8	61.69	67.69	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.30	6.215342 0.8	61.57	68.48	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.40	6.215342 0.8	61.44	69.27	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.50	6.215342 0.8	61.31	70.06	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.60	6.215342 0.8	61.17	70.83	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.70	6.215342 0.8	61.03	71.60	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.80	6.215342 0.8	59.97	72.36	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
3.90	6.215342 0.8	59.94	73.12	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.00	6.215342 0.8	59.91	73.86	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.10	6.215342 0.8	59.83	74.60	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.20	6.215342 0.8	59.72	75.33	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.30	6.215342 0.8	59.60	76.06	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.40	6.215342 0.8	59.53	76.78	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.50	6.215342 0.8	59.46	77.49	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.60	6.215342 0.8	59.38	78.19	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.70	6.215342 0.8	59.30	78.88	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.80	6.215342 0.8	59.21	79.57	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
4.90	6.215342 0.8	59.12	80.24	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
5.00	6.215342 0.8	58.82	80.91	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05
5.10	6.215342 0.8	58.63	81.58	0.60803E 06	0.25567E 05	0.60803E 06	0.40000E 05

## TRAJECTORY PARAMETERS • TRAJECTORY NUMBER

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	TRAJECTORY NUMBER	HEIGHT(FT)	VELOCITY(FT/S)	BAL COEFF.(FT**2/SIG)	ATMOS/DENS,(SIG/FT**3)
5.20	58.42	58.42	58.42	58.42	32.23	0.60803E 06	0.255674E 05	0.0
5.30	58.22	58.22	58.22	58.22	82.88	0.60803E 06	0.255674E 05	0.0
5.40	58.01	58.01	58.01	58.01	83.52	0.60803E 06	0.255674E 05	0.0
5.50	57.80	57.80	57.80	57.80	84.15	0.60803E 06	0.255674E 05	0.0
5.60	57.56	57.56	57.56	57.56	84.77	0.60803E 06	0.255674E 05	0.0
5.70	57.36	57.36	57.36	57.36	85.39	0.60803E 06	0.255674E 05	0.0
5.80	57.14	57.14	57.14	57.14	86.00	0.60803E 06	0.255674E 05	0.0
5.90	56.92	56.92	56.92	56.92	86.60	0.60803E 06	0.255674E 05	0.0
6.00	56.69	56.69	56.69	56.69	87.19	0.60803E 06	0.255674E 05	0.0
6.10	56.46	56.46	56.46	56.46	87.78	0.60803E 06	0.255674E 05	0.0
6.20	56.22	56.22	56.22	56.22	88.35	0.60803E 06	0.255674E 05	0.0
6.30	55.99	55.99	55.99	55.99	88.93	0.60803E 06	0.255674E 05	0.0
6.40	55.75	55.75	55.75	55.75	89.49	0.60803E 06	0.255674E 05	0.0
6.50	55.50	55.50	55.50	55.50	90.04	0.60803E 06	0.255674E 05	0.0
6.60	55.26	55.26	55.26	55.26	90.59	0.60803E 06	0.255674E 05	0.0
6.70	55.01	55.01	55.01	55.01	91.14	0.60803E 06	0.255674E 05	0.0
6.80	54.76	54.76	54.76	54.76	91.67	0.60803E 06	0.255674E 05	0.0
6.90	54.51	54.51	54.51	54.51	92.20	0.60803E 06	0.255674E 05	0.0
7.00	54.25	54.25	54.25	54.25	92.72	0.60803E 06	0.255674E 05	0.0
7.10	53.99	53.99	53.99	53.99	93.23	0.60803E 06	0.255674E 05	0.0
7.20	53.73	53.73	53.73	53.73	93.74	0.60803E 06	0.255674E 05	0.0
7.30	53.47	53.47	53.47	53.47	94.24	0.60803E 06	0.255674E 05	0.0
7.40	53.20	53.20	53.20	53.20	94.74	0.60803E 06	0.255674E 05	0.0
7.50	52.94	52.94	52.94	52.94	95.23	0.60803E 06	0.255674E 05	0.0
7.60	52.67	52.67	52.67	52.67	95.71	0.60803E 06	0.255674E 05	0.0
7.70	52.40	52.40	52.40	52.40	96.18	0.60803E 06	0.255674E 05	0.0
7.80	52.12	52.12	52.12	52.12	96.65	0.60803E 06	0.255674E 05	0.0
7.90	51.85	51.85	51.85	51.85	97.12	0.60803E 06	0.255674E 05	0.0
8.00	51.57	51.57	51.57	51.57	97.57	0.60803E 06	0.255674E 05	0.0
8.10	51.29	51.29	51.29	51.29	98.03	0.60803E 06	0.255674E 05	0.0
8.20	51.01	51.01	51.01	51.01	98.47	0.60803E 06	0.255674E 05	0.0
8.30	50.72	50.72	50.72	50.72	98.91	0.60803E 06	0.255674E 05	0.0
8.40	50.44	50.44	50.44	50.44	99.35	0.60803E 06	0.255674E 05	0.0
8.50	50.15	50.15	50.15	50.15	99.78	0.60803E 06	0.255674E 05	0.0
8.60	49.86	49.86	49.86	49.86	100.20	0.60803E 06	0.255674E 05	0.0
8.70	49.57	49.57	49.57	49.57	100.62	0.60803E 06	0.255674E 05	0.0
8.80	49.28	49.28	49.28	49.28	101.03	0.60803E 06	0.255674E 05	0.0
8.90	48.99	48.99	48.99	48.99	101.44	0.60803E 06	0.255674E 05	0.0
9.00	48.69	48.69	48.69	48.69	101.84	0.60803E 06	0.255674E 05	0.0
9.10	48.39	48.39	48.39	48.39	102.24	0.60803E 06	0.255674E 05	0.0
9.20	48.08	48.08	48.08	48.08	102.63	0.60803E 06	0.255674E 05	0.0
9.30	47.79	47.79	47.79	47.79	103.02	0.60803E 06	0.255674E 05	0.0
9.40	47.49	47.49	47.49	47.49	103.40	0.60803E 06	0.255674E 05	0.0
9.50	47.19	47.19	47.19	47.19	103.78	0.60803E 06	0.255674E 05	0.0
9.60	46.88	46.88	46.88	46.88	104.15	0.60803E 06	0.255674E 05	0.0
9.70	46.58	46.58	46.58	46.58	104.52	0.60803E 06	0.255674E 05	0.0
9.80	46.27	46.27	46.27	46.27	104.89	0.60803E 06	0.255674E 05	0.0
9.90	45.96	45.96	45.96	45.96	105.25	0.60803E 06	0.255674E 05	0.0
10.00	45.65	45.65	45.65	45.65	105.61	0.60803E 06	0.255674E 05	0.0
10.10	45.34	45.34	45.34	45.34	105.96	0.60803E 06	0.255674E 05	0.0
10.20	45.03	45.03	45.03	45.03	106.31	0.60803E 06	0.255674E 05	0.0
10.30	44.72	44.72	44.72	44.72	106.65	0.60803E 06	0.255674E 05	0.0

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER 1

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(FT)	VELOCITY(FT/S)	BAL.CORR.(FT/R/SIG)	ATMOS.DRAG.(SIG/RT•••)
10.40	215342	44.4	106.99	0.6084E 06	0.255674E 05		
10.50	215342	44.09	107.33	0.6084E 06	0.255674E 05		
10.60	215342	43.77	107.66	0.6084E 06	0.255674E 05		
10.70	215342	43.45	107.99	0.6084E 06	0.255674E 05		
10.80	215342	43.13	108.31	0.6084E 06	0.255674E 05		
10.90	215342	42.81	108.63	0.6084E 06	0.255674E 05		
11.00	215342	42.49	108.95	0.6084E 06	0.255674E 05		
11.10	215342	42.17	109.26	0.6084E 06	0.255674E 05		
11.20	215342	41.85	109.57	0.6084E 06	0.255674E 05		
11.30	215342	41.52	109.88	0.6084E 06	0.255674E 05		
11.40	215342	41.20	110.19	0.6084E 06	0.255674E 05		
11.50	215342	40.87	110.49	0.6084E 06	0.255674E 05		
11.60	215342	40.54	110.78	0.6084E 06	0.255674E 05		
11.70	215342	40.22	111.08	0.6084E 06	0.255674E 05		
11.80	215342	39.89	111.37	0.6084E 06	0.255674E 05		
11.90	215342	39.56	111.66	0.6084E 06	0.255674E 05		
12.00	215342	39.23	111.94	0.6084E 06	0.255674E 05		
12.10	215342	38.90	112.22	0.6084E 06	0.255674E 05		
12.20	215342	38.57	112.50	0.6084E 06	0.255674E 05		
12.30	215342	38.23	112.78	0.6084E 06	0.255674E 05		
12.40	215342	37.90	113.05	0.6084E 06	0.255674E 05		
12.50	215342	37.56	113.33	0.6084E 06	0.255674E 05		
12.60	215342	37.23	113.59	0.6084E 06	0.255674E 05		
12.70	215342	36.89	113.86	0.6084E 06	0.255674E 05		
12.80	215342	36.56	114.12	0.6084E 06	0.255674E 05		
12.90	215342	36.22	114.38	0.6084E 06	0.255674E 05		
13.00	215342	35.88	114.64	0.6084E 06	0.255674E 05		
13.10	215342	35.54	114.90	0.6084E 06	0.255674E 05		
13.20	215342	35.21	115.15	0.6084E 06	0.255674E 05		
13.30	215342	34.87	115.40	0.6084E 06	0.255674E 05		
13.40	215342	34.53	115.65	0.6084E 06	0.255674E 05		
13.50	215342	34.18	115.90	0.6084E 06	0.255674E 05		
13.60	215342	33.84	116.14	0.6084E 06	0.255674E 05		
13.70	215342	33.50	116.39	0.6084E 06	0.255674E 05		
13.80	215342	33.16	116.63	0.6084E 06	0.255674E 05		
13.90	215342	32.82	116.87	0.6084E 06	0.255674E 05		
14.00	215342	32.47	117.10	0.6084E 06	0.255674E 05		
14.10	215342	32.13	117.34	0.6084E 06	0.255674E 05		
14.20	215342	31.78	117.57	0.6084E 06	0.255674E 05		
14.30	215342	31.44	117.80	0.6084E 06	0.255674E 05		
14.40	215342	31.09	118.03	0.6084E 06	0.255674E 05		
14.50	215342	30.74	118.25	0.6084E 06	0.255674E 05		
14.60	215342	30.40	118.48	0.6084E 06	0.255674E 05		
14.70	215342	30.05	118.70	0.6084E 06	0.255674E 05		
14.80	215342	29.7	118.92	0.6084E 06	0.255674E 05		
14.90	215342	29.35	119.14	0.6084E 06	0.255674E 05		
15.00	215342	29.01	119.36	0.6084E 06	0.255674E 05		
15.10	215342	28.66	119.58	0.6084E 06	0.255674E 05		
15.20	215342	28.31	119.79	0.6084E 06	0.255674E 05		
15.30	215342	27.96	120.01	0.6084E 06	0.255674E 05		
15.40	215342	27.61	120.22	0.6084E 06	0.255674E 05		
15.50	215342	27.26	120.43	0.6084E 06	0.255674E 05		

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(FT)	VELOCITY(FT/S)	BAL.COEFT.(FT*2/SLG)	ATMOS.DENS.(SIG/FT*3)
15.60	• 21534E 0 8	26. 91	120. 64	0.6804E 0 6	0.2557E 0 5	0	0
15.70	• 21534E 0 8	26. 55	120. 84	0.6804E 0 6	0.2557E 0 5	0	0
15.80	• 21534E 0 8	26. 2	121. 05	0.6804E 0 6	0.2557E 0 5	0	0
15.90	• 21534E 0 8	25. 85	121. 25	0.6804E 0 6	0.2557E 0 5	0	0
16.00	• 21534E 0 8	25. 5	121. 46	0.6804E 0 6	0.2557E 0 5	0	0
16.10	• 21534E 0 8	25. 14	121. 66	0.6804E 0 6	0.2557E 0 5	0	0
16.60	• 21534E 0 8	24. 79	121. 86	0.6804E 0 6	0.2557E 0 5	0	0
16.70	• 21534E 0 8	24. 44	122. 06	0.6804E 0 6	0.2557E 0 5	0	0
16.80	• 21534E 0 8	24. 08	122. 26	0.6804E 0 6	0.2557E 0 5	0	0
16.90	• 21534E 0 8	23. 73	122. 45	0.6804E 0 6	0.2557E 0 5	0	0
17.00	• 21534E 0 8	23. 37	122. 65	0.6804E 0 6	0.2557E 0 5	0	0
17.10	• 21534E 0 8	23. 02	122. 84	0.6804E 0 6	0.2557E 0 5	0	0
17.20	• 21534E 0 8	22. 66	123. 04	0.6805E 0 6	0.2557E 0 5	0	0
17.30	• 21534E 0 8	22. 31	123. 23	0.6805E 0 6	0.2557E 0 5	0	0
17.40	• 21534E 0 8	21. 95	123. 42	0.6805E 0 6	0.2557E 0 5	0	0
17.50	• 21534E 0 8	21. 60	123. 61	0.6805E 0 6	0.2557E 0 5	0	0
17.60	• 21534E 0 8	21. 24	123. 80	0.6805E 0 6	0.2557E 0 5	0	0
17.70	• 21534E 0 8	20. 88	123. 98	0.6805E 0 6	0.2557E 0 5	0	0
17.80	• 21534E 0 8	20. 53	124. 17	0.6805E 0 6	0.2557E 0 5	0	0
17.90	• 21534E 0 8	20. 17	124. 36	0.6805E 0 6	0.2557E 0 5	0	0
18.00	• 21534E 0 8	19. 81	124. 54	0.6805E 0 6	0.2557E 0 5	0	0
18.10	• 21534E 0 8	19. 45	124. 73	0.6805E 0 6	0.2557E 0 5	0	0
18.20	• 21534E 0 8	19. 1	124. 91	0.6805E 0 6	0.2557E 0 5	0	0
18.30	• 21534E 0 8	18. 74	125. 09	0.6805E 0 6	0.2557E 0 5	0	0
18.40	• 21534E 0 8	18. 38	125. 27	0.6805E 0 6	0.2557E 0 5	0	0
18.50	• 21534E 0 8	18. 02	125. 45	0.6805E 0 6	0.2557E 0 5	0	0
18.60	• 21534E 0 8	17. 66	125. 63	0.6805E 0 6	0.2557E 0 5	0	0
18.70	• 21534E 0 8	17. 30	125. 81	0.6805E 0 6	0.2557E 0 5	0	0
18.80	• 21534E 0 8	16. 95	125. 99	0.6805E 0 6	0.2557E 0 5	0	0
18.90	• 21534E 0 8	16. 59	126. 17	0.6805E 0 6	0.2557E 0 5	0	0
18.50	• 21534E 0 8	16. 23	126. 34	0.6805E 0 6	0.2557E 0 5	0	0
18.60	• 21534E 0 8	15. 87	126. 52	0.6805E 0 6	0.2557E 0 5	0	0
18.70	• 21534E 0 8	15. 51	126. 69	0.6805E 0 6	0.2557E 0 5	0	0
18.80	• 21534E 0 8	15. 15	126. 87	0.6805E 0 6	0.2557E 0 5	0	0
18.90	• 21534E 0 8	14. 79	127. 04	0.6805E 0 6	0.2557E 0 5	0	0
19.00	• 21534E 0 8	14. 43	127. 21	0.6805E 0 6	0.2557E 0 5	0	0
19.10	• 21534E 0 8	14. 07	127. 38	0.6805E 0 6	0.2557E 0 5	0	0
19.20	• 21534E 0 8	13. 70	127. 56	0.6805E 0 6	0.2557E 0 5	0	0
19.30	• 21534E 0 8	13. 34	127. 73	0.6805E 0 6	0.2557E 0 5	0	0
19.40	• 21534E 0 8	12. 98	127. 90	0.6805E 0 6	0.2557E 0 5	0	0
19.50	• 21534E 0 8	12. 62	128. 07	0.6805E 0 6	0.2557E 0 5	0	0
19.60	• 21534E 0 8	12. 26	128. 24	0.6805E 0 6	0.2557E 0 5	0	0
19.70	• 21534E 0 8	11. 9	128. 41	0.6805E 0 6	0.2557E 0 5	0	0
19.80	• 21534E 0 8	11. 54	128. 57	0.6805E 0 6	0.2557E 0 5	0	0
19.90	• 21534E 0 8	11. 17	128. 74	0.6805E 0 6	0.2557E 0 5	0	0
20.00	• 21534E 0 8						

## RADAR PARAMETERS , TRAJECTORY NUMBER 1 RADAR SITE 1 35.900 DEG.LAT. 233.333 DEG.LONG.

TIME (MEN)	SL RANGE (NM)	SL RANGE-RATE (FT/SEC)	ELEVATION (DEG)	EL RATE (DEG/S)	AZIMUTH (DEG)	AZ RATE (DEG/S)	RADIUS (KRY)	INERTIAL PHI (DEG)
11.90	0.761123	-0.174541E+05	1.30	0.52722E-01	291.64	-0.21342E+00	1.929	51.66
12.00	0.743974E+03	-0.170559E+05	1.62	0.52862E-01	290.34	-0.22332E+00	1.929	51.84
12.10	0.727374E+03	-0.166477E+05	1.94	0.52912E-01	288.97	-0.23322E+00	1.929	52.22
12.20	0.711130E+03	-0.162420E+05	2.26	0.52852E-01	287.53	-0.24412E+00	1.929	52.50
12.30	0.695377E+03	-0.157212E+05	2.57	0.52662E-01	286.03	-0.25612E+00	1.929	52.78
12.40	0.680113E+03	-0.152089E+05	2.89	0.52322E-01	284.46	-0.26812E+00	1.929	53.05
12.50	0.665372E+03	-0.146591E+05	3.10	0.51812E-01	282.81	-0.28042E+00	1.929	53.33
12.60	0.651193E+03	-0.141047E+05	3.51	0.51092E-01	281.9	-0.29302E+00	1.929	53.59
12.70	0.637611E+03	-0.134442E+05	3.81	0.50142E-01	279.3	-0.30592E+00	1.929	53.86
12.80	0.624667E+03	-0.127795E+05	4.11	0.48932E-01	277.42	-0.31912E+00	1.929	54.12
12.90	0.612442E+03	-0.120742E+05	4.40	0.47442E-01	275.47	-0.33212E+00	1.929	54.38
13.00	0.600858E+03	-0.113161E+05	4.68	0.45622E-01	273.43	-0.35562E+00	1.929	54.64
13.10	0.590778E+03	-0.105222E+05	4.95	0.43622E-01	271.32	-0.35872E+00	1.929	54.90
13.20	0.580195E+03	-0.968219E+04	5.20	0.40942E-01	269.13	-0.37152E+00	1.929	55.15
13.30	0.570981E+03	-0.880665E+04	5.44	0.38032E-01	266.86	-0.38392E+00	1.929	55.40
13.40	0.562749E+03	-0.787661E+04	5.66	0.34732E-01	264.52	-0.39562E+00	1.929	55.65
13.50	0.555446E+03	-0.691305E+04	5.85	0.31052E-01	262.12	-0.40682E+00	1.929	55.90
13.60	0.549116E+03	-0.591189E+04	6.03	0.27002E-01	259.65	-0.41642E+00	1.929	56.14
13.70	0.543787E+03	-0.498146E+04	6.18	0.22602E-01	257.13	-0.42462E+00	1.929	56.39
13.80	0.539491E+03	-0.382156E+04	6.30	0.178942E-01	254.56	-0.43172E+00	1.929	56.63
13.90	0.536252E+03	-0.273892E+04	6.39	0.12942E-01	251.95	-0.43742E+00	1.929	56.87
14.00	0.534090E+03	-0.162915E+04	6.45	0.77912E-02	249.32	-0.44602E+00	1.929	57.10
14.10	0.533019E+03	-0.530454E+03	6.48	0.25282E-02	246.6	-0.44282E+00	1.929	57.34
14.20	0.530446E+03	-0.581810E+03	6.48	0.27722E-02	244.01	-0.44282E+00	1.929	57.57
14.30	0.534165E+03	-0.169061E+04	6.45	0.80302E-02	241.36	-0.45602E+00	1.929	57.80
14.40	0.536327E+03	-0.278866E+04	6.39	0.13172E-01	238.72	-0.45692E+00	1.929	58.03
14.50	0.539665E+03	-0.387162E+04	6.39	0.18112E-01	236.12	-0.45312E+00	1.929	58.25
14.60	0.544009E+03	-0.492851E+04	6.17	0.22802E-01	233.55	-0.42432E+00	1.929	58.48
14.70	0.549383E+03	-0.595851E+04	6.02	0.271182E-01	231.03	-0.41562E+00	1.929	58.70
14.80	0.555758E+03	-0.695550E+04	5.84	0.31222E-01	228.56	-0.40602E+00	1.929	58.92
14.90	0.563992E+03	-0.791638E+04	5.65	0.34882E-01	226.16	-0.39542E+00	1.929	59.14
15.00	0.571369E+03	-0.883749E+04	5.43	0.38152E-01	223.82	-0.38382E+00	1.929	59.36
15.10	0.585268E+03	-0.971675E+04	5.19	0.41042E-01	221.56	-0.37142E+00	1.929	59.58
15.20	0.590533E+03	-0.105531E+05	4.93	0.43542E-01	219.37	-0.35832E+00	1.929	59.79
15.30	0.601342E+03	-0.113458E+05	4.67	0.45682E-01	217.6	-0.34522E+00	1.929	60.01
15.40	0.612912E+03	-0.120942E+05	4.39	0.47482E-01	215.23	-0.33912E+00	1.929	60.22
15.50	0.625199E+03	-0.128092E+05	4.10	0.48962E-01	213.28	-0.31872E+00	1.929	60.43
15.60	0.638163E+03	-0.134647E+05	3.80	0.51092E-01	211.41	-0.30562E+00	1.929	60.64
15.70	0.651761E+03	-0.140875E+05	3.50	0.52662E-01	209.61	-0.29272E+00	1.929	60.84
15.80	0.665954E+03	-0.146712E+05	3.19	0.51792E-01	207.89	-0.28042E+00	1.929	61.05
15.90	0.684752E+03	-0.152172E+05	2.18	0.52302E-01	206.5	-0.26792E+00	1.929	61.25
16.00	0.695977E+03	-0.157275E+05	2.56	0.52632E-01	204.68	-0.25602E+00	1.929	61.46
16.10	0.711735E+03	-0.162005E+05	2.24	0.52812E-01	203.18	-0.24462E+00	1.929	61.66
16.20	0.727948E+03	-0.166465E+05	1.93	0.52862E-01	201.74	-0.23372E+00	1.929	61.86
16.30	0.744584E+03	-0.170632E+05	1.29	0.52672E-01	199.06	-0.22322E+00	1.929	62.06
16.40	0.761616E+03	-0.174439E+05	1.29	0.52672E-01	199.06	-0.21322E+00	1.929	62.26

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER 4

TIME (MIN)	RADIUS (FT)	LATITUDE (DEG)	LONGITUDE (DEG)	HEIGHT (FT)	VELOCITY (FT/S)	BAL. COEFF. (PT. #/SLG)	ATMOS. DENS. (SIG/PT. #)
0.	*21534E 08	62.7	40.35	0.60093E 06	0.255574E 05	0.	0.
0.10	*21534E 08	62.76	41.21	0.60086E 06	0.255674E 05	0.	0.
0.20	*21534E 08	62.8	42.07	0.60092E 06	0.255574E 05	0.	0.
0.30	*21534E 08	62.85	42.93	0.60082E 06	0.255673E 05	0.	0.
0.40	*21534E 08	62.89	43.80	0.60085E 06	0.255673E 05	0.	0.
0.50	*21534E 08	62.92	44.67	0.60081E 06	0.255672E 05	0.	0.
0.60	*21534E 08	62.95	45.54	0.60021E 06	0.255672E 05	0.	0.
0.70	*21534E 08	62.97	46.41	0.60082E 06	0.255672E 05	0.	0.
0.80	*21534E 08	62.99	47.28	0.60027E 06	0.255671E 05	0.	0.
0.90	*21534E 08	63.00	48.15	0.600830E 06	0.255671E 05	0.	0.
1.00	*21534E 08	63.0	49.03	0.60033E 06	0.255671E 05	0.	0.
1.10	*21534E 08	63.0	49.90	0.60036E 06	0.2556702E 05	0.	0.
1.20	*21534E 08	62.99	50.77	0.600839E 06	0.2556702E 05	0.	0.
1.30	*21534E 08	62.98	51.65	0.600842E 06	0.2556702E 05	0.	0.
1.40	*21534E 08	62.96	52.52	0.600845E 06	0.2556692E 05	0.	0.
1.50	*21534E 08	62.94	53.39	0.600848E 06	0.2556692E 05	0.	0.
1.60	*21534E 08	62.91	54.26	0.600851E 06	0.2556692E 05	0.	0.
1.70	*21534E 08	62.87	55.13	0.60054E 06	0.2556682E 05	0.	0.
1.80	*21534E 08	62.83	55.99	0.600857E 06	0.2556682E 05	0.	0.
1.90	*21534E 08	62.78	56.85	0.60060E 06	0.2556672E 05	0.	0.
2.00	*21534E 08	62.73	57.71	0.600863E 06	0.2556672E 05	0.	0.
2.10	*21534E 08	62.67	58.57	0.60066E 06	0.2556672E 05	0.	0.
2.20	*21534E 08	62.61	59.42	0.600692E 06	0.2556662E 05	0.	0.
2.30	*21534E 08	62.54	60.27	0.60072E 06	0.2556662E 05	0.	0.
2.40	*21534E 08	62.47	61.11	0.60074E 06	0.2556662E 05	0.	0.
2.50	*21534E 08	62.39	61.95	0.600877E 06	0.2556652E 05	0.	0.
2.60	*21534E 08	62.3	62.79	0.60080E 06	0.2556652E 05	0.	0.
2.70	*21534E 08	62.21	63.62	0.60083E 06	0.2556652E 05	0.	0.
2.80	*21534E 08	62.12	64.45	0.60086E 06	0.255664E 05	0.	0.
2.90	*21535E 08	62.02	65.26	0.60089E 06	0.255664E 05	0.	0.
3.00	*21535E 08	61.9	66.08	0.60092E 06	0.255664E 05	0.	0.
3.10	*21535E 08	61.8C	66.89	0.600895E 06	0.255663E 05	0.	0.
3.20	*21535E 08	61.69	67.69	0.60098E 06	0.255663E 05	0.	0.
3.30	*21535E 08	61.57	68.48	0.60091E 06	0.255663E 05	0.	0.
3.40	*21535E 08	61.44	69.27	0.60094E 06	0.255662E 05	0.	0.
3.50	*21535E 08	61.31	70.05	0.60097E 06	0.255662E 05	0.	0.
3.60	*21535E 08	61.17	70.83	0.60010E 06	0.255662E 05	0.	0.
3.70	*21535E 08	60.94	75.33	0.60027E 06	0.255559E 05	0.	0.
3.80	*21535E 08	60.89	71.60	0.60013E 06	0.255661E 05	0.	0.
3.90	*21535E 08	60.74	72.36	0.60016E 06	0.255559E 05	0.	0.
4.00	*21535E 08	60.59	73.11	0.60018E 06	0.255660E 05	0.	0.
4.10	*21535E 08	60.43	73.86	0.60021E 06	0.255660E 05	0.	0.
4.20	*21535E 08	60.27	74.60	0.60024E 06	0.255660E 05	0.	0.
4.30	*21535E 08	60.1C	75.33	0.60027E 06	0.255559E 05	0.	0.
4.40	*21535E 08	59.93	76.06	0.60030E 06	0.255659E 05	0.	0.
4.50	*21535E 08	59.76	76.77	0.60033E 06	0.255659E 05	0.	0.
4.60	*21535E 08	59.58	77.48	0.60036E 06	0.255658E 05	0.	0.
4.70	*21535E 08	59.4C	78.18	0.60038E 06	0.255658E 05	0.	0.
4.80	*21535E 08	59.21	79.56	0.60041E 06	0.255658E 05	0.	0.
4.90	*21535E 08	59.02	80.24	0.60047E 06	0.255657E 05	0.	0.
5.00	*21535E 08	58.82	80.91	0.60050E 06	0.255657E 05	0.	0.
5.10	*21535E 08	58.63	81.57	0.600923E 06	0.255562E 05	0.	0.

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(DEG)	VELOCITY(FT/S)	BAL. COEF.(PT/SLG)	ATMOS. DENSI.(SLG/PT*2/SLG)
5.20	215352.08	59.42	82.23	0.6095E 06	0.255556E 05	0	0
5.30	215352.08	58.22	82.88	0.6098E 06	0.255568E 05	0	0
5.40	215352.08	58.01	83.52	0.6091E 06	0.255555E 05	0	0
5.50	215352.08	57.80	84.15	0.6094E 06	0.255565E 05	0	0
5.60	215352.08	57.58	84.77	0.6097E 06	0.255565E 05	0	0
5.70	215352.08	57.37	85.39	0.6099E 06	0.255564E 05	0	0
5.80	215352.08	57.14	85.99	0.6092E 06	0.255564E 05	0	0
5.90	215352.08	56.92	86.59	0.6095E 06	0.255564E 05	0	0
6.00	215352.08	56.69	87.19	0.6098E 06	0.255563E 05	0	0
6.10	215352.08	56.46	87.77	0.6092E 06	0.255563E 05	0	0
6.20	215352.08	56.22	88.35	0.6093E 06	0.255563E 05	0	0
6.30	215352.08	55.99	88.92	0.6096E 06	0.255562E 05	0	0
6.40	215352.08	55.75	89.49	0.6098E 06	0.255562E 05	0	0
6.50	215352.08	55.51	90.04	0.6091E 06	0.255562E 05	0	0
6.60	215352.08	55.26	90.59	0.6094E 06	0.255552E 05	0	0
6.70	215352.08	55.01	91.13	0.6097E 06	0.255561E 05	0	0
6.80	215352.08	54.76	91.67	0.6093E 06	0.255561E 05	0	0
6.90	215352.08	54.52	92.20	0.6092E 06	0.255561E 05	0	0
7.00	215352.08	54.25	92.72	0.6105E 06	0.255559E 05	0	0
7.10	215352.08	53.99	93.24	0.6107E 06	0.255560E 05	0	0
7.20	215352.08	53.73	93.74	0.6102E 06	0.255550E 05	0	0
7.30	215352.08	53.47	94.24	0.6105E 06	0.255561E 05	0	0
7.40	215352.08	53.21	94.73	0.6105E 06	0.255561E 05	0	0
7.50	215352.08	52.94	95.22	0.6108E 06	0.255561E 05	0	0
7.60	215352.08	52.67	95.70	0.6102E 06	0.255561E 05	0	0
7.70	215352.08	52.40	96.18	0.6103E 06	0.255561E 05	0	0
7.80	215352.08	52.12	96.65	0.6105E 06	0.255561E 05	0	0
7.90	215352.08	51.85	97.11	0.6102E 06	0.255561E 05	0	0
8.00	215352.08	51.58	97.57	0.6103E 06	0.255561E 05	0	0
8.10	215352.08	51.29	98.02	0.6103E 06	0.255561E 05	0	0
8.20	215352.08	51.01	98.47	0.6105E 06	0.255561E 05	0	0
8.30	215352.08	50.73	98.91	0.6102E 06	0.255561E 05	0	0
8.40	215352.08	50.44	99.34	0.6102E 06	0.255561E 05	0	0
8.50	215352.08	50.15	99.77	0.6103E 06	0.255561E 05	0	0
8.60	215352.08	49.86	100.20	0.6103E 06	0.255561E 05	0	0
8.70	215352.08	49.57	100.61	0.6108E 06	0.255561E 05	0	0
8.80	215352.08	49.28	101.03	0.6105E 06	0.255561E 05	0	0
8.90	215352.08	48.99	101.43	0.6103E 06	0.255561E 05	0	0
9.00	215352.08	48.69	101.84	0.6105E 06	0.255561E 05	0	0
9.10	215352.08	48.40	102.23	0.6108E 06	0.255561E 05	0	0
9.20	215352.08	48.11	102.63	0.6100E 06	0.255561E 05	0	0
9.30	215352.08	47.80	103.01	0.6102E 06	0.255561E 05	0	0
9.40	215352.08	47.51	103.40	0.6105E 06	0.255561E 05	0	0
9.50	215352.08	47.19	103.78	0.6107E 06	0.255561E 05	0	0
9.60	215352.08	46.89	104.15	0.6109E 06	0.255561E 05	0	0
9.70	215352.08	46.58	104.52	0.6102E 06	0.255561E 05	0	0
9.80	215352.08	46.28	104.88	0.6104E 06	0.255561E 05	0	0
9.90	215352.08	45.97	105.24	0.6106E 06	0.255561E 05	0	0
10.00	215352.08	45.66	105.60	0.6109E 06	0.255561E 05	0	0
10.10	215352.08	45.35	105.95	0.6101E 06	0.255561E 05	0	0
10.20	215352.08	45.03	106.30	0.6103E 06	0.255561E 05	0	0
10.30	215352.08	44.72	106.65	0.6108E 06	0.255561E 05	0	0

TIME(MIN)	RADIUS(FT)	TRAJECTORY NUMBER	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(DEG)	VELOCITY(FT/S)	BAL.COEFF.(FT**2/SLG)	ATMOS.DENS.(SLG/FT**3)
10.40	4.215372	48	44.41	44.09	106.98	0.61088E 06	0.2556402 05	0.2556402 05
10.50	4.215372	48	44.40	44.09	107.32	0.61090E 06	0.2556402 05	0.2556402 05
10.60	4.215372	48	43.77	43.46	107.65	0.61092E 06	0.2556402 05	0.2556402 05
10.70	4.215372	48	43.46	43.46	107.98	0.61094E 06	0.2556402 05	0.2556402 05
10.80	4.215372	48	43.44	43.44	108.31	0.61097E 06	0.2556392 05	0.2556392 05
10.90	4.215372	48	42.82	42.82	108.63	0.61099E 06	0.2556392 05	0.2556392 05
11.00	4.215372	48	42.5	42.5	108.94	0.61101E 06	0.2556392 05	0.2556392 05
11.10	4.215372	48	42.17	42.17	109.26	0.61103E 06	0.2556392 05	0.2556392 05
11.20	4.215372	48	41.95	41.95	109.57	0.61105E 06	0.2556392 05	0.2556392 05
11.30	4.215372	48	41.53	41.53	109.88	0.61107E 06	0.2556382 05	0.2556382 05
11.40	4.215372	48	41.2	41.2	110.18	0.61109E 06	0.2556382 05	0.2556382 05
11.50	4.215372	48	40.85	40.85	110.48	0.61111E 06	0.2556382 05	0.2556382 05
11.60	4.215372	48	40.55	40.55	110.78	0.61113E 06	0.2556372 05	0.2556372 05
11.70	4.215372	48	40.22	40.22	111.07	0.61115E 06	0.2556372 05	0.2556372 05
11.80	4.215372	48	39.89	39.89	111.36	0.61117E 06	0.2556372 05	0.2556372 05
11.90	4.215372	48	39.56	39.56	111.65	0.61119E 06	0.2556372 05	0.2556372 05
12.00	4.215372	48	39.23	39.23	111.94	0.61121E 06	0.2556362 05	0.2556362 05
12.10	4.215372	48	38.9	38.9	112.22	0.61123E 06	0.2556362 05	0.2556362 05
12.20	4.215372	48	38.57	38.57	112.50	0.61125E 06	0.2556362 05	0.2556362 05
12.30	4.215372	48	38.24	38.24	112.78	0.61127E 06	0.2556362 05	0.2556362 05
12.40	4.215372	48	37.91	37.91	113.05	0.61129E 06	0.2556352 05	0.2556352 05
12.50	4.215372	48	37.57	37.57	113.32	0.61131E 06	0.2556352 05	0.2556352 05
12.60	4.215372	48	37.24	37.24	113.59	0.61133E 06	0.2556352 05	0.2556352 05
12.70	4.215372	48	36.9	36.9	113.85	0.61135E 06	0.2556352 05	0.2556352 05
12.80	4.215372	48	36.56	36.56	114.12	0.61137E 06	0.2556352 05	0.2556352 05
12.90	4.215372	48	36.23	36.23	114.38	0.61139E 06	0.2556342 05	0.2556342 05
13.00	4.215372	48	35.89	35.89	114.64	0.61140E 06	0.2556342 05	0.2556342 05
13.10	4.215372	48	35.55	35.55	114.89	0.61142E 06	0.2556342 05	0.2556342 05
13.20	4.215372	48	35.21	35.21	115.15	0.61144E 06	0.2556342 05	0.2556342 05
13.30	4.215372	48	34.87	34.87	115.40	0.61146E 06	0.2556342 05	0.2556342 05
13.40	4.215372	48	34.53	34.53	115.65	0.61148E 06	0.2556342 05	0.2556342 05
13.50	4.215372	48	34.19	34.19	115.99	0.61149E 06	0.2556332 05	0.2556332 05
13.60	4.215372	48	33.85	33.85	116.14	0.61151E 06	0.2556332 05	0.2556332 05
13.70	4.215372	48	33.51	33.51	116.38	0.61153E 06	0.2556332 05	0.2556332 05
13.80	4.215372	48	33.17	33.17	116.62	0.61154E 06	0.2556332 05	0.2556332 05
13.90	4.215372	48	32.82	32.82	116.86	0.61156E 06	0.2556332 05	0.2556332 05
14.00	4.215372	48	32.48	32.48	117.10	0.61158E 06	0.2556332 05	0.2556332 05
14.10	4.215372	48	32.14	32.14	117.33	0.61159E 06	0.2556322 05	0.2556322 05
14.20	4.215372	48	31.79	31.79	117.56	0.61161E 06	0.2556322 05	0.2556322 05
14.30	4.215372	48	31.45	31.45	117.79	0.61163E 06	0.2556312 05	0.2556312 05
14.40	4.215372	48	31.1	31.1	118.02	0.61164E 06	0.2556312 05	0.2556312 05
14.50	4.215372	48	30.75	30.75	118.25	0.61166E 06	0.2556312 05	0.2556312 05
14.60	4.215372	48	30.41	30.41	118.47	0.61167E 06	0.2556312 05	0.2556312 05
14.70	4.215372	48	30.06	30.06	118.70	0.61169E 06	0.2556312 05	0.2556312 05
14.80	4.215372	48	29.71	29.71	118.92	0.61170E 06	0.2556312 05	0.2556312 05
14.90	4.215372	48	29.36	29.36	119.14	0.61172E 06	0.2556312 05	0.2556312 05
15.00	4.215372	48	29.02	29.02	119.35	0.61173E 06	0.2556312 05	0.2556312 05
15.10	4.215372	48	28.67	28.67	119.57	0.61175E 06	0.2556302 05	0.2556302 05
15.20	4.215372	48	28.32	28.32	119.79	0.61176E 06	0.2556302 05	0.2556302 05
15.30	4.215372	48	27.97	27.97	120.00	0.61178E 06	0.2556302 05	0.2556302 05
15.40	4.215372	48	27.62	27.62	120.21	0.61179E 06	0.2556302 05	0.2556302 05
15.50	4.215372	48	27.27	27.27	120.42	0.61180E 06	0.2556292 05	0.2556292 05

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER 4

TIME(WN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(FT)	VELOCITY(FT/SEC)	BAL. COEFF.(FT**4/SIG)	ATMOS DENS.(SLG/FT**3)
15.50	21537E 08	26.92	120.63	0.61182E 06	0.255649E 05		
15.50	21537E 08	26.56	120.84	0.61182E 06	0.255649E 05		
15.50	21537E 08	26.21	121.04	0.61182E 06	0.255649E 05		
15.50	21537E 08	25.16	121.25	0.61182E 06	0.255649E 05		
15.50	21538E 08	25.51	121.45	0.61182E 06	0.255649E 05		
15.50	21538E 08	25.16	121.65	0.61182E 06	0.255649E 05		
15.50	21538E 08	24.81	121.85	0.61182E 06	0.255649E 05		
15.50	21538E 08	24.45	122.05	0.61182E 06	0.255649E 05		
15.50	21538E 08	24.10	122.25	0.61182E 06	0.255649E 05		
15.50	21538E 08	23.44	122.45	0.61182E 06	0.255649E 05		
15.50	21538E 08	23.39	122.64	0.61182E 06	0.255649E 05		
15.50	21538E 08	23.03	122.84	0.61182E 06	0.255649E 05		
15.50	21538E 08	22.68	123.03	0.61182E 06	0.255649E 05		
15.50	21538E 08	22.32	123.22	0.61182E 06	0.255649E 05		
15.50	21538E 08	21.97	123.41	0.61182E 06	0.255649E 05		
15.50	21538E 08	21.61	123.60	0.61182E 06	0.255649E 05		
15.50	21538E 08	21.25	123.79	0.61182E 06	0.255649E 05		
15.50	21538E 08	20.90	123.98	0.61182E 06	0.255649E 05		
15.50	21538E 08	20.44	124.16	0.61182E 06	0.255649E 05		
15.50	21538E 08	20.18	124.35	0.61182E 06	0.255649E 05		
15.50	21538E 08	19.83	124.53	0.61182E 06	0.255649E 05		
15.50	21538E 08	19.47	124.72	0.61182E 06	0.255649E 05		
15.50	21538E 08	19.11	124.91	0.61182E 06	0.255649E 05		
15.50	21538E 08	18.75	125.08	0.61182E 06	0.255649E 05		
15.50	21538E 08	18.39	125.26	0.61182E 06	0.255649E 05		
15.50	21538E 08	18.04	125.44	0.61182E 06	0.255649E 05		
15.50	21538E 08	17.68	125.62	0.61182E 06	0.255649E 05		
15.50	21538E 08	17.32	125.80	0.61182E 06	0.255649E 05		
15.50	21538E 08	16.96	125.98	0.61182E 06	0.255649E 05		
15.50	21538E 08	16.60	126.16	0.61182E 06	0.255649E 05		
15.50	21538E 08	16.24	126.33	0.61182E 06	0.255649E 05		
15.50	21538E 08	15.88	126.51	0.61182E 06	0.255649E 05		
15.50	21538E 08	15.52	126.68	0.61182E 06	0.255649E 05		
15.50	21538E 08	15.16	126.86	0.61182E 06	0.255649E 05		
15.50	21538E 08	14.81	127.03	0.61182E 06	0.255649E 05		
15.50	21538E 08	14.44	127.20	0.61182E 06	0.255649E 05		
15.50	21538E 08	14.08	127.38	0.61182E 06	0.255649E 05		
15.50	21538E 08	13.72	127.55	0.61182E 06	0.255649E 05		
15.50	21538E 08	13.36	127.72	0.61182E 06	0.255649E 05		
15.50	21538E 08	13.00	127.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	12.64	128.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	12.28	128.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	11.91	128.40	0.61182E 06	0.255649E 05		
15.50	21538E 08	11.55	128.56	0.61182E 06	0.255649E 05		
15.50	21538E 08	11.19	128.73	0.61182E 06	0.255649E 05		
15.50	21538E 08	10.80	128.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	10.44	129.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	10.00	129.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	9.55	129.40	0.61182E 06	0.255649E 05		
15.50	21538E 08	9.19	129.56	0.61182E 06	0.255649E 05		
15.50	21538E 08	8.80	129.73	0.61182E 06	0.255649E 05		
15.50	21538E 08	8.44	129.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	8.00	130.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	7.55	130.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	7.19	130.40	0.61182E 06	0.255649E 05		
15.50	21538E 08	6.80	130.56	0.61182E 06	0.255649E 05		
15.50	21538E 08	6.44	130.73	0.61182E 06	0.255649E 05		
15.50	21538E 08	6.00	130.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	5.55	131.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	5.19	131.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	4.80	131.40	0.61182E 06	0.255649E 05		
15.50	21538E 08	4.44	131.56	0.61182E 06	0.255649E 05		
15.50	21538E 08	4.00	131.73	0.61182E 06	0.255649E 05		
15.50	21538E 08	3.55	131.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	3.19	132.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	2.80	132.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	2.44	132.40	0.61182E 06	0.255649E 05		
15.50	21538E 08	2.00	132.56	0.61182E 06	0.255649E 05		
15.50	21538E 08	1.55	132.73	0.61182E 06	0.255649E 05		
15.50	21538E 08	1.19	132.89	0.61182E 06	0.255649E 05		
15.50	21538E 08	0.80	133.06	0.61182E 06	0.255649E 05		
15.50	21538E 08	0.44	133.23	0.61182E 06	0.255649E 05		
15.50	21538E 08	0.00	133.40	0.61182E 06	0.255649E 05		

RADAR PARAMETERS • TRAJECTORY NUMBER 4				RADAR SIZE 1	35.900 DEG.LAT.	233.333 DEG.LONG.
TIME (MIN)	SL RANGE (NM)	SL RANGE-RATE (FT/S)	ELEVATION (DEG)	EL RATE (DEG/S)	AZIMUTH (DEG)	AZ RATE (DEG/S)
11.80	0.778882E+03	-0.178166E+05	1.02	0.5267E-01	292.92	+0.1029
11.90	0.761476E+03	-0.174544E+05	1.34	0.5288E-01	291.67	+0.1029
12.00	0.744441E+03	-0.170659E+05	1.65	0.5302E-01	290.36	+0.1029
12.10	0.727803E+03	-0.166493E+05	1.97	0.5302E-01	288.99	+0.1029
12.20	0.711591E+03	-0.162028E+05	2.29	0.5302E-01	287.56	+0.1029
12.30	0.695834E+03	-0.157244E+05	2.61	0.5285E-01	286.06	+0.1029
12.40	0.685567E+03	-0.152122E+05	2.92	0.5252E-01	284.49	+0.1029
12.50	0.665822E+03	-0.146642E+05	3.24	0.5202E-01	282.85	+0.1029
12.60	0.651636E+03	-0.140767E+05	3.55	0.5129E-01	281.13	+0.1029
12.70	0.638048E+03	-0.134538E+05	3.85	0.4505E-01	279.33	+0.1029
12.80	0.625196E+03	-0.127871E+05	4.15	0.4952E-01	277.46	+0.1029
12.90	0.612622E+03	-0.120803E+05	4.44	0.4662E-01	275.51	+0.1029
13.00	0.612682E+03	-0.113295E+05	4.72	0.4552E-01	273.48	+0.1029
13.10	0.590477E+03	-0.105351E+05	4.99	0.4398E-01	271.37	+0.1029
13.20	0.574892E+03	-0.969719E+04	5.25	0.4172E-01	269.18	+0.1029
13.30	0.571351E+03	-0.881643E+04	5.49	0.3822E-01	266.92	+0.1029
13.40	0.563128E+03	-0.809418E+04	5.71	0.3497E-01	264.58	+0.1029
13.50	0.555783E+03	-0.693258E+04	5.90	0.3122E-01	262.18	+0.1029
13.60	0.546431E+03	-0.593457E+04	6.06	0.2722E-01	259.71	+0.1029
13.70	0.544681E+03	-0.490396E+04	6.23	0.2282E-01	257.19	+0.1029
13.80	0.539761E+03	-0.384534E+04	6.35	0.1812E-01	254.62	+0.1029
13.90	0.536499E+03	-0.276492E+04	6.45	0.1352E-01	252.02	+0.1029
14.00	0.531311E+03	-0.166672E+04	6.51	0.7932E-02	249.38	+0.1029
14.10	0.513213E+03	-0.558085E+03	6.54	0.2719E-02	246.73	+0.1029
14.20	0.533211E+03	-0.553326E+03	6.54	0.2591E-02	244.08	+0.1029
14.30	0.531304E+03	-0.166335E+04	6.45	0.2852E-02	241.43	+0.1029
14.40	0.536487E+03	-0.275932E+04	6.45	0.1302E-01	238.80	+0.1029
14.50	0.519744E+03	-0.383993E+04	6.36	-0.1802E-01	236.19	+0.1029
14.60	0.504588E+03	-0.489870E+04	6.23	-0.2272E-01	233.62	+0.1029
14.70	0.549402E+03	-0.592812E+04	6.08	-0.2212E-01	231.10	+0.1029
14.80	0.555747E+03	-0.692546E+04	5.91	-0.3112E-01	228.63	+0.1029
14.90	0.560595E+03	-0.288633E+04	5.71	-0.3468E-01	226.23	+0.1029
15.00	0.571313E+03	-0.887762E+04	5.49	-0.3852E-01	223.89	+0.1029
15.10	0.580429E+03	-0.968763E+04	5.25	-0.4106E-01	221.63	+0.1029
15.20	0.555462E+03	-0.052462E+05	5.00	-0.4352E-01	219.44	+0.1029
15.30	0.611878E+03	-0.113180E+05	4.73	-0.4572E-01	217.33	+0.1029
15.40	0.622973E+03	-0.126782E+05	4.45	-0.4755E-01	215.29	+0.1029
15.50	0.624991E+03	-0.127746E+05	4.16	-0.4902E-01	213.34	+0.1029
15.60	0.639292E+03	-0.134392E+05	3.86	-0.5028E-01	211.46	+0.1029
15.70	0.651502E+03	-0.140629E+05	3.56	-0.5120E-01	209.67	+0.1029
15.80	0.655672E+03	-0.146674E+05	3.25	-0.5191E-01	207.95	+0.1029
15.90	0.680399E+03	-0.151942E+05	2.94	-0.5242E-01	206.30	+0.1029
16.00	0.675648E+03	-0.157053E+05	2.62	-0.5273E-01	204.73	+0.1029
16.10	0.713858E+03	-0.161825E+05	2.30	-0.5295E-01	203.23	+0.1029
16.20	0.727577E+03	-0.166279E+05	1.99	-0.5295E-01	201.79	+0.1029
16.30	0.744194E+03	-0.170433E+05	1.67	-0.5295E-01	200.42	+0.1029
16.40	0.761262E+03	-0.17436E+05	1.35	-0.5282E-01	199.11	+0.1029
16.50	0.785872E+03	-0.177916E+05	1.03	-0.5255E-01	197.86	+0.1029

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER 5

TIME(MIN)	RADIUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(DEG)	VELOCITY(FT/S)	BAL.CORR.(SIG. FIGS.)	ATMOS.DENS.(SIG.FIGS.)
0.	62.534E 08	62.70	40.35	0.6083E 06	0.255551E 05	0	0
0.10	62.534E 08	62.76	41.21	0.6083E 06	0.255551E 05	0	0
0.20	62.534E 08	62.81	42.07	0.6083E 06	0.255551E 05	0	0
0.30	62.534E 08	62.95	42.93	0.6083E 06	0.255551E 05	0	0
0.40	62.534E 08	62.89	43.80	0.6083E 06	0.255551E 05	0	0
0.50	62.534E 08	62.92	44.67	0.6083E 06	0.255551E 05	0	0
0.60	62.534E 08	62.95	45.54	0.6083E 06	0.255551E 05	0	0
0.70	62.534E 08	62.97	46.41	0.6083E 06	0.255551E 05	0	0
0.80	62.534E 08	62.99	47.28	0.6083E 06	0.255551E 05	0	0
0.90	62.534E 08	63.00	48.15	0.6083E 06	0.255551E 05	0	0
1.00	62.534E 08	63.00	49.03	0.6083E 06	0.255551E 05	0	0
1.10	62.534E 08	63.00	49.90	0.6083E 06	0.255551E 05	0	0
1.20	62.534E 08	62.99	50.77	0.6081E 06	0.255551E 05	0	0
1.30	62.534E 08	62.98	51.65	0.6080E 06	0.255551E 05	0	0
1.40	62.534E 08	62.96	52.52	0.6080E 06	0.255551E 05	0	0
1.50	62.534E 08	62.94	53.39	0.6080E 06	0.255551E 05	0	0
1.60	62.534E 08	62.91	54.26	0.6080E 06	0.255551E 05	0	0
1.70	62.534E 08	62.87	55.13	0.6080E 06	0.255551E 05	0	0
1.80	62.534E 08	62.83	55.99	0.6080E 06	0.255551E 05	0	0
1.90	62.534E 08	62.78	56.85	0.6079E 06	0.255551E 05	0	0
2.00	62.534E 08	62.73	57.71	0.6079E 06	0.255551E 05	0	0
2.10	62.534E 08	62.67	58.57	0.6078E 06	0.255551E 05	0	0
2.20	62.534E 08	62.61	59.42	0.6078E 06	0.255551E 05	0	0
2.30	62.534E 08	62.54	60.27	0.6078E 06	0.255551E 05	0	0
2.40	62.534E 08	62.47	61.11	0.6078E 06	0.255551E 05	0	0
2.50	62.534E 08	62.39	61.95	0.6077E 06	0.255551E 05	0	0
2.60	62.534E 08	62.33	62.79	0.6076E 06	0.255551E 05	0	0
2.70	62.534E 08	62.21	63.62	0.6076E 06	0.255551E 05	0	0
2.80	62.534E 08	62.14	64.47	0.6075E 06	0.255551E 05	0	0
2.90	62.534E 08	62.02	65.26	0.6075E 06	0.255551E 05	0	0
3.00	62.534E 08	61.91	66.08	0.6074E 06	0.255551E 05	0	0
3.10	62.534E 08	61.80	66.88	0.6073E 06	0.255551E 05	0	0
3.20	62.534E 08	61.69	67.69	0.6073E 06	0.255551E 05	0	0
3.30	62.534E 08	61.57	68.48	0.6072E 06	0.255551E 05	0	0
3.40	62.534E 08	61.44	69.27	0.6072E 06	0.255551E 05	0	0
3.50	62.534E 08	61.31	70.05	0.6071E 06	0.255551E 05	0	0
3.60	62.534E 08	61.18	70.83	0.6070E 06	0.255551E 05	0	0
3.70	62.534E 08	61.04	71.60	0.6070E 06	0.255551E 05	0	0
3.80	62.534E 08	60.89	72.36	0.6070E 06	0.255551E 05	0	0
3.90	62.534E 08	60.74	73.11	0.6070E 06	0.255551E 05	0	0
4.00	62.534E 08	60.59	73.86	0.6070E 06	0.255551E 05	0	0
4.10	62.534E 08	60.43	74.60	0.6070E 06	0.255551E 05	0	0
4.20	62.534E 08	60.27	75.33	0.6070E 06	0.255551E 05	0	0
4.30	62.534E 08	60.10	76.06	0.6070E 06	0.255551E 05	0	0
4.40	62.534E 08	59.93	76.77	0.6070E 06	0.255551E 05	0	0
4.50	62.534E 08	59.76	77.48	0.6070E 06	0.255551E 05	0	0
4.60	62.534E 08	59.58	78.18	0.6070E 06	0.255551E 05	0	0
4.70	62.534E 08	59.40	78.88	0.6071E 06	0.255551E 05	0	0
4.80	62.534E 08	59.21	79.56	0.6070E 06	0.255551E 05	0	0
4.90	62.534E 08	59.02	80.24	0.6070E 06	0.255551E 05	0	0
5.00	62.534E 08	58.82	80.91	0.6070E 06	0.255551E 05	0	0
5.10	62.534E 08	58.63	81.57	0.6070E 06	0.255551E 05	0	0

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER

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TIME(MIN)	RADIUS(FT)	LATITUDE(LEG)	LONGITUDE(DEG)	HEIGHT(FT)	VELOCITY(FT/S)	BAL.COEFF.(FT**2/SIG)	ATMOS.DENS.(SIG/FT**3)
5.20	21533E 8	58.42	82.23	0.6077E 06	0.255654E 05	0.	0.
5.30	21533E 08	58.22	82.88	0.6077E 06	0.255654E 05	0.	0.
5.40	21533E 8	56.	83.52	0.6077E 06	0.255654E 05	0.	0.
5.50	21533E 08	57.80	84.15	0.6077E 06	0.255655E 05	0.	0.
5.60	21533E 8	57.58	84.77	0.6077E 06	0.255655E 05	0.	0.
5.70	21533E 08	57.37	85.39	0.6077E 06	0.255655E 05	0.	0.
5.80	21533E 8	57.14	85.99	0.6077E 06	0.255655E 05	0.	0.
5.90	21533E 08	56.92	86.59	0.60769E 06	0.255655E 05	0.	0.
6.00	21533E 8	56.69	87.19	0.60768E 06	0.255655E 05	0.	0.
6.10	21533E 08	56.46	87.77	0.60767E 06	0.255655E 05	0.	0.
6.20	21533E 8	56.22	88.35	0.60766E 06	0.255655E 05	0.	0.
6.30	21533E 08	55.99	88.92	0.60764E 06	0.255655E 05	0.	0.
6.40	21533E 8	55.75	89.49	0.60763E 06	0.255655E 05	0.	0.
6.50	21533E 08	55.51	90.04	0.60762E 06	0.255655E 05	0.	0.
6.60	21533E 8	55.26	90.59	0.60761E 06	0.255655E 05	0.	0.
6.70	21533E 08	55.01	91.13	0.60760E 06	0.255655E 05	0.	0.
6.80	21533E 8	54.76	91.67	0.60758E 06	0.255655E 05	0.	0.
6.90	21533E 08	54.51	92.20	0.60757E 06	0.255655E 05	0.	0.
7.00	21533E 8	54.25	92.72	0.60756E 06	0.255655E 05	0.	0.
7.10	21533E 08	53.95	93.23	0.60754E 06	0.255657E 05	0.	0.
7.20	21533E 8	53.73	93.74	0.60753E 06	0.255657E 05	0.	0.
7.30	21533E 08	53.47	94.24	0.60752E 06	0.255657E 05	0.	0.
7.40	21533E 8	53.21	94.74	0.60750E 06	0.255657E 05	0.	0.
7.50	21533E 08	52.94	95.22	0.60749E 06	0.255657E 05	0.	0.
7.60	21533E 8	52.67	95.71	0.60747E 06	0.255658E 05	0.	0.
7.70	21533E 08	52.43	96.18	0.60746E 06	0.255658E 05	0.	0.
7.80	21533E 8	52.12	96.65	0.60745E 06	0.255658E 05	0.	0.
7.90	21533E 08	51.85	97.11	0.60743E 06	0.255658E 05	0.	0.
8.00	21533E 8	51.57	97.57	0.60742E 06	0.255658E 05	0.	0.
8.10	21533E 08	51.29	98.02	0.60740E 06	0.255659E 05	0.	0.
8.20	21533E 8	51.01	98.47	0.60739E 06	0.255659E 05	0.	0.
8.30	21533E 08	50.73	98.91	0.60737E 06	0.255659E 05	0.	0.
8.40	21533E 8	50.44	99.34	0.60736E 06	0.255659E 05	0.	0.
8.50	21533E 08	50.15	99.77	0.60734E 06	0.255659E 05	0.	0.
8.60	21533E 8	49.86	100.20	0.60732E 06	0.255659E 05	0.	0.
8.70	21533E 08	49.57	100.62	0.60731E 06	0.255660E 05	0.	0.
8.80	21533E 8	49.28	101.03	0.60729E 06	0.255660E 05	0.	0.
8.90	21533E 08	48.99	101.44	0.60728E 06	0.255660E 05	0.	0.
9.00	21533E 8	48.69	101.84	0.60726E 06	0.255660E 05	0.	0.
9.10	21533E 08	48.39	102.24	0.60724E 06	0.255660E 05	0.	0.
9.20	21533E 8	48.11	102.63	0.60723E 06	0.255661E 05	0.	0.
9.30	21533E 08	47.80	103.02	0.60721E 06	0.255661E 05	0.	0.
9.40	21533E 8	47.49	103.40	0.60719E 06	0.255661E 05	0.	0.
9.50	21533E 08	47.19	103.78	0.60718E 06	0.255661E 05	0.	0.
9.60	21533E 8	46.89	104.15	0.60716E 06	0.255661E 05	0.	0.
9.70	21533E 08	46.58	104.52	0.60714E 06	0.255662E 05	0.	0.
9.80	21533E 8	46.27	104.89	0.60712E 06	0.255662E 05	0.	0.
9.90	21533E 8	45.97	105.25	0.60710E 06	0.255662E 05	0.	0.
10.00	21533E 8	45.66	105.60	0.60709E 06	0.255662E 05	0.	0.
10.10	21533E 08	45.34	105.96	0.60707E 06	0.255662E 05	0.	0.
10.20	21533E 8	45.03	106.30	0.60705E 06	0.255662E 05	0.	0.
10.30	21533E 08	44.72	106.65	0.60703E 06	0.255663E 05	0.	0.

## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER

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TIME(MIN)	RADIUS(LFT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(DEG)	VELOCITY(FT/SEC)	BAL.CORR.(PTO/PILOT)	ATMOS.DENS.(SLG/PSI*000)
10.40	0.215320 08	64.4	106.99	0.607012 06	0.2556632 05	Q	Q
10.50	0.215320 08	64.09	107.32	0.606992 06	0.2556632 05	Q	Q
10.60	0.215320 08	63.77	107.66	0.606986 06	0.2556642 05	Q	Q
10.70	0.215320 08	63.45	107.98	0.606962 06	0.2556642 05	Q	Q
10.80	0.215320 08	63.13	108.31	0.606942 06	0.2556642 05	Q	Q
10.90	0.215320 08	62.81	108.63	0.606922 06	0.2556642 05	Q	Q
11.00	0.215320 08	62.49	108.95	0.606902 06	0.2556642 05	Q	Q
11.10	0.215320 08	62.17	109.26	0.606882 06	0.2556642 05	Q	Q
11.20	0.215320 08	61.85	109.57	0.606862 06	0.2556642 05	Q	Q
11.30	0.215320 08	61.52	109.88	0.606842 06	0.2556632 05	Q	Q
11.40	0.215320 08	61.20	110.18	0.606822 06	0.2556632 05	Q	Q
11.50	0.215320 08	60.87	110.48	0.606802 06	0.2556632 05	Q	Q
11.60	0.215320 08	60.55	110.78	0.606782 06	0.2556632 05	Q	Q
11.70	0.215320 08	60.22	111.08	0.606762 06	0.2556632 05	Q	Q
11.80	0.215320 08	59.89	111.37	0.606742 06	0.2556632 05	Q	Q
11.90	0.215320 08	59.56	111.66	0.606722 06	0.2556632 05	Q	Q
12.00	0.215320 08	59.23	111.94	0.606702 06	0.2556672 05	Q	Q
12.10	0.215320 08	58.90	112.22	0.606682 06	0.2556672 05	Q	Q
12.20	0.215320 08	58.57	112.50	0.606662 06	0.2556672 05	Q	Q
12.30	0.215320 08	58.23	112.78	0.606642 06	0.2556672 05	Q	Q
12.40	0.215320 08	57.90	113.05	0.606612 06	0.2556682 05	Q	Q
12.50	0.215320 08	57.57	113.32	0.606592 06	0.2556682 05	Q	Q
12.60	0.215320 08	57.23	113.59	0.606572 06	0.2556682 05	Q	Q
12.70	0.215320 08	56.90	113.86	0.606552 06	0.2556692 05	Q	Q
12.80	0.215320 08	56.56	114.12	0.606532 06	0.2556692 05	Q	Q
12.90	0.215320 08	56.22	114.38	0.606512 06	0.2556692 05	Q	Q
13.00	0.215320 08	55.88	114.64	0.606482 06	0.2556692 05	Q	Q
13.10	0.215320 08	55.55	114.90	0.606462 06	0.2556702 05	Q	Q
13.20	0.215320 08	55.21	115.15	0.606442 06	0.2556702 05	Q	Q
13.30	0.215320 08	54.87	115.40	0.606422 06	0.2556702 05	Q	Q
13.40	0.215320 08	54.53	115.65	0.606392 06	0.2556702 05	Q	Q
13.50	0.215320 08	54.19	115.90	0.606372 06	0.2556712 05	Q	Q
13.60	0.215320 08	53.84	116.14	0.606352 06	0.2556712 05	Q	Q
13.70	0.215320 08	53.51	116.39	0.606332 06	0.2556712 05	Q	Q
13.80	0.215320 08	53.16	116.63	0.606312 06	0.2556722 05	Q	Q
13.90	0.215320 08	52.82	116.86	0.606282 06	0.2556722 05	Q	Q
14.00	0.215320 08	52.47	117.10	0.606262 06	0.2556722 05	Q	Q
14.10	0.215320 08	52.13	117.34	0.606232 06	0.2556732 05	Q	Q
14.20	0.215320 08	51.78	117.57	0.606212 06	0.2556732 05	Q	Q
14.30	0.215320 08	51.44	117.80	0.606192 06	0.2556732 05	Q	Q
14.40	0.215320 08	51.09	118.03	0.606172 06	0.2556732 05	Q	Q
14.50	0.215320 08	50.75	118.25	0.606142 06	0.2556732 05	Q	Q
14.60	0.215320 08	50.41	118.48	0.606122 06	0.2556742 05	Q	Q
14.70	0.215320 08	50.05	118.70	0.606092 06	0.2556742 05	Q	Q
14.80	0.215320 08	49.70	118.92	0.606072 06	0.2556742 05	Q	Q
14.90	0.215320 08	49.36	119.14	0.606052 06	0.2556752 05	Q	Q
15.00	0.215320 08	49.01	119.36	0.606032 06	0.2556752 05	Q	Q
15.10	0.215320 08	48.66	119.58	0.606002 06	0.2556752 05	Q	Q
15.20	0.215320 08	48.31	119.79	0.605972 06	0.2556752 05	Q	Q
15.30	0.215320 08	47.96	120.01	0.605952 06	0.2556762 05	Q	Q
15.40	0.215320 08	47.61	120.22	0.605932 06	0.2556762 05	Q	Q
15.50	0.215320 08	47.26	120.43	0.605912 06	0.2556762 05	Q	Q

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## TRAJECTORY PARAMETERS - TRAJECTORY NUMBER

TIME(MIN)	RAUTUS(FT)	LATITUDE(DEG)	LONGITUDE(DEG)	HEIGHT(FT/S)	BAL COEFF, FT**2/SIG	ATHOS DENS, (SIG/PT**3)
15.60	*21532E 8	26.9	120.64	0.60567E 06	0.255677E 05	0.
15.70	*21531E 0.8	26.85	120.64	0.60585E 06	0.255677E 05	0.
15.80	*21531E 0.8	26.8	121.05	0.60582E 06	0.255677E 05	0.
15.90	*21531E 0.8	25.85	121.25	0.60580E 06	0.255678E 05	0.
16.00	*21531E 0.8	25.5	121.46	0.60577E 06	0.255678E 05	0.
16.10	*21531E 0.8	25.1	121.66	0.60575E 06	0.255678E 05	0.
16.20	*21531E 0.8	24.79	121.86	0.60572E 06	0.255678E 05	0.
16.30	*21531E 0.8	24.44	122.06	0.60570E 06	0.255678E 05	0.
16.40	*21531E 0.8	24.08	122.26	0.60567E 06	0.255678E 05	0.
16.50	*21531E 0.8	23.73	122.45	0.60565E 06	0.255678E 05	0.
16.60	*21531E 0.8	23.37	122.65	0.60562E 06	0.255680E 05	0.
16.70	*21531E 0.8	23.02	122.84	0.60560E 06	0.255680E 05	0.
16.80	*21531E 0.8	22.66	123.04	0.60557E 06	0.255680E 05	0.
16.90	*21531E 0.8	22.31	123.23	0.60555E 06	0.255681E 05	0.
17.00	*21531E 0.8	21.95	123.42	0.60552E 06	0.255681E 05	0.
17.10	*21531E 0.8	21.60	123.61	0.60549E 06	0.255681E 05	0.
17.20	*21531E 0.8	21.24	123.80	0.60547E 06	0.255681E 05	0.
17.30	*21531E 0.8	20.88	123.96	0.60544E 06	0.255682E 05	0.
17.40	*21531E 0.8	20.52	124.17	0.60542E 06	0.255682E 05	0.
17.50	*21531E 0.8	20.17	124.36	0.60539E 06	0.255682E 05	0.
17.60	*21531E 0.8	19.81	124.54	0.60536E 06	0.255682E 05	0.
17.70	*21531E 0.8	19.45	124.73	0.60534E 06	0.255682E 05	0.
17.80	*21531E 0.8	19.1	124.91	0.60531E 06	0.255682E 05	0.
17.90	*21531E 0.8	18.74	125.09	0.60529E 06	0.255684E 05	0.
18.00	*21531E 0.8	18.38	125.27	0.60526E 06	0.255684E 05	0.
18.10	*21531E 0.8	18.02	125.45	0.60523E 06	0.255684E 05	0.
18.20	*21531E 0.8	17.66	125.63	0.60521E 06	0.255684E 05	0.
18.30	*21531E 0.8	17.31	125.81	0.60518E 06	0.255685E 05	0.
18.40	*21531E 0.8	16.94	125.99	0.60515E 06	0.255685E 05	0.
18.50	*21531E 0.8	16.59	126.17	0.60513E 06	0.255686E 05	0.
18.60	*21531E 0.8	16.23	126.34	0.60510E 06	0.255686E 05	0.
18.70	*21531E 0.8	15.87	126.52	0.60507E 06	0.255686E 05	0.
18.80	*21531E 0.8	15.51	126.69	0.60505E 06	0.255686E 05	0.
18.90	*21531E 0.8	15.15	126.87	0.60502E 06	0.255687E 05	0.
19.00	*21531E 0.8	14.79	127.04	0.60499E 06	0.255687E 05	0.
19.10	*21531E 0.8	14.42	127.21	0.60497E 06	0.255687E 05	0.
19.20	*21531E 0.8	14.06	127.38	0.60494E 06	0.255688E 05	0.
19.30	*21531E 0.8	13.71	127.56	0.60491E 06	0.255688E 05	0.
19.40	*21531E 0.8	13.36	127.73	0.60488E 06	0.255688E 05	0.
19.50	*21530E 0.8	12.98	127.90	0.60486E 06	0.255689E 05	0.
19.60	*21531E 0.8	12.62	128.07	0.60483E 06	0.255689E 05	0.
19.70	*21530E 0.8	12.26	128.24	0.60480E 06	0.255689E 05	0.
19.80	*21531E 0.8	11.91	128.41	0.60478E 06	0.255690E 05	0.
19.90	*21530E 0.8	11.54	128.57	0.60475E 06	0.255690E 05	0.
20.00	*21531E 0.8	11.17	128.74	0.60472E 06	0.255690E 05	0.

## RADAR PARAMETERS , TRAJECTORY NUMBER 5 RADAR SITE 1

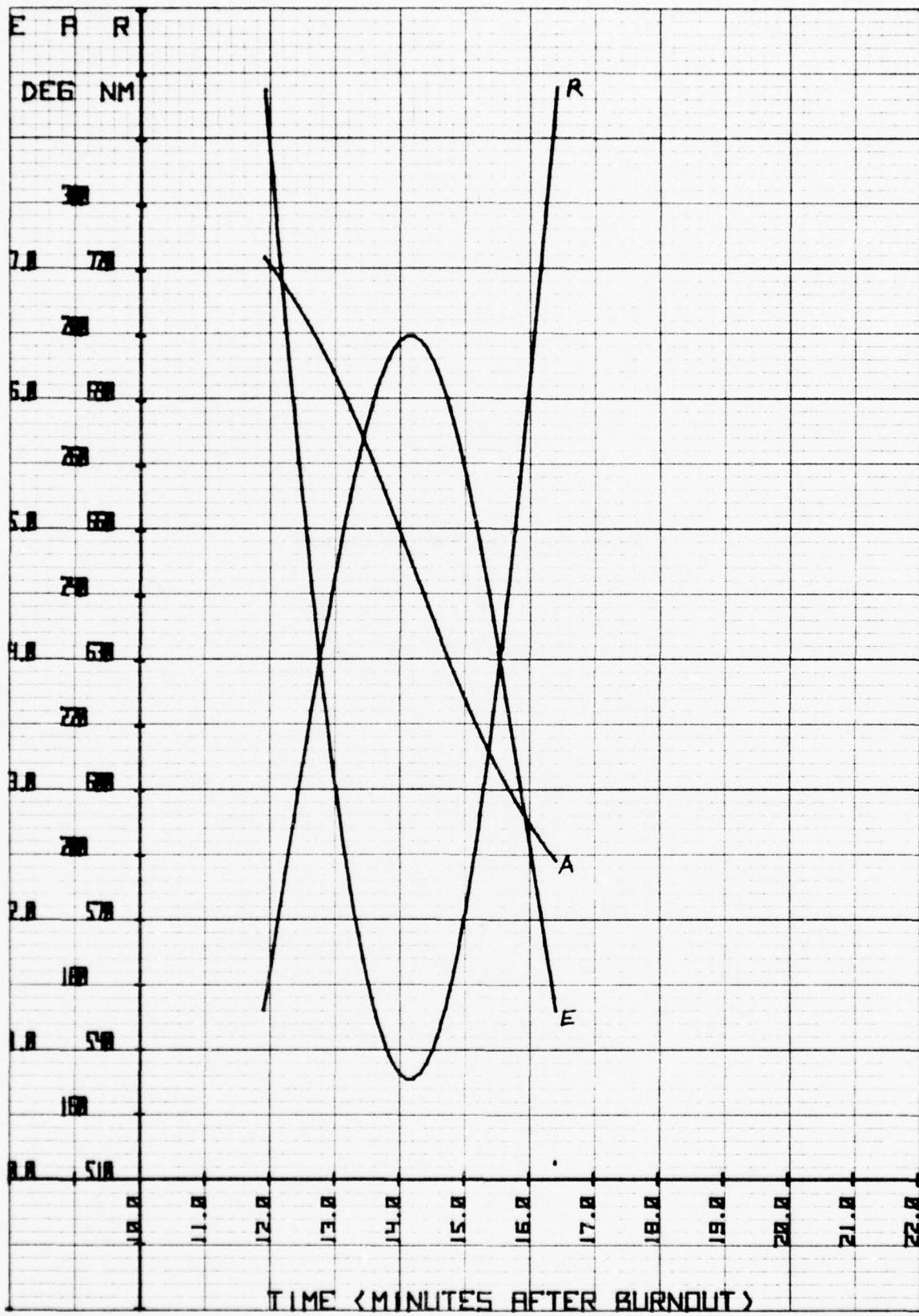
TIME 35.800 DEG.LAT.

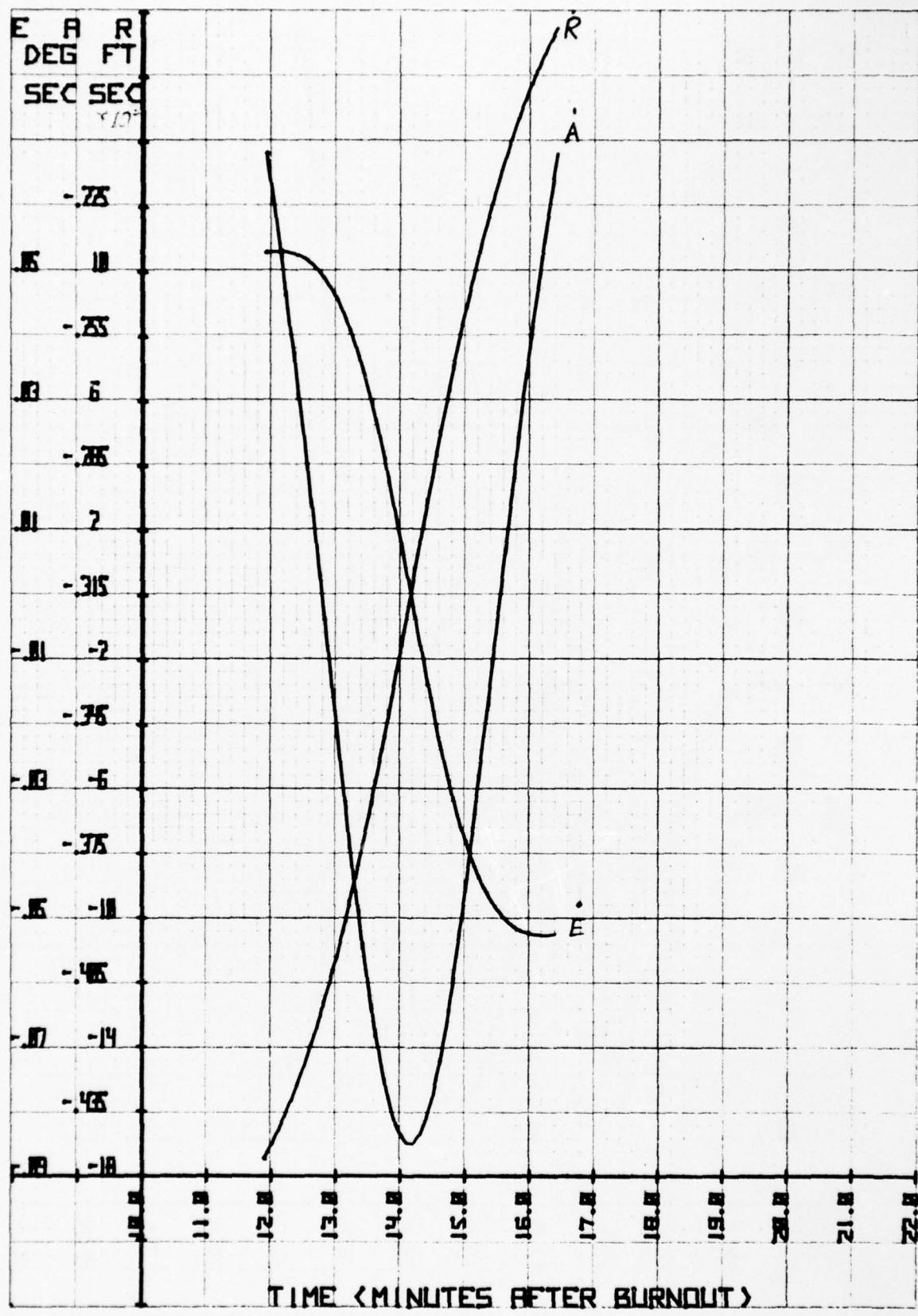
233.333 DEG.LONG.

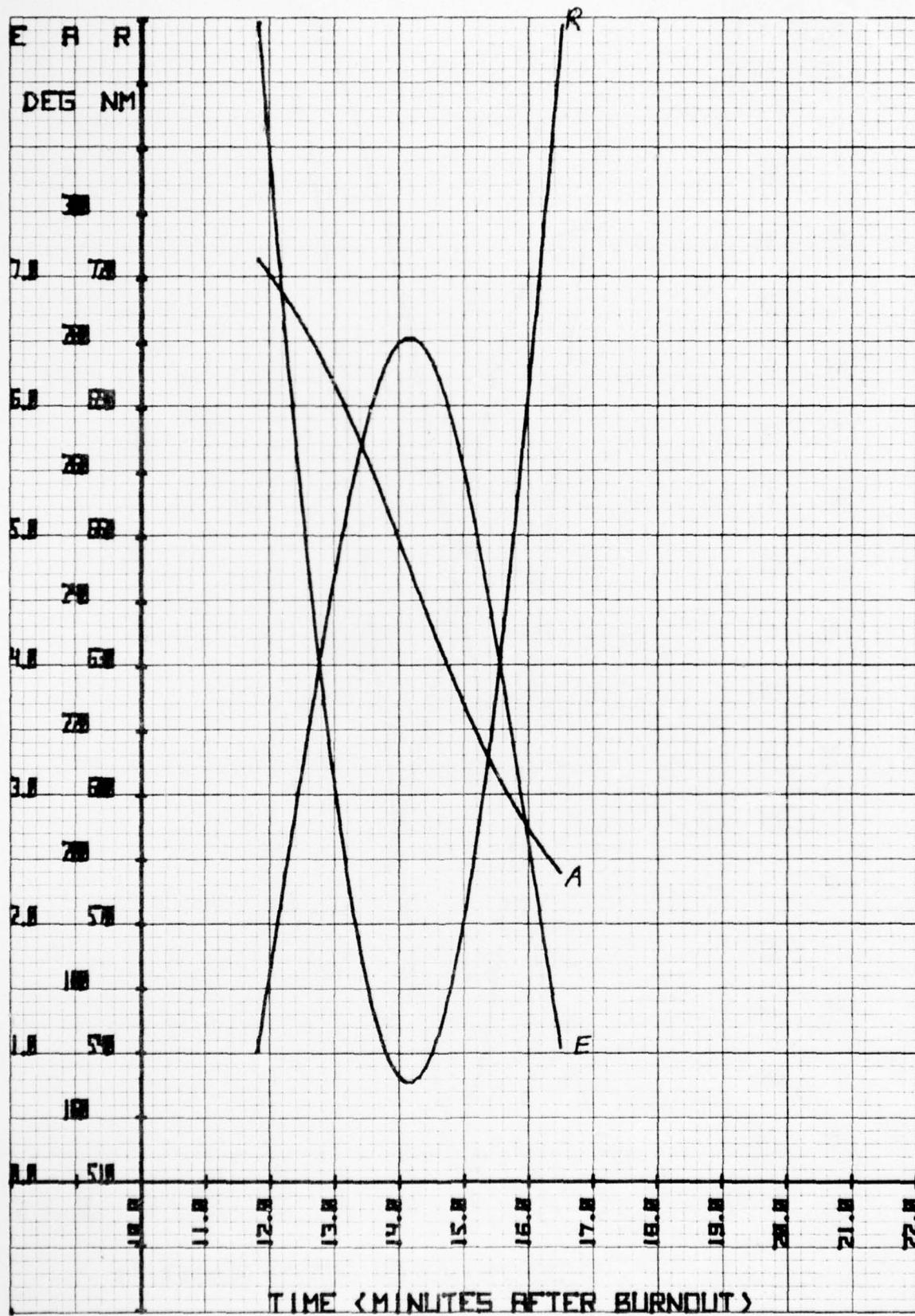
TIME (MM)	SL RANGE (MM)	SL RANGE-RATE (FT/SEC)	ELEVATION (DEG)	EL RATE (DEG/SEC)	AZIMUTH (DEG)	AZ RATE (DEG/SEC)	RADIUS (ERU)	INERTIAL PHZ (DEG)
11.90	0.761 682 0.3	-0.174577 0.05	1.29	0.5262 0.01	291.65	0.2130 0.0	1.929	51.66
12.00	0.740292 0.3	-0.170688 0.05	1.60	0.5276 0.01	290.34	0.2232 0.0	1.929	51.64
12.10	0.722388 0.3	-0.166518 0.05	1.92	0.5280 0.01	288.97	0.2332 0.0	1.929	51.62
12.20	0.711174 0.2	-0.162047 0.05	2.24	0.5274 0.01	287.54	0.2442 0.0	1.929	51.60
12.30	0.695462 0.3	-0.157257 0.05	2.55	0.5255 0.01	286.04	0.2552 0.0	1.929	51.58
12.40	0.680147 0.3	-0.152128 0.05	2.87	0.5221 0.01	284.47	0.2662 0.0	1.929	51.56
12.50	0.665438 0.3	-0.146640 0.05	3.18	0.5169 0.01	282.82	0.2780 0.0	1.929	51.54
12.60	0.651218 0.3	-0.140776 0.05	3.49	0.5097 0.01	281.10	0.2928 0.0	1.929	51.52
12.70	0.637631 0.3	-0.135182 0.05	3.79	0.5032 0.01	279.31	0.3058 0.0	1.929	51.50
12.80	0.624682 0.3	-0.127851 0.05	4.09	0.4882 0.01	277.43	0.3192 0.0	1.929	51.48
12.90	0.612112 0.3	-0.120762 0.05	4.37	0.4732 0.01	275.48	0.3323 0.0	1.929	51.46
13.00	0.600861 0.3	-0.113242 0.05	4.65	0.4551 0.01	273.44	0.3455 0.0	1.929	51.44
13.10	0.590752 0.3	-0.105285 0.05	4.92	0.4335 0.01	271.33	0.3587 0.0	1.929	51.42
13.20	0.580962 0.3	-0.968922 0.04	5.17	0.4083 0.01	269.14	0.3712 0.0	1.929	51.40
13.30	0.570663 0.3	-0.8807 0.04	5.41	0.3792 0.01	266.87	0.3836 0.0	1.929	51.38
13.40	0.562272 0.3	-0.288331 0.04	5.63	0.3463 0.01	264.54	0.3956 0.0	1.929	51.36
13.50	0.555422 0.3	-0.692018 0.04	5.82	0.3096 0.01	262.13	0.4061 0.0	1.929	51.34
13.60	0.549181 0.3	-0.920632 0.04	6.00	0.2691 0.01	259.66	0.4161 0.0	1.929	51.32
13.70	0.543452 0.3	-0.488848 0.04	6.15	0.2252 0.01	257.14	0.4242 0.0	1.929	51.30
13.80	0.539442 0.3	-0.328354 0.04	6.27	0.1782 0.01	254.57	0.4312 0.0	1.929	51.28
13.90	0.536196 0.3	-0.274562 0.04	6.36	0.1282 0.01	251.91	0.4381 0.0	1.929	51.26
14.00	0.534282 0.3	-0.164631 0.04	6.42	0.7733 0.02	249.32	0.4502 0.0	1.929	51.24
14.10	0.532502 0.3	-0.536933 0.03	6.45	0.2482 0.02	246.68	0.4622 0.0	1.929	51.22
14.20	0.532970 0.3	-0.515714 0.03	6.45	0.2809 0.02	244.02	0.4742 0.0	1.929	51.20
14.30	0.534852 0.3	-0.168472 0.04	6.42	0.8058 0.02	241.37	0.4862 0.0	1.929	51.18
14.40	0.536291 0.3	-0.278328 0.04	6.35	0.1319 0.01	238.74	0.4982 0.0	1.929	51.16
14.50	0.539532 0.3	-0.384942 0.04	6.26	0.1812 0.01	236.13	0.5112 0.0	1.929	51.14
14.60	0.543928 0.3	-0.492362 0.04	6.14	0.2280 0.01	233.56	0.5242 0.0	1.929	51.12
14.70	0.549823 0.3	-0.594472 0.04	5.99	0.2718 0.01	231.04	0.5362 0.0	1.929	51.10
14.80	0.555528 0.3	-0.691672 0.04	5.81	0.3120 0.01	228.57	0.5482 0.0	1.929	51.08
14.90	0.562993 0.3	-0.792664 0.04	5.61	0.3486 0.01	226.17	0.5592 0.0	1.929	51.06
15.00	0.571262 0.3	-0.883404 0.04	5.39	0.3813 0.01	223.83	0.5635 0.0	1.929	51.04
15.10	0.581422 0.3	-0.973772 0.04	5.16	0.4101 0.01	221.57	0.5712 0.0	1.929	51.02
15.20	0.590442 0.3	-0.105505 0.05	4.90	0.4351 0.01	219.38	0.5852 0.0	1.929	51.00
15.30	0.612121 0.3	-0.113436 0.05	4.64	0.4565 0.01	217.05	0.5952 0.0	1.929	50.98
15.40	0.612782 0.3	-0.120930 0.05	4.36	0.4744 0.01	215.24	0.6062 0.0	1.929	50.96
15.50	0.625774 0.3	-0.127932 0.05	4.07	0.4892 0.01	213.28	0.6182 0.0	1.929	50.94
15.60	0.638062 0.3	-0.134634 0.05	3.77	0.5011 0.01	211.41	0.6307 0.0	1.929	50.92
15.70	0.651632 0.3	-0.148666 0.05	3.47	0.5104 0.01	209.62	0.6428 0.0	1.929	50.90
15.80	0.665862 0.3	-0.146705 0.05	3.16	0.5175 0.01	207.90	0.6548 0.0	1.929	50.88
15.90	0.685762 0.3	-0.151682 0.05	2.85	0.5225 0.01	206.25	0.6679 0.0	1.929	50.86
16.00	0.695872 0.3	-0.157273 0.05	2.53	0.5258 0.01	204.68	0.6801 0.0	1.929	50.84
16.10	0.711652 0.3	-0.162040 0.05	2.22	0.5276 0.01	203.18	0.6947 0.0	1.929	50.82
16.20	0.727818 0.3	-0.166488 0.05	1.90	0.5281 0.01	201.74	0.7093 0.0	1.929	50.80
16.30	0.744452 0.3	-0.170636 0.05	1.58	0.5276 0.01	200.37	0.7232 0.0	1.929	50.78
16.40	0.761487 0.3	-0.174504 0.05	1.27	0.5262 0.01	199.07	0.7413 0.0	1.929	50.76

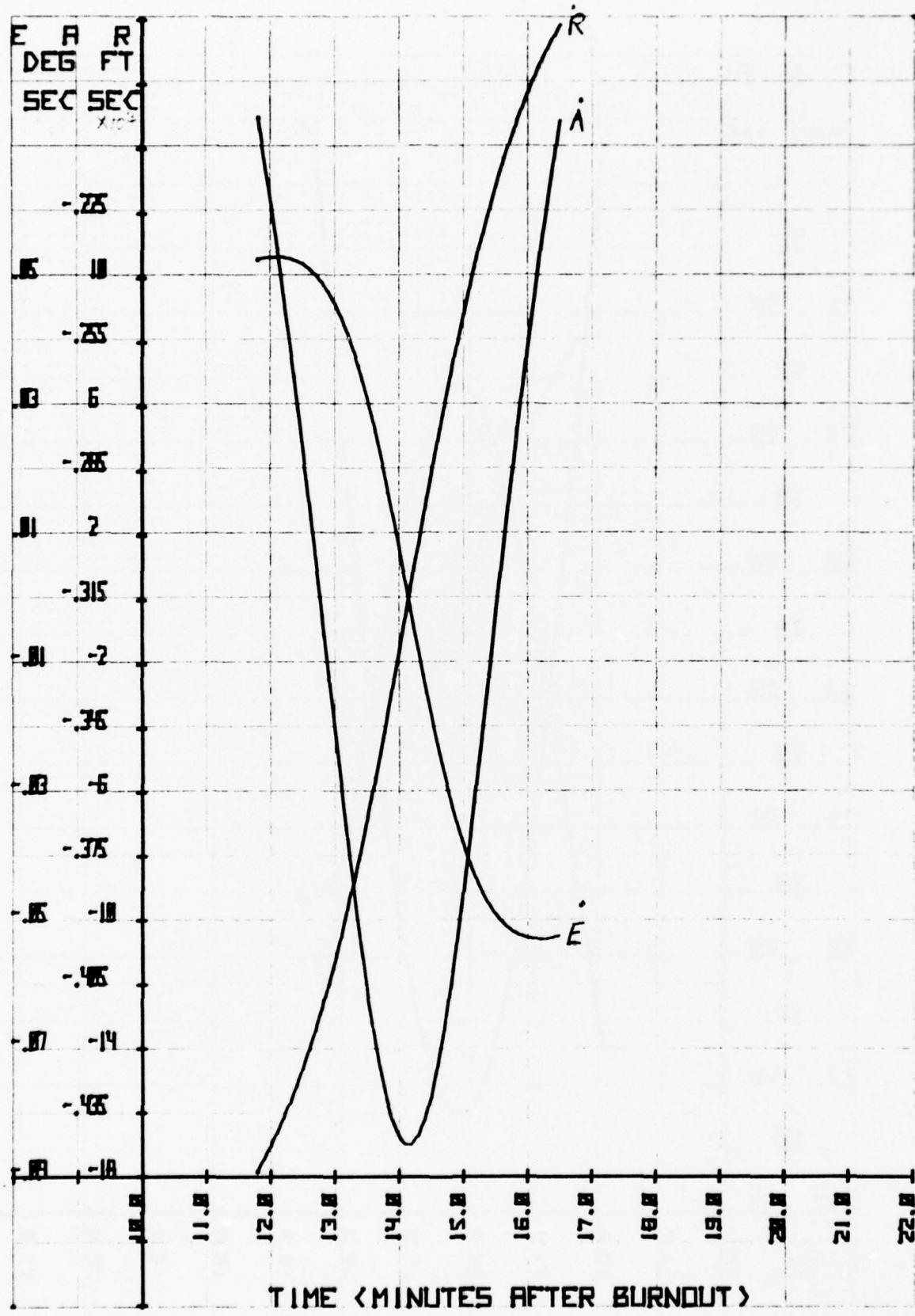
**Plots from the Sample Output**

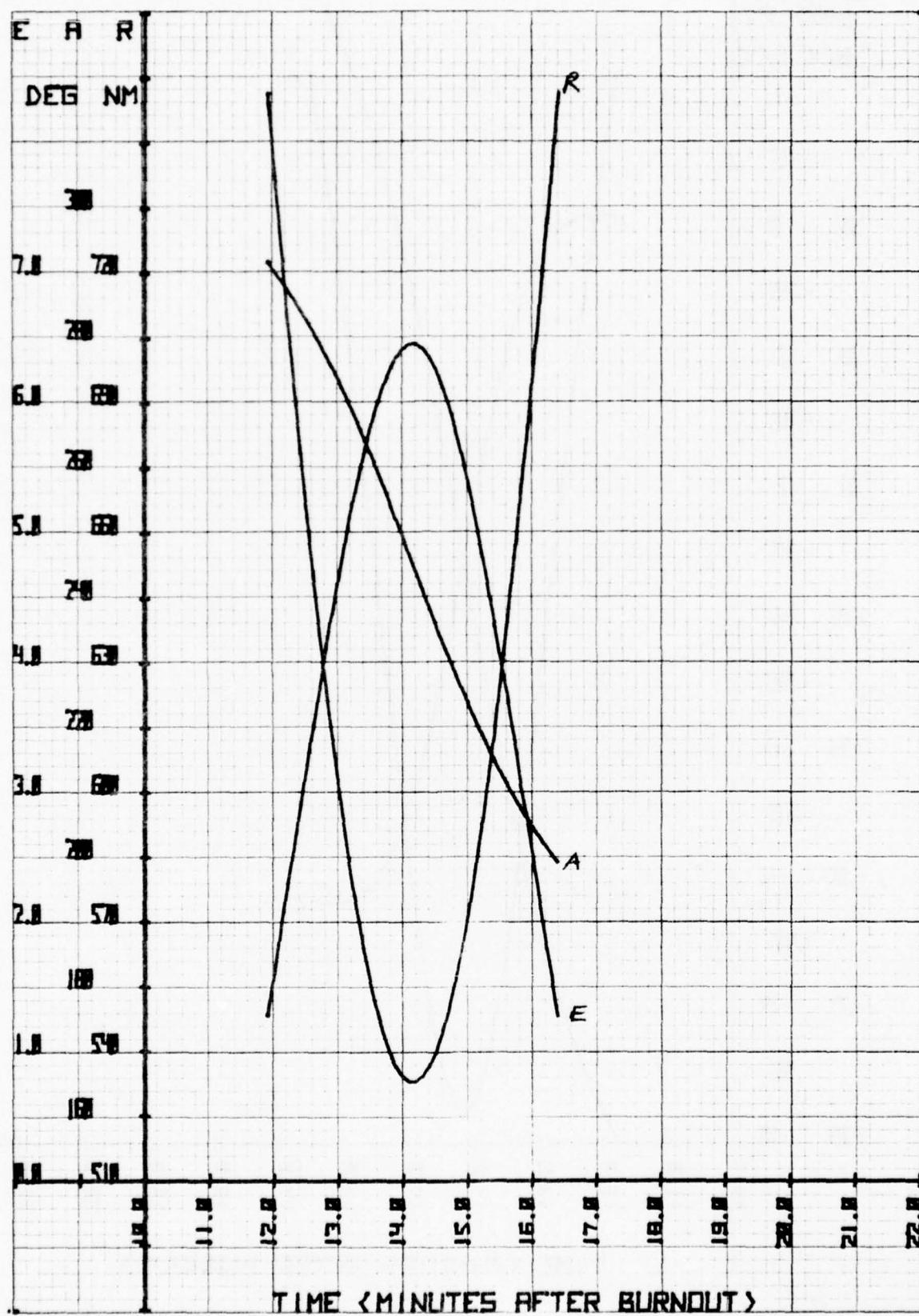
Traj. 1

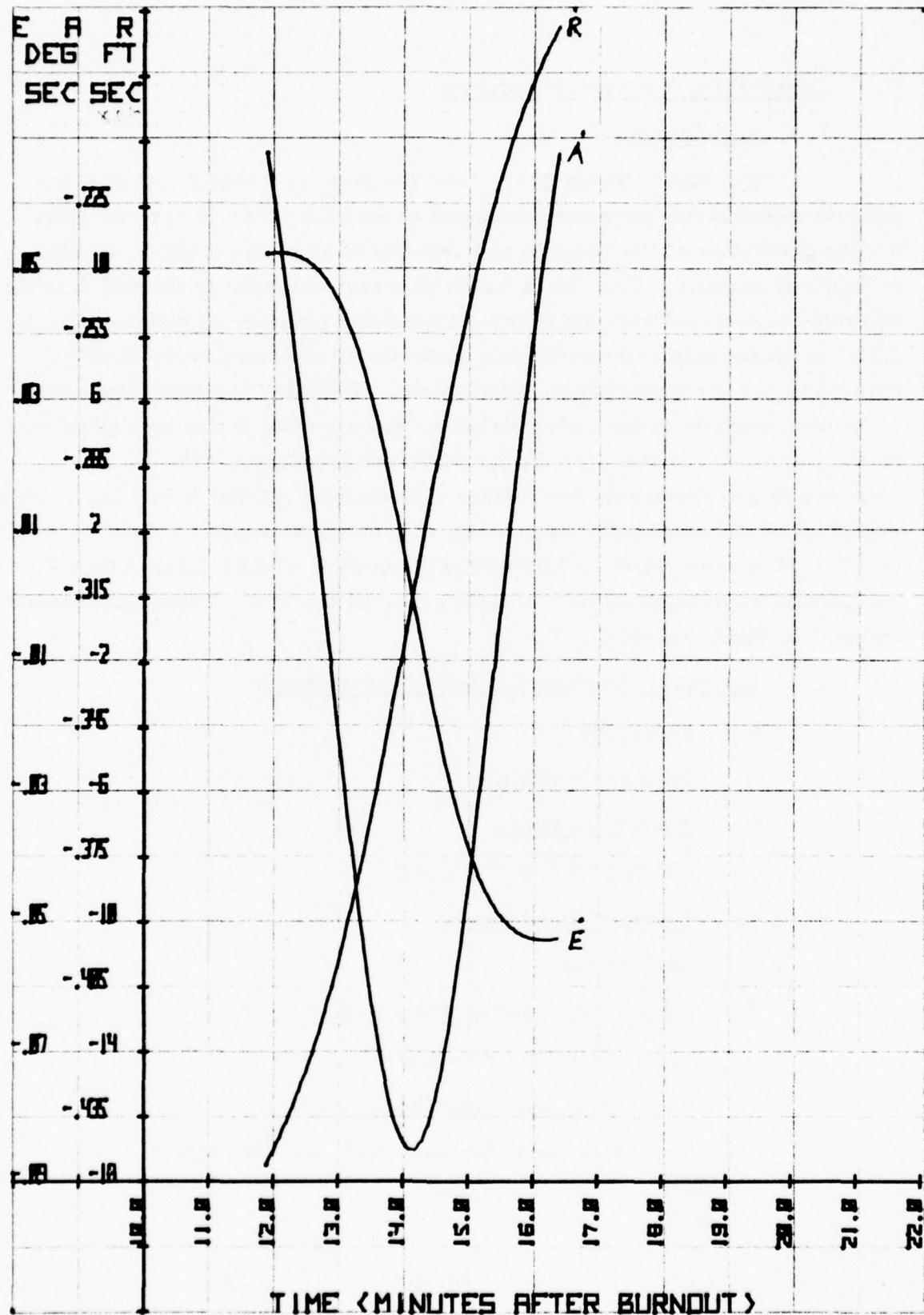












C. Cobra Talon Trajectory Program

1. Introduction

The Cobra Talon Trajectory Program is a modification of the general perturbation program developed at RADC by Mr. George A. Ellis for the prediction of the position and velocity of an earth-orbiting satellite or ballistic missile. The Cobra Talon program was used to furnish data for the study associated with the Cobra Talon radar project. It differs from Mr. Ellis' program primarily in the use of the first trajectory as the nominal trajectory for the perturbation calculations. PRC/ISC has made the necessary modifications to the Cobra Talon program so that it can be implemented on the interactive system for the RADC Radar Simulator. The reader is referred to two documents for further information: "COBRA TALON STUDY COMPUTER PROGRAMS," by John C. Cleary and Leonard C. Gratch, RADC/OC-TM-71-4, and "SIMULATION PROGRAM FOR THREE DEGREES OF FREEDOM TRAJECTORIES," by George A. Ellis, et al, Technical Memorandum No. EMA-TM-66-5.

2. Computer Program Operating Environment

a. Computer

Honeywell 6000.

b. Source Language

FORTRAN Y under GCOS.

c. Memory Requirement

16 K words

d. Typical Processing Time Required

0.25 hours (900 seconds)

e. Peripheral Equipment Requirement

Four disc files (file codes: 02, 03, 04, 07).

f. Non-system Subroutines Required

ATMOSP	Atmospheric model.
CONVER	Conversion of trajectory to radar coordinates.
EQTNX	Computation of acceleration components.
ICERBM	Performs initialization for trajectory computations.
INPUTT	Input subroutine.
OUTPUT	Stores trajectory data in an array for outputting.
PRINT2	Prints out trajectory and radar data.
RKG	Performs 4th order Runge-Kutta-Gill integration of equations of motion.
SAVE	Outputs trajectory and radar data onto files.

3. Inputs

The following is the set of input parameters required for the Cobra Talon Trajectory Program:

NAMELIST IN1

TM - Maximum forward trajectory run time (minutes)

TMI - Cut-off time for backwards trajectory (minutes)

NAMELIST IN2

CA - Surface range - dummy variable (degrees)

BETA - Missile heading angle measured clockwise from north (degrees).

GAM - Missile re-entry angle relative to vertical (degrees).

HX - Height of missile at burnout (feet), referenced to earth's surface.

NAMELIST IN3

KZ - Program control variable.

= 0 differences are calculated relative to third trajectory.

=1 differences are calculated relative to first trajectory.

NAMELIST IN4

ELIM - Maximum co-latitude of elevation angle for which radar coverage parameters are determined (degrees).

NAMELIST IN5

VO - Initial velocity of missile (ft. /min.).

INERTL - Initial velocity option variable.

=1, initial velocity is inertial velocity (SATELLITE orbit).

=0, initial velocity is burnout velocity (MISSILE trajectories)

NAMELIST IN6

ZK - ZK=g/2Bc (Bc=ballistic coefficient in lbs./ft.<sup>2</sup> and g=32.2 ft./sec.<sup>2</sup>), measured in ft.<sup>2</sup>/slugs.

KAT - Atmospheric model option variable.

=0, sets the atmospheric density to zero.

=1, use the atmospheric model.

NAMELIST IN7

A - Out of trajectory plane perturbation, + ejected to the left of nominal trajectory (ft./sec.)

B - In plane perturbation, + ejected backward from nominal trajectory (ft./sec.).

C - In plane perturbation, + ejected upwards from nominal trajectory (ft./sec.).

MM - MM=3 gives nominal trajectory, MM greater than 3 gives MM minus 3 perturbed trajectories.

NAMELIST IN8

SC1 - Radar latitude (positive north and negative south of equator) (degrees).

SC2 - Radar longitude west of Greenwich (degrees).

AH - Altitude above sea level of radar (feet).

NAMELIST IN9

GLAM - Launch longitude east of Greenwich (degrees).

THE - Launch latitude (positive north and negative south of equator in degrees).

GLAMI - Impact longitude east of Greenwich (degrees).

THEI - Impact latitude (positive north and negative south of equator, in degrees).

4. Output

Output from the Cobra Talon Trajectory Program first consists of a printout of the input data for the computer run. Secondly, the output consists of a printout of data generated for the first trajectory. This data is printed out as a list of trajectory parameters (e.g., radius, latitude, longitude, etc.) versus incremental trajectory time points (generally separated by 0.1 min. increments) from start time to end time. If the target, whose trajectory has been generated, is detected by a radar site, a listing of the radar parameters computed for the site, from initial time of detection to time of leaving coverage, is also produced. A description of the complete set of output quantities for the first trajectory follows:

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
Time	Min.	The time from burnout of the missile along its trajectory or time from the initiation of the satellite orbit, if that is appropriate.
Radius	Ft.	Earth-centered radius of the trajectory or the distance of the missile or satellite from the earth center at the time point above.
Latitude	Deg.	Position in latitude of the missile/satellite in its trajectory at the above time point.
Longitude	Deg.	Position in longitude of the missile/satellite, east of Greenwich.
Height	Ft.	Altitude above sea level of the missile.
Velocity	Ft./Sec.	Inertial velocity of the missile/satellite along its trajectory.

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
R(Sea Level)	Ft.	Radius of spherical earth model.
Density	Slugs/Ft. <sup>3</sup>	Atmospheric density.
R-Dot	Ft./Sec.	Geocentric radial component of velocity.
Lat. -Dot	Deg./Sec.	Geocentric latitude component of velocity.
Long. -Dot	Deg./Sec.	Geocentric longitude component of velocity.
R-Dot Dot	Ft./Sec. <sup>2</sup>	Geocentric radial component of acceleration.
Lat. -Dot Dot	Deg./Sec. <sup>2</sup>	Geocentric latitude component of acceleration.
Long. -Dot Dot	Deg./Sec. <sup>2</sup>	Geocentric longitude component of acceleration.

If the target of the first trajectory is detected by radar, the trajectory in terms of radar coordinates is printed out as follows:

Time	Min.	Same as for Time described above.
Slant Range	Ft.	Radar slant range to the missile/satellite for the time point.
S1 Range Rate	Ft./Sec.	Radar slant range rate.
S1 Range R Dot	Ft./Sec. <sup>2</sup>	Radar slant range acceleration.
Azimuth	Deg.	Radar azimuth look-angle to missile, measured clockwise from north.
Az Rate	Deg./Sec.	Radar azimuth angle rate.
Az R Dot	Deg./Sec. <sup>2</sup>	Radar azimuth angle acceleration.
Elevation	Deg.	Radar elevation look-angle to missile.
E1 Rate	Deg./Sec.	Radar elevation angle rate.
E1 R Dot	Deg./Sec. <sup>2</sup>	Radar elevation angle acceleration.
Reentry Angle	Deg.	Missile re-entry angle.
Heading	Deg.	Missile heading angle.

If more than one trajectory is generated in the computer run, the above set of trajectory data will be computed for the second, third, etc., trajectories also. Radar parameters for the targets corresponding to the trajectories will also be calculated, if the targets are detected.

Following the last set of trajectory and radar data, radar parameter differences may be calculated and printed out. These differences will be produced for each perturbed trajectory when MM is greater than or equal to 4. The parameter differences represent the values obtained by subtracting the radar parameters for the perturbed trajectories from the corresponding parameters for the nominal trajectory (trajectory #1 or #3). Below is a list of the output quantities comprising the radar parameter differences:

<u>Output Parameter</u>	<u>Units</u>	<u>Description</u>
Time	Min.	Same as for Time described previously.
Slant Range ( $\Delta R$ )	Ft.	Difference in radar slant range (nominal trajectory slant range - perturbed trajectory slant range).
Sl Range Rate ( $\Delta \dot{R}$ )	Ft./Sec.	Difference in radar slant range rate.
Sl Range Rate Dot ( $\Delta \ddot{R}$ )	Ft./Sec. <sup>2</sup>	Difference in radar slant range acceleration.
Azimuth ( $\Delta A$ )	Deg.	Difference in radar azimuth look-angle to missile.
Azimuth Rate ( $\Delta \dot{A}$ )	Deg./Sec.	Difference in radar azimuth angle rate.
Azimuth Rate Dot ( $\Delta \ddot{A}$ )	Deg./Sec. <sup>2</sup>	Difference in radar azimuth acceleration.
Elevation ( $\Delta E$ )	Deg.	Difference in radar elevation look-angle to missile.
Elevation Rate ( $\Delta \dot{E}$ )	Deg./Sec.	Difference in radar elevation angle rate.
Elevation Rate Dot ( $\Delta \ddot{E}$ )	Deg./Sec. <sup>2</sup>	Difference in radar elevation angle acceleration.
Angular Separation in Radar Beam	Deg.	Total angular separation in the radar beam.

The reader is referred to the sample output for an illustration of the printout format. The set of trajectory and radar parameters for the first trajectory only is included there, as is the set of radar parameter differences for the first perturbed trajectory only.

5. Sample Job Stream

The sample job stream on the following page is set up for producing plots of radar data from the first trajectory. This data is placed on file STORE1 and would be punched out onto cards for plotting by means of the Hewlett-Packard 9820A calculator/plotter if plots were desired. If plots are not wanted, line 80 of the job stream could be replaced by 0080\$; DISC: 02, X1R, 10L.

0010\$:IDENT:CLEARY,CONTI ,65121104RADC  
0020\$:USERID:CLEARY\$THREE  
0030\$:L0VL0AD  
0040\$:OPTIONJ:F0RTRAN  
0050\$:SELECT:CLEARY/0TRAJT  
0060\$:EXECUTE  
0070\$:LIMITS:40,16K,,15000  
0030\$:PRMFL:02,R/V,L,CLEARY/STORE1  
0090\$:DISC:03,X2R,50L  
0100\$:DISC:04,X3R,10L  
0110\$:DISC:07,X4R,10L  
0120\$:DATA:05  
0130 \$IN1  
0140 TM=44.0D0,  
0150 TMI = 0.0D0,  
0160 \$END  
0170 \$IN2  
0180 CA=91.5651D0,BETA=278.0D0,  
0190 GAM=55.0D0,HX=4.0D5,  
0200 \$END  
0210 \$IN3  
0220 KZ=1,  
0230 \$END  
0240 \$IN4  
0250 ELIM = 39.5D0,  
0260 \$END  
0270 \$IN5  
0280 V0=1.056D6,  
0290 INERTL=0,  
0300 \$END  
0310 \$IN6  
0320 ZK=0.321D-1,KAT=1,  
0330 \$END  
0340 \$IN7  
0350 A=7\*0.0D0,5.0D0,2\*3.533D0,  
0360 B=4\*0.0D0,5.0D0,3.533D0,-3.533D0,0.0D0,3.533D0,-3.533D0,  
0370 C=3\*0.0D0,5.0D0,0.0D0,2\*3.533D0,3\*0.0D0,  
0380 MM=8,  
0390 \$END  
0400 \$IN8  
0410 SC1=13.2D0,SC2=0.5333334D0,  
0420 AH = 0.0D0,  
0430 \$END  
0440 \$IN9  
0450 GLAM=27.0D0,THE=42.5D0,  
0460 GLAMI=60.0D0, THEI=-40.0D0,  
0470 \$END  
0480\$:ENDJOB  
0490\*\*\*EOF

Sample Job Stream for the Cobra Talon Trajectory Program

**RADC FORM 0-56** PREVIOUS EDITION WILL BE USED  
APR 69

HIS 6000 Batch Submittal Form

Source Listing of the Cobra Talon Trajectory Program

30667 81 01-07-76 15.345

C	PROGRAM TRAJ CONVERTED TALON CLEARY	00001000
	DOUBLE PRECISION X,XD,XDD,T0,TM	00001010
	DOUBLE PRECISION TC,TI,MM,TM	00001020
	DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q	00001030
	DOUBLE PRECISION ARRAY1	00001040
	DOUBLE PRECISION TN,STN	00001050
	DOUBLE PRECISION RADANG	00001060
	COMMON/TS/T,H,XYZ,RSL,PZ	00001070
	COMMON/A/R,W	00001080
	COMMON/ST/P(3),Q(3)	00001090
	COMMON/BS/X(3), XD(3), XDD(3)	00001100
	COMMON/AX/TM,M	00001110
	COMMON/ISW	00001120
	COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)	00001130
	COMMON/NTRAJ/MM	00001140
	COMMON/SW1/KZ	00001150
C	KZ .NE. 1 GIVES ORIGINAL PROGRAM	00001160
	CALL INPUTT	00001170
	ICTR = 3	00001180
	ISW = 0	00001190
	CALL FLGEOF (02,IEOFN)	00001200
	CALL FLGEOF (07,IEOFP)	00001210
	R = 20925640.00	00001220
	W=0.4375269048D-2	00001230
	MK=5.72951D1	00001240
	ITM * MM	00001250
4	DO 17 M = 1,ITM	00001260
	IF(KZ.NE.1) GO TO 540	00001270
	IF(M.EQ.2) GO TO 17	00001280
	IF(M.EQ.3) GO TO 17	00001290
540	CONTINUE	00001300
	CALL SAVE(Q)	00001310
	CALL ICERBM(R)	00001320
	DO 11 I=1,3	00001330
	P(I) = 0.0D0	00001340
11	G(I) = 0.0D0	00001350
	IF(M.EQ.2)GO TO 60	00001360
	FO=.1D-1	00001370
	IT=10	00001380
	KA=0	00001390
	KB=0	00001400
20	DO 16 K=1,60	00001410
	DO 1 K9=1,IT	00001420
	IF(H.LT.0.0D0)GO TO 2	00001430
9	CALL RKG(T0)	00001450
	T = T + FO	00001460
	CALL EQTNX	00001470
	IF(T-TM)1,2,2	00001480
1	CONTINUE	00001490
	IF(M.GE.3) GO TO 3	00001500
	CALL OUTPUT(K1)	00001510
	CALL CONVER	00001520

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IF(PZ,NE,0,000)GO TO 92	00001530
GO TO 16	00001540
92 IF(KA.EQ.1)GO TO 94	00001550
KA=1	00001560
KB=T	00001570
DO=.1D-2	00001580
IT = 1000	00001590
GO TO 16	00001600
94 IF(H-2.0D3)96,96,16	00001610
96 IF(KB.EQ.1)GO TO 18	00001620
KB=1	00001630
BT=T	00001640
DO=.1D-2	00001650
IT = 1000	00001660
GO TO 16	00001670
3 CALL OUTPUT(K1)	00001680
CALL CONVER	00001690
IF(PZ,NE,0,000)GO TO 62	00001700
GO TO 16	00001710
62 IF(H-2.0D3)63,63,64	00001720
63 DO=.1D-2	00001730
IT=1	00001740
DO TO 16	00001750
64 DO=.1D-2	00001760
IT = 1000	00001770
16 CONTINUE	00001780
GO TO 20	00001790
2 IF(M.EQ.1)GO TO 80	00001800
CALL PRINT2(1)	00001810
CALL PRINT2(-1)	00001820
GO TO 17	00001830
80 CALL PRINT2(1)	00001840
CALL PR1NT2(-1)	00001850
GO TO 17	00001860
80 DO=.1D-2	00001870
IT=1	00001880
70 DO 18 K6=1,60	00001890
DO 40 KB=1,IT	00001900
IF(T.LE.0.0D0)GO TO 86	00001910
DO TO 10	00001920
86 CALL PRINT2(1)	00001930
DO TO 17	00001940
10 CALL RKG(T0)	00001950
T = T+T0	00001960
CALL EQTNX	00001970
40 CONTINUE	00001980
CALL OUTPUT(K1)	00001990
TX=DABS(T-T1)	00002000
IF(TX.LE.,1D-4)GO TO 42	00002010
IF(T.LE.T1)GO TO 44	00002020
DO TO 18	00002030
42 IT=20	00002040

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10=-.1D-2	00002050
GO TO 18	00002060
44 TX=DABS(T-TC)	00002070
IF(TX,LE.,.3D-4) GO TO 46	00002080
GO TO 18	00002090
46 IT=10	00002100
IT=.1D-1	00002110
18 CONTINUE	00002120
GO TO 70	00002130
57 CONTINUE	00002140
22 END FILE 2	00002150
REWIND 2	00002160
END FILE 7	00002170
REWIND 7	00002180
READ (02) ARRAY	00002190
IF(IEOFN) 305,69,305	00002200
69 STN = ARRAY(1)	00002210
STN = STN	00002220
STT = ARRAY(1)	00002230
PRINT 330	00002240
330 FORMAT(1H1,/////////////////////////////66(2H# ),//38X,	00002250
*RADAR PARAMETER DIFFERENCES(PERTURBED-NOMINAL)",	00002260
*84/66(2H# ),/66(2H# ),/1H1)	00002270
PRINT 440,M	00002400
PRINT 340	00002410
PRINT 337	00002420
PRINT 999	00002430
PRINT 345	00002440
PRINT 336	00002450
PRINT 999	00002460
999 FORMAT(1H )	00002470
440 FORMAT(1H1,20X,5H M = ,I4)	00002480
340 FORMAT(1H0,4HTIME,4X,11HSLANT RANGE,7X,13HSL RANGE RATE,6X,17HSL R	00002490
1ANGE RATE DOT,7X,7HAZIMUTH,8X,12HAZIMUTH RATE)	00002500
345 FORMAT(1UX,16HAZIMUTH RATE DOT,4X,9HELEVATION,8X,14HELEVATION RATE	00002510
1UX,18HELEVATION RATE DOT)	00002520
310 READ (07) ARRAY1	00002530
IF(IEOPP) 200,204,200	00002540
204 STT1 = ARRAY1(1)	00002550
203 IF(STT.EQ.STT1) GO TO 250	00002560
IF(STT.GT.STT1) GO TO 210	00002570
214 READ (02) ARRAY	00002580
IF(IEOFN) 305,202,305	00002590
202 STT = ARRAY(1)	00002600
GO TO 203	00002610
305 ICTR = ICTR + 1	00002620
IF(ITM.EQ.ICTR) GO TO 200	00002630
PRINT 440,M	00002640
PRINT 340	00002650
PRINT 337	00002660
PRINT 999	00002670
PRINT 345	00002680

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PRINT 336          00002690
PRINT 999          00002700
387 FORMAT(2X,7HMINUTES,2X,4HFEET,14X,9HFEET/SEC,10X,12HFEET/SEC/SEC,00002710
$ 62X,7HDEGREES,5X,11HDEGREES/SEC) 00002720
336 FORMAT(10X,15HDEGREES/SEC/SEC,5X,7HDEGREES;10X,11HDEGREES/SEC,9X,15HDEGREES/SEC/SEC) 00002730
337 REWIND 2        00002740
CALL FLGEOF (02,IEOFN) 00002750
IF (STT,LE,STT1) GO TO 333 00002760
333 GO TO 201       00002770
333 READ (07) ARRAY1 00002780
IF (IEOFFP) 200,334,200 00002790
334 BT1=ARRAY1(1) 00002800
IF (STT,LE,STT1) GO TO 333 00002820
READ (02) ARRAY 00002830
IF (IEOFN) 305,335,305 00002840
335 BT1=ARRAY1(1) 00002850
GO TO 203         00002860
210 IF (SSTN,EQ,STT1) GO TO 212 00002870
GO TO 310         00002880
212 REWIND 2        00002890
CALL FLGEOF (02,IEOFN) 00002900
GO TO 214         00002910
250 DT = ARRAY(1) 00002920
DRS = - (ARRAY(2)-ARRAY1(2)) 00002930
DRSD = - (ARRAY(3)-ARRAY1(3)) 00002940
DRSDD = - (ARRAY(4)-ARRAY1(4)) 00002950
DSIG = - (ARRAY(5)-ARRAY1(5)) 00002960
DSIGD = - (ARRAY(6)-ARRAY1(6)) 00002970
DSIGDD = - (ARRAY(7)-ARRAY1(7)) 00002980
DEL = - (ARRAY(8)-ARRAY1(8)) 00002990
DELD = - (ARRAY(9)-ARRAY1(9)) 00003000
DELDD = - (ARRAY(10)-ARRAY1(10)) 00003010
RADANG = DSORT(DSIG**2 + DEL**2) 00003020
PRINT 350,DT,DRS,DRSD,DRSDD,DSIG,DSIGD,DSIGDD,DEL,DELD,DELDD 00003030
PRINT 700,RADANG 00003040
PRINT 999          00003050
700 FORMAT(1H0,36H ANGULAR SEPARATION IN RADAR BEAM = ,D22.10) 00003060
350 FORMAT(F7.3,2X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10/ 00003070
1      9X,D17.10,2X,D17.10,2X,D17.10,2X,D17.10) 00003080
201 READ (02) ARRAY 00003090
IF (IEOFN) 305,312,305 00003100
312 BT1 = ARRAY(1) 00003110
GO TO 310         00003120
200 BYOP          00003130
END              00003140
```

3520T B1 01-05-76 17.927

SUBROUTINE EQTNX	00003150
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q	00003160
DOUBLE PRECISION V6,EL2,EL3,EL4,EL5,EL6,AA	00003170
DOUBLE PRECISION DV,XYZ,ZK,S1,S2,S3,S4,S6,VA,VDD,VD,S23,Q1,Q2,Q3	00003180
DOUBLE PRECISION X,XD,XDD	00003190
DOUBLE PRECISION A,R,W	00003200
DIMENSION DV(5)	00003210
COMMON/BS/X(3),XD(3),XDD(3)	00003220
COMMON/TS/T,H,XYZ,RSL,PZ	00003230
COMMON/A/R,W	00003240
COMMON/EQATM0/ZK,KAT	00003250
DATA DV/2.42167*4D12;4*0.000/	00003260
S6=2.000	00003270
S1=DCOS(X(2))	00003280
S2=DSIN(X(2))	00003290
S3=DSIN(S6*X(2))	00003300
S4=DCOS(S6*X(2))	00003310
RSL = R	00003320
W= X(1)- RSL	00003330
IF(KAT.EQ.1) GO TO 21	00003340
20 PZ = 0.000	00003350
GO TO 30	00003360
21 CALL ATMOSP	00003370
30 VA = (XD(1)*XD(1))/(X(1)*X(1))+XD(2)*XD(2)*(S1*(XD(3)+W))**2	00003380
XYZ=X(1)*DSQRT(VA)	00003390
22 VDD= XD(1)*XD(1)+ X(1)*XD(2)*X(1)*XD(2)+(X(1)*(XD(3)-W)*S1)**2	00003400
VD=DSQRT(VDD)	00003410
S23=-PZ-ZK*VD	00003420
Q1= S23*XD(1)	00003430
S2= S23*XD(2)	00003440
S3= S23*(XD(3)-W)	00003450
V6 = R/X(1)	00003460
EL2=X(1)*XD(2)*XD(2)+0.5D0*(1.0D0+S4)*(W+XD(3))*(W+XD(3))*X(1)	00003470
EL3=DV(1)*X(1)*V6+DV(2)/X(1)*V6**3+3.0D0*S4-1.0D0	00003480
EL4=DV(3)/X(1)*V6**5*(35.0D0*S4*S4-10.0D0*S4-13.0D0)	00003490
XDD(1)= EL2-EL3-EL4+Q1	00003500
EL5=(-S6*XD(2)*XD(1))/X(1))-0.5D0*S3*(W+XD(3))*(W+XD(3))	00003510
EL6=-DV(4)/(X(1)*X(1))*V6**3+S3+DV(5)/(X(1)*X(1))*V6**5*S3*(1.0D0-0.0D0*S4)	00003520
17.0D0*S4)	00003530
XDD(2)=EL5+EL6+Q2	00003540
AA=-1.0D0*(W+XD(3))	00003550
XDD(3)=AA*- (S6*XD(1)/X(1))-AA*(S6*XD(2)*S23/S1**3)	00003560
RETURN	00003570
END	00003580

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```
SUBROUTINE ICERBM(P)          0 0 359
  DOUBLE PRECISION VO,RAT      0 0 359
  DOUBLE PRECISION RDP,RTDP,RLDP,C13,GMU,CA,GAM,BETA,GLAM,HX,THE,RO 0 0 361
  DOUBLE PRECISION X,XD,XDD    0 0 362
  DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,Q 0 0 363
  DOUBLE PRECISION P,GEO,GLAMD,ROD,THED 0 0 364
  DOUBLE PRECISION XN,XIN     0 0 365
  DOUBLE PRECISION COSGAM,COSHET,SINGAM,SINRET,V2,A,B,C 0 0 366
  DOUBLE PRECISION SNI,VBOOR,VDO 0 0 367
  COMMON/BS/X(3),XD(3),XDD(3) 0 0 368
  COMMON/TS/T,H,XYZ,RSL,PZ    0 0 369
  COMMON/A/R,W                0 0 370
  COMMON/IC/CA,BETA,GAM,HX,GLAM,THE,GLAM1,THE1 0 0 371
  COMMON/PTURB/A(2),B(2),C(2) 0 0 372
  COMMON/IC2/VO,INERTL        0 0 373
  COMMON/SW1/KZ                0 0 374
  COMMON/IC3/TM1              0 0 375
  DIMENSION RDP(2),RLDP(2),RTDP(2) 0 0 376
  DIMENSION XN(3),XDN(3)       0 0 377
  DIMENSION XN1(2),XDN1(2)     0 0 378
  DOUBLE PRECISION GLAM1,THE1 0 0 379
  DOUBLE PRECISION TM1       0 0 380
  DOUBLE PRECISION TN,STM,TM 0 0 381
  COMMON/AX/TM,M               0 0 382
  C13=0.717453292519943205769237 0 0 383
  GMU=5.167514019               0 0 384
  RO = R + HX                  0 0 385
  IF(M=2)6,1,15                0 0 386
6  CONTINUE
  XD(1)=VO*DCOS(GAM*C13)      0 0 387
  XD(2)=VO/RO*DSIN(GAM*C13)*DCOS(BETA*C13) 0 0 388
  RAT=RO*DCOS(THE*C13)         0 0 389
  XD(3)=VO*DSIN(GAM*C13)*DSIN(BETA*C13)/RAT 0 0 390
  IF(INERTL.EQ.1)XD(3)=XD(3)-W 0 0 391
  X(1)=RD 0 0 392
  X(2)= THE*C13 0 0 393
  X(3)= GLAM*C13 0 0 394
4  CALL EQTNX                  0 0 395
  CALL CONVER                  0 0 396
  CALL OUTPUT(K)               0 0 397
  IF(KZ.NE.1) GO TO 3 0 0 398
  DO 32 I=1,3 0 0 399
  XN(I)=X(I) 0 0 400
  XDN1(I)=XD(I) 0 0 401
32  CONTINUE 0 0 402
30  CONTINUE 0 0 403
  TN=TM 0 0 404
  RETURN
C   TARGET LOCATION
10  CONTINUE 0 0 405
  X(2)=THE*I*C13 0 0 406
  X(3)=GLAM*I*C13 0 0 407
                                         0 0 408
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```
TM = TMI  
CALL OUTPUT(K)  
RETURN  
16 T=0.0D0  
TM= TN  
IF(M.GT.3) GO TO 20  
DO 18 I = 1,3  
XN(I) = X(I)  
XDN(I) = XD(I)  
18 CONTINUE  
CALL EQTNX  
CALL OUTPUT(K)  
RETURN  
20 IF(KZ.NE.1) GO TO 35  
DO 25 I=1,3  
X(I) = XN1(I)  
XD(I) = XDN1(I)  
XN(I) = XN1(I)  
XDN(I) = XDN1(I)  
25 CONTINUE  
GO TO 45  
35 X(I) = XN(I)  
45 CONTINUE  
SN1 = DCOS(XN(2)*C13)  
VBODR = DSQRT((XDN(1)/XN(1))**2 + XDN(2)*XDN(2)+(SN1*XDN(3))**2) 0004330  
VBO = XN(1) * VBODR 0004340  
BETA = DATAN2(XDN(3)*SN1 , XDN(2)) 0004350  
COSBET = DCOS(BETA) 0004360  
SINBET = DSIN(BETA) 0004370  
COSGAM = XDN(1) / VBO 0004380  
SINGAM = XDN(2) / (VBODR * COSBET) 0004390  
V2 = B(M)*SINGAM+C(M)*COSGAM 0004400  
RDP(M) = (-B(M)*COSGAM+C(M)*SINGAM)*60.0D0 0004410  
RTDP(M) = (-V2*COSBET-A(M)*SINBET)*60.0D0 0004420  
RLDP(M) = (-V2*SINBET+A(M)*COSBET)*60.0D0 0004430  
XD(1) = XDN(1) + RDP(M) 0004440  
XD(2) = XDN(2) + RTDP(M)/XN(1) 0004450  
RATN = XN(1)* DCOS(XN(2)*C13) 0004460  
XD(3) = XDN(3) + RLDP(M)/RATN 0004470  
CALL EQTNX 0004480  
CALL CONVER 0004490  
CALL OUTPUT(K) 0004500  
RETURN 0004510  
END 0004520
```

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SUBROUTINE ATMO\$P	00004530
DOUBLE PRECISION HP,H2P,SK3,HB,PB,SK1,SK2,CD,ST	00004540
DOUBLE PRECISION TS,T,H,V,RSL,PZ,XYZ	00004550
COMMON/TS/T,H,XYZ,RSL,PZ	00004560
HP=.3048D+H	00004570
H2P=HP/(1.0D0+HP/6.356766D7)	00004580
IF(HP-.3D4)20,25,25	00004590
20 IF(HP-.7D4)21,29,29	00004600
21 IF(HP-.25D4)22,31,30	00004610
22 IF(HP-.1D4)23,31,31	00004620
23 IF(HP)28,28,32	00004630
25 IF(HP-.7D4)33,33,26	00004640
26 IF(HP-.1D4)34,34,27	00004650
27 IF(HP-.5D5)35,35,28	00004660
28 PZ=0.0D0	00004670
C1=0.0D0	00004680
C2=0.0D0	00004690
C3=0.0D0	00004700
RETURN	00004710
29 SK3=.120869D-3	00004720
HB=4.7D4	00004730
PB=2.8804D-6	00004740
GO TO 37	00004750
30 SK1=.138466D-4	00004760
SK2=1.13883D1	00004770
PB=7.765D-5	00004780
HB=2.5D4	00004790
GO TO 36	00004800
31 SK3=.157689D-3	00004810
HB=1.1D4	00004820
PB=7.062D-4	00004830
GO TO 37	00004840
32 SK1=-0.225569D-4	00004850
SK2=-5.25612D-1	00004860
PB=2.37692D-3	00004870
HB=0.0D1	00004880
GO TO 36	00004890
33 SK1=-0.15927D-4	00004900
SK2=-7.59218D-1	00004910
PB=1.39456D-6	00004920
HB=5.3D4	00004930
GO TO 36	00004940
34 SK3=.216234D-3	00004950
HB=7.9D4	00004960
PB=4.1169D-8	00004970
GO TO 37	00004980
35 SK1=.241458D-4	00004990
SK2=8.5412D-1	00005000
PB=4.261D-9	00005010
HB=9.0D4	00005020
36 CD=1.0D0+SK1*(42D-HB)	00005030
ST=-(1.0D0+SK2)	00005040

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RZ= PB*(CD**ST)	00005050
RETURN	00005060
37 RZ=PB*DEXP1-SK3*(H2P+HB)	00005070
RETURN	00005080
END	00005090

3684T 51 01-05-76 18.495

SUBROUTINE OUTPJT(K)	00005100
DOUBLE PRECISION CC	00005110
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,O	00005120
DOUBLE PRECISION X,XD,XDD	00005130
DOUBLE PRECISION Y,ARRAY1	00005140
COMMON/T5/T,H,XYZ,RSL,PZ	00005150
COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)	00005160
COMMON/B5/X(3),XD(3),XDD(3)	00005170
DATA CC/57.295779513,8232 876798155/	00005180
ARRAY(1)=T	00005190
ARRAY(2)=X(1)	00005200
ARRAY(3)= X(2)*CC	00005210
ARRAY(4)= X(3)*CC	00005220
ARRAY(5)=H	00005230
ARRAY(6)=XYZ/.6D2	00005240
ARRAY(7)=RSL	00005250
ARRAY(8)=PZ	00005260
ARRAY(9)=XD(1)/ .6D2	00005270
ARRAY(10)=XD(2)*CC/.6D2	00005280
ARRAY(11)=XD(3)*CC/.6D2	00005290
ARRAY(12)=XD(1)/ .36D4	00005300
ARRAY(13)=XD(2)*CC/.36D4	00005310
ARRAY(14)=XD(3)*CC/.36D4	00005320
CALL SAVE (1)	00005330
RETURN	00005340
END	00005350

66947 01 01-06-76 .9.489

SUBROUTINE SAVE (N)	00005360
DOUBLE PRECISION SC1,SC2,ARRAY1	00005370
COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)	00005380
IF(N)2,3,1	00005390
3 MAX1= 0	00005400
MAX2= 0	00005410
REWIND 3	00005420
REWIND 4	00005430
RETURN	00005440
1 WRITE (3) ARRAY	00005450
MAX1=MAX1+1	00005460
RETURN	00005470
2 WRITE (4) ARRAY	00005480
MAX2=MAX2+1	00005490
RETURN	00005500
END	00005510

6711T 01 01-06-70 9.573

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SUBROUTINE PRINT2(N)          0 05520
  DOUBLE PRECISION ARRAY,SC1,SC2,ARRAY1      0105530
  COMMON/SW1/XZ      00015540
  COMMON/AX/TM,9      01015550
  COMMON/PARAM/ARRAY(2^),MAX1,MAX2,SC1,SC2,ARRAY1(2^) 00005560
  DOUBLE PRECISION TM      00015570
  IF(N)2,1,1      00015580
  1  REWIND 3      00015590
  IFLAG=0      010 5600
  DO 3 I=1,MAX1      010 5610
  IF(IFLAG.NE.0) GO TO 5      01005620
  14  PRINT 10,2      010 5630
 1002  FORMAT(1H1,2X,4HTIME,7X,6HRADIUS,12X,6HLATITUDE,7X,9HLONGITUDE,
    112X,6HHEIGHT,11X,8HVELOCITY,9X,12HR(SEA LEVEL),8X,7HDENSITY,//)
  IFLAG=52      000 5650
  5  READ (3) ARRAY      00005660
  PRINT 10,1,(ARRAY(J),J=1,8)      00005670
 1000  FORMAT(1X,F8.4,F1X,D17.10,2X,D14.7,2X,D16.9,2X,D15.9,
    *2X,D17.1),1X,
    1D17.10,2X,D14.7)      00005680
  3  IFLAG=IFLAG-1      00005690
  REWIND 3      01015700
  IFLAG=0      01015710
  DO 4 I=1,MAX1      01015720
  IF(IFLAG.NE.0) GO TO 7      01015730
  6  PRINT 10,3      00015740
 1003  FORMAT(1H1,2X,4HTIME,9X,5HR-DOT,13X,6HLAT,-DOT,8X,9HLONG,-DOT,
    110X,6HR-DOT DOT,9X,12HLAT,-DOT DOT,8X,13HLONG,-DOT DOT,//)
  IFLAG=52      00005770
  7  READ (3) ARRAY      00005780
  PRINT 10,1,ARRAY(1),(ARRAY(J),J=9,14)      00005790
 1001  FORMAT(F8.4,2X,D16.9,4X,D13.6,4X,D13.6,4X,D16.9,4X,D16.7,4X,D16.7,
    14X,D16.7)      00005800
  4  IFLAG=IFLAG-1      010 5810
  RETURN      000 5820
  2  REWIND 4      00005830
  IFLAG=1      010 5840
  DO 10 I=1,MAX2      010 5850
  IF(IFLAG.NE.0) GO TO 9      010 5860
  8  PRINT 10,8,SC1,SC2      010 5870
 1008  FORMAT(1H1,5SX,16HSENSOR-LATITUDE ,F9.5,5X,13HLONGITUDE(W),
    1F10.5,/)      010 5880
  PRINT 10,4      010 5890
 1004  FORMAT(2X,9HTIME(MIN),7X,15HSLANT RANGE(FT),3X,21HSL RANGE RATE(FT/SEC),
    1/SEC),3X,25HSL RANGE RDOT(FT/SEC/SEC),3X,12HAZIMUTH(DEG),3X,
    216HAZ RATE(DEG/SEC))      010 5900
  IFLAG=52      010 5910
  9  READ (4) ARRAY      010 5920
  PRINT 10,5,(ARRAY(J),J=1,6)      010 5930
 1005  FORMAT(F8.4,   D21.12,D21.12,D24.12,5X,D16.9,4X,D12.5)      010 5940
  10  IFLAG=IFLAG-1      00005950
  REWIND 4      00005960
  IFLAG=0      010 5970
  9  READ (4) ARRAY      010 5980
  PRINT 10,5,(ARRAY(J),J=1,6)      010 5990
 1005  FORMAT(F8.4,   D21.12,D21.12,D24.12,5X,D16.9,4X,D12.5)      010 6000
  10  IFLAG=IFLAG-1      00006010
  REWIND 4      00006020
```

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1	IFLAG=1	00006030
2	DO 11 I=1,MAX2	00006040
3	IF(IFLAG,NE,0)GO TO 13	00006050
4	12 PRINT 10,6	00006060
5	1006 FORMAT(1H1,2X,9HTIME(MIN),2X,20HAZ RDOT(DEG/SEC/SEC),3X,14HELEVATI	00006070
6	10N(DEGT,5X,16HEL RATE(DEG/SEC),3X,2HREL RDOT(DEG/SEC/SEC),2X,13HRE	00006080
7	20NTRY ANGLE,6X,7HHEADING)	00006090
8	13 IFLAG=52	00006100
9	13 READ (4)ARRAY	00006110
10	13 PRINT 1007,ARRAY(1),(ARRAY(J),J=7,12)	00006120
11	1007 FORMAT(F8.4, D19.8,7X,D16.7,5X,D16.7,D23,12,4X,D12.6,4X,D12.6)	00006130
12	11 IFLAG=IFLAG-1	00006140
13	12 PRINT 1010	00006150
14	1010 FORMAT(53X,13HEN OF OUTPUT)	00006160
15	14 RETURN	00006170
16	15 END	00006180

```

SUBROUTINE CONVER          000 6190
DOUBLE PRECISION CS,SS,XS,YS,ZS,SRS,DSPS,RS,RSD,XNUM1,XNUM2,XNUM3 000 6200
DOUBLE PRECISION COST,COSL,SINT,SINL,EX,Y,Z,EXD,YD,ZD,XDR,YDP,ZDP 000 6210
DOUBLE PRECISION TWOP1,EF,F,REQ,BK2,BK3,BK4,AK,W2,W3,W4,W5,FT,FT2 000 6220
DOUBLE PRECISION XNUM,XMUM,S1K,W9,S2K,S3K,S1K2,S2K2,OPS,E,W7    000 6230
DOUBLE PRECISION XNLM,ED,SIG,W14,W15,SIGD,RSDD,SIGDD,EDD      000 6240
DOUBLE PRECISION ARRAY,SC1,SC2,T,H,XYZ,RSL,PZ,R,W,P,O      000 6250
DOUBLE PRECISION X,XD,XDD          000 6260
    DOUBLE PRECISION AH,ACTAG1, ACTAG2, ACTAG3      000 6270
DOUBLE PRECISION EL,ELD,ELDD      000 6280
DOUBLE PRECISION TN,STN,TM      000 6290
DOUBLE PRECISION ARRAY1      000 6300
DOUBLE PRECISION PI,HALFPI,THAPI,ARSIN,COSLT,GNUM,GDEM,BETA,GAM 000 6310
DOUBLE PRECISION AH,XPIM,VPRIME,GNUM2,COSB      000 6320
    DOUBLE PRECISION ELIM      000 6330
    COMMON/COEL/E_IM      000 6340
COMMON ISW          000 6350
COMMON/PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20) 000 6360
COMMON/TB/T+H,XYZ,RSL,PZ      000 6370
COMMON/BS/X(3),XD(3),XDD(3)      000 6380
COMMON/AX/TM,M      000 6390
    COMMON/SW1/KZ      000 6400
    COMMON/CONV/AH      000 6410
    COMMON/CONV/IK,JK      000 6420
COST=DCOS(X(2))      000 6430
COSL=DCOS(X(3))      000 6440
EF=57.295779513 8232.876798155      000 6450
F=0.0D0      000 6460
RE=20925640.0      000 6470
BK2=3.3726718220-3      000 6480
BK3=5.687349290-5      000 6490
BK4=1.26.515570-8      000 6500
AK =0.017453292519943295769237      000 6510
PI = 3.141592653589793238462643400      000 6520
HALFPI = PI/2.0D0      000 6530
THAPI = 1.5D +PI      000 6540
TWOP1 = 2.0D0 +PI      000 6550
SINT=DSIN(X(2))      000 6560
SINL=DSIN(X(3))      000 6570
EX =X(1)*COST*COSL      000 6580
Y =-X(1)*COST*SINL      000 6590
Z =X(1)*SINT      000 6600
EXD =XD(1)*COST*COSL-X(1)*XD(2)*SINT*COSL-X(1)*XD(3)*COST*SINL 000 6610
YD =-XD(1)*COST*SINL+X(1)*XD(2)*SINT*SINL-X(1)*XD(3)*COST*COSL 000 6620
ZD =XD(1)*SINT+X(1)*XD(2)*COST      000 6630
XD2=(XD(1)-X(1)*(XD(2)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*COSL 000 6640
1 -(2. D0*XD(1)*XD(2)+X(1)*XD(2))*SINT*COSL      000 6650
2 -(2. D0*XD(1)*XD(3)+X(1)*XD(3))*COST*SINL      000 6660
3 +2. D0*X(1)*XD(2)*XD(3)*SINT*SINL      000 6670
YD2=-(XD(1)-X(1)*(XD(1)*XD(2))-X(1)*(XD(3)*XD(3)))*COST*SINL 000 6680
1 +(2. D0*XD(1)*XD(2)+X(1)*XD(2))*SINT*SINL      000 6690
2 -(X(1)*XD(3)+2. D0*X(1)*XD(3))*COST*COSL      000 6700

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```

3      +2.0DU*X(1)*XD(2)*XD(3)*SINT*COSL          00006710
      1DP=(XDD(1)-X(1)*XD(2)*XD(2))/SINT          00006720
1      +(2.0DU*X(1)*XD(2)+X(1)*XDD(2))*COST        00006730
W2=DSIN(SC1*AK)                                00006740
W3=DCOS(SC1*AK)                                00006750
W4=DSIN(SC2*AK)                                00006760
W5=DCOS(SC2*AK)                                00006770
FT=(1.0DU-F)**2                                00006780
FT2=(2.0DU-F)**2                                00006790
ES=REQ/(DSQRT(1.0DU-FT2*W2**2))              00006800
SS=(CS*FT)+AH                                  00006810
WS=(CS+AH)*W3*45                               00006820
YS=(CS+AH)*W3*44                               00006830
ZS=SS*W2                                      00006840
RS=DSQRT(XS**2+YS**2+ZS**2)                  00006850
DPS=0.000                                     00006860
S1K=-((EX-XS)*W2*W5+(Y-YS)*W2*W4-(Z-ZS)*W3) 00006870
W9=SC2*AK                                      00006880
S2K=X(1)*COST*DSIN(X(3)+W9)                  00006890
S3K=(EX-XS)*W3*W5+(Y-YS)*W3*W4+(Z-ZS)*W2    00006900
S1K2=S1K**2                                    00006910
S2K2=S2K**2                                    00006920
S3K2=S3K**2                                    00006930
RS=DSQRT(S1K2+S2K2+S3K2)                    00006940
RSD=(EXD*(EX-XS)+YD*(Y-YS)+ZD*(Z-ZS))/RS   00006950
XNUM1=((EX-XS)*XS)/RS                        00006960
XNUM2=((Y-YS)*YS)/RS                        00006970
XNUM3=((Z-ZS)*ZS)/RS                        00006980
XNUM=(XNUM1+XNUM2+XNUM3)/SRS                00006990
XNUM=(XNUM1+XNUM2+XNUM3)*RS                 00007000
OPS=DSQRT(S1K2+S2K2)                         00007010
ACTAG1= OPS/S3K                                00007020
B*DATAN2(OPS,S3K)                            00007030
IF (M.EQ.3) GO TO 30                          00007040
IF(T.LT.TN) GO TO 200                         00007050
IF(E.LT.-.0D0.AND.ELIM.LT.99.0D0)GO TO 200  00007060
IF(E.LE.(ELIM*AK))GO TO 47                   00007062
GO TO 201                                     00007064
30 IF(E.LE.(ELIM*AK)) GO TO 40               00007070
GO TO 200                                     00007080
40 IF(ISW-NE.0) GO TO 47                      00007090
TN = T                                         00007100
ISW = 1                                         00007110
47 EL = TWOPI/4, D-E                           00007120
45 W6=DSIN(E)                                 00007130
W7=DCOS(E)                                 00007140
XNLM=XS*EXD+YS*YD+ZS*ZD                      00007150
ER=(-RS*XNLM+XMUM*RSD)/(SRS*(RS**2)*DSIN(E+DPS)) 00007160
ELD=-ED                                       00007170
65 ACTAG2= S2K/S1K                            00007180
SIG=DATAN2(S2K,S1K)                          00007190
IF(SIG.GE.0.000) GO TO 9                     00007200

```

90	$BIG = SIG + TWOPI$	00007210
	$W14 = DSIN(SIG)$	00007220
	$W15 = DCOS(SIG)$	00007230
	IF(DABS(W14).GE.1.0D-15.AND.W6.GT.0.0D0)GO TO 105	00007240
100	SIGD=0.000	00007250
	GO TO 110	00007260
105	$BIGD = (EXP*W2*W5 + YDP*W2*W4 - ZDP*W3 + (RSD*W6*RS*ED*W7)*W15)$	00007270
	$1/(RS*W6*W14)$	00007280
110	$XSUM1 = (XS/SRS)*(XDP/RS)$	00007290
	$XSUM2 = (YS/SRS)*(YDP/RS)$	00007300
	$XSUM3 = (ZS/SRS)*(ZDP/RS)$	00007310
	$XSUM = (XSUM1 + XSUM2 + XSUM3)/(DSIN(E+DSPS))$	00007320
	$RSDD = (((EX-XS)*XDP + (Y-YS)*YDP + (Z-ZS)*ZDP)$	00007330
1	$+ (EXD*EXD + YD*YD + ZD*ZD - RSD*RSD))/RS$	00007340
	$EDD = -XSUM + ((XNJM/DSIN(E+DSPS))*(RSDD/RS)) - (ED*ED*(DCOS(E+DSPS)$	00007350
1	$/DSIN(E+DSPS))) - (2.0D0*ED*(RSD/RS))$	00007360
	$ELDD = -EDD$	00007370
	IF(DABS(W14).GE.1.0D-16.AND.W6.GT.0.0D0)GO TO 108	00007380
	$BIGD = 0.0D0$	00007390
	GO TO 109	00007400
108	$SIGDD = (XDP*W2*W5 + YDP*W2*W4 - ZDP*W3 - 2.0D0*RSD*W6*W14*SIGD$	00007410
1	$- 2.0D0*RS*W7*W14*ED*SIGD - 2.0D0*RS*W6*W15*SIGD*SIGD$	00007420
2	$+ 2.0D0*RSD*W7*W15*ED + RSDD*W6*W15*RS*EDD*W7*W15)/(RS*W6*W14)$	00007430
109	SIGD= SIGD*EF	00007440
	EL=EL*EF	00007450
	ELD=ELD*EF/0.6D2	00007460
	ELDD=ELDD*EF/0.36D4	00007470
	BIG=SIG*EF	00007480
	SIGDD=SIGDD*EF	00007490
	ARRAY(1)=T	00007500
	ARRAY(2)= RS	00007510
	ARRAY(3)= RSD/0.6D2	00007520
	ARRAY(4)=RSDD/0.36D4	00007530
	ARRAY(5)=SIG	00007540
	ARRAY(6)=SIGD/0.6D2	00007550
	ARRAY(7)=SIGDD/0.36D4	00007560
	ARRAY(8)=EL	00007570
	ARRAY(9)=ELD	00007580
	ARRAY(10)=ELDD	00007590
C	CALCULATION OF HEADING ANGLE(CLOCKWISE 0 TO 2PI)	00007600
	COSLT = XD(3)*COST/XD(2)	00007610
	IF (XD(2)) 1,2,3	00007620
C	ZERO XD(2)	00007630
2	IF (COSLT) 4,5,6	00007640
C	NEGATIVE COSLT	00007650
4	BETA = TIHAPI	00007660
	GO TO 60	00007670
C	ZERO COSLT	00007680
5	BETA = 1.0D1*PI	00007690
	GO TO 60	00007700
C	POSITIVE COSLT	00007710
6	BETA = HALFPI	00007720

C	60 TO 60	00007730
C	NEGATIVE XD(2)	00007740
C	1 IF (COSLT) 9,8,9	00007750
C	NEGATIVE OR POSITIVE COSLT	00007760
C	9 BETA = PI + DATAN(COSLT)	00007770
C	60 TO 60	00007780
C	ZERO COSLT	00007790
C	8 BETA = PI	00007800
C	60 TO 60	00007810
C	POSITIVE XD(2)	00007820
C	3 IF (COSLT) 10,11,12	00007830
C	NEGATIVE COSLT	00007840
C	10 BETA = TWOPI + DATAN(COSLT)	00007850
C	60 TO 60	00007860
C	ZERO COSLT	00007870
C	11 BETA = 0.000D0	00007880
C	60 TO 60	00007890
C	POSITIVE COSLT	00007900
C	12 BETA = DATAN(COSLT)	00007910
C	CALCULATION OF RE/ENTRY ANGLE(CLOCKWISE & TG 2PI)	00007920
C	60 GNUM = X(1)*XD(2)	00007930
C	GDSB = DCOS(BETA)	00007940
C	GDEM = XD(1)*COSB	00007950
C	1F(GDEM) 13,14,15	00007960
C	ZERO GDEM	00007970
C	14 IF (GNUM) 16,17,18	00007980
C	NEGATIVE GNUM	00007990
C	16 ARSIN = TIHAPI	00008000
C	60 TO 62	00008010
C	ZERO GNUM	00008020
C	17 ARSIN = 1.0D1+PI	00008030
C	60 TO 62	00008040
C	POSITIVE GNUM	00008050
C	18 ARSIN = HALFPI	00008060
C	60 TO 62	00008070
C	NEGATIVE GDEM	00008080
C	19 IF (GNUM) 19,20,19	00008090
C	NEGATIVE OR POSITIVE GNUM	00008100
C	19 ACTAG3 = GNUM/GDEM	00008110
C	ARSIN = PI+DATAN(ACTAG3)	00008120
C	60 TO 62	00008130
C	ZERO GNUM	00008140
C	20 ARSIN = PI	00008150
C	60 TO 62	00008160
C	POSITIVE GDEM	00008170
C	19 IF (GNUM) 21,22,23	00008180
C	NEGATIVE GNUM	00008190
C	21 ACTAG3 = GNUM/GDEM	00008200
C	ARSIN=TWOPI + DATAN(ACTAG3)	00008210
C	60 TO 62	00008220
C	ZERO GNUM	00008230
C	22 ARSIN = 0.0D0	00008240

	GO TO 62	0308250
C	POSITIVE GNUM	0208260
23	ACTAG3 = GNUM/GDEM	0008270
	ARSIN = DATAN( ACTAG3 )	0008280
	GO TO 62	0008290
62	GAM = ARSIN	0208300
	GAM = GAM*EF	0008310
	ARRAY(11) = GAM	0208320
	BETA = BETA*EF	0008330
	ARRAY(12) = BETA	0208340
	IF(KZ.NE.1) GO TO 540	0008350
	IF(M.EQ.1) GO TO 190	0208360
	GO TO 640	0208370
540	IF(M.EQ.3) GO TO 190	0208380
640	CONTINUE	0008390
	WRITE(07) ARRAY	0208400
	GO TO 195	0008410
190	WRITE(02) ARRAY	0208420
195	CALL SAVE (-1)	0208430
200	RETURN	0208440
	END	0208450

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```
SUBROUTINE RKG(T0)          00008460
  DOUBLE PRECISION C,F,D,A,B,DEG,DXN,DXDX,DL,SAD,ABLE,BAKER 00008470
  DOUBLE PRECISION X,XD,XDD 00008480
  DOUBLE PRECISION P,Q 00008490
  DIMENSION C(4), F(4), D(4), A(3),B(3) 00008500
  COMMON /RS/ X(3),XD(3),XDD(3) 00008510
  COMMON /ST/ P(3), Q(3) 00008520
  DATA C/0.5D0,.2928932188,1.707106781,.1666666667/ 00008530
  DATA D/0.5D0,.2928932188,1.707106781,0.5D0/ 00008540
  DATA F/2.0D0,1.0D0,1.0D0,2.0D0/ 00008550
  BF=57.295779513,82320876798155 00008560
  DO 10 J=1,4 00008570
    CALL EOTNX
  DO 10 I=1,3 00008580
    A(I)=XD(I)
    B(I)=XDD(I)
    DXN=(A(I)-F(J)*B(I))*C(J) 00008590
    DXDX=(B(I)-F(J)*P(I))*C(J) 00008600
    DL=T0*DXN 00008610
    X(I)=X(I)+DL 00008620
    XD(I)=XD(I)+T0*DXDX 00008630
    S(I)=Q(I)+3.0D0*DXN-D(J)*A(I) 00008640
  10   P(I)=P(I)+3.0D0*DXDX-D(J)*B(I) 00008650
    SAD=X(3)-6.283185307179586476925287 00008660
    IF ( SAD ) 12,11,11 00008670
  11   X(3) = SAD 00008680
  12   RETURN 00008690
END 00008700
  00008710
  00008720
  00008730
```

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SUBROUTINE INPUTT	000 8740
COMMON/SW1/KZ	00008750
COMMON/AX/TM,MT	00008760
COMMON/IC/CA,BETA,GAM,HX,GLAM,THE,GLAMI,THEI	00008770
COMMON/IC2/V0,INERTL	00008780
COMMON/IC3/TMI	00008790
*PARAM/ARRAY(20),MAX1,MAX2,SC1,SC2,ARRAY1(20)	00008800
COMMON/THS/T,H,XYZ,RSL,PZ	00008810
COMMON/PTURB/A(20),B(20),C(20)	00008820
COMMON/CONV/AH	00008830
COMMON/NTRAJY/MM	00008840
COMMON/EQATMO/ZK,KAT	00008850
COMMON/CON/IK,JK	00008860
COMMON/COEL/E-LIM	00008870
DOUBLE PRECISION TM,CA,BETA,GAM,HX	00008880
DOUBLE PRECISION TMI	00008890
DOUBLE PRECISION A,B,C	00008900
DOUBLE PRECISION SC1,SC2,AH	00008910
*.ARRAY,ARRAY1	00008920
DOUBLE PRECISION T,H,XYZ,RSL,PZ	00008930
DOUBLE PRECISION ZK	00008940
DOUBLE PRECISION GLAM,THE,GLAMI,THEI	00008950
DOUBLE PRECISION V0	00008960
DOUBLE PRECISION E-LIM,EELIM	00008970
IK = 1	00008980
JK = 10	00008990
NAMELIST/IN1/TM,TMI	00009000
NAMELIST/IN2/CA,BETA,GAM,HX	00009010
NAMELIST/IN3/KZ	00009020
NAMELIST/IN4/E-LIM	00009030
*/IN5/V0,INERTL	00009040
NAMELIST/IN6/ZK,KAT	00009050
C KAT = 1 CALL ATMOSPHERE	00009060
C KAT = 0 SET ATMOSPHERIC DENSITY = U	00009070
NAMELIST/IN7/A,B,C,MM	00009080
C MM EQUAL 3 GIVES NOMINAL TRAJECTORY	00009090
C MM GREATER THAN 3 GIVES MM-3 PERTURBED TRAJECTORIES	00009100
NAMELIST/TNS/SC1,SC2,AH	00009110
NAMELIST/IN9/GLAM,THE,GLAMI,THEI	00009120
C GLAM = LAUNCH LONGITUDE **AND** THE = LAUNCH LATITUDE	00009130
C IN DEGREES	00009140
C GLAMI = IMPACT LONGITUDE **AND** TREI = IMPACT LATITUDE	00009150
C IN DEGREES	00009160
C FOR SOUTH LATITUDES USE A NEGATIVE THE OR TREI	00009170
C SENIOR LONGITUDE MEASURED WEST OF GREENWICH, ALL OTHER	00009180
C LONGITUDES ARE MEASURED WEST OF GREENWICH	00009190
READ(5,IN1)	00009200
IK=0	00009205
JK=0	00009206
READ(5,IN2)	00009210
READ(5,IN3)	00009220
READ(5,IN4)	00009230

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READ(5,IN5)	00009240
READ(5,IN6)	00009250
READ(5,IN7)	00009260
READ(5,IN8)	00009270
READ(5,IN9)	00009280
DELIM = 90,000-ELIM	00009290
WRITE(6,5)	00009300
WRITE(6,10) TM,TMI	00009310
WRITE(6,20) CA,HX	00009320
WRITE(6,30) BETA	00009330
WRITE(6,40) GAM,VO,INERTL	00009340
WRITE(6,50) ZK	00009350
WRITE(6,53) KAT	00009360
WRITE(6,140) CZ	00009370
WRITE(6,54)	00009380
WRITE(6,55) MM	00009390
WRITE(6,60)	00009400
WRITE(6,70)	00009410
WRITE(6,80) (A(NN),B(NN),C(NN),NN=1,20)	00009420
WRITE(6,90)	00009430
WRITE(6,100)	00009440
WRITE(6,110) SC1,SC2,AH	00009450
WRITE(6,120) GAM,THE	00009460
WRITE(6,130) GLAVI,THET	00009470
WRITE(6,150) EELIM	00009480
5 FORMAT(1H1,55X,"INPUTS")	00009490
10 FORMAT(1H0,34H MAXIMUM RUN TIME (FORWARD) TM = ,D16.8,4HMIN,,5X,300009500 *7H CUT-OFF TIME (BACKWARDS) TMI = ,D16.8,"MIN.")	00009510
20 FORMAT(1H0,21H SURFACE RANGE CA = ,D16.8,8H DEGREES,5X,16H ALTITU00009520 *DE HX = ,D16.8,5H FEET)	00009530
30 FORMAT(1H0,60H MISSILE HEADING ANGLE MEASURED CLOCKWISE FROM NORTH00009540 * BETA = ,D16.8,3H DEGREES)	00009550
40 FORMAT(1H1,22H REENTRY ANGLE GAM = ,D25.8,8H DEGREES,5X,24H INITI00009560 *AL VELOCITY VO = ,D25.18,7H FT/MIN,	00009570
*150X,"INERTL = ",I3.5X,	00009572
*768X,"IF INERTL = ,INITIAL VELOCITY IS BURNOUT VELOCITY",	00009574
*768X,"IF INERTL = 1,INITIAL VELOCITY IS INERTIAL VELOCITY")	00009576
50 FORMAT(1H1,2X,54ZK = ,D25.18,36H FT**2/SLUGS , BALLISTIC COEFFICI00009580 *ENT)	00009590
53 FORMAT(1H1,7H KAT = ,I2,I1X,55H NO ATMOSPHERE SET KAT = 0 , FOR AT00009600 *OSPHERE SET KAT = 1)	00009610
54 FORMAT(1H1,55H FOR CASE OF NO ATMOSPHERE, ATMOSPHERIC DENSITY PZ 00009620 * = 0)	00009630
55 FORMAT(1H1,64 M1 = ,I4)	00009640
60 FORMAT(1H1,45X,3JH PERTURBED VELOCITY COMPONENTS)	00009650
70 FORMAT(1H1,4X,3JH PERTURBATION TO LEFT = FT/SEC,9X,3JH PERTURBATI00009660 *ON BACKWARDS - FT/SEC,9X,3JH PERTURBATION UPWARDS - FT/SEC)	00009670
80 FORMAT(1H1,7X,D25.18,I5X,D25.18,I5X,D25.18)	00009680
90 FORMAT(1H1,39X,41H SENSOR'S COORDINATES IN DEGREES AND FEET)	00009690
100 FORMAT(1H1,10X,18H GEODETIC LATITUDE,12X,38H LONGITUDE, WEST OF GR00009700 *EENWICH MERIDIAN,8X,25H ALTITUDE ABOVE SEA-LEVEL)	00009710
110 FORMAT(1H1,7X,3(D25.18,15X))	00009720

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120 FORMAT(1H0,20H LAUNCH LONGITUDE = ,D25.18,5X,12H LATITUDE = ,D25.100019730  
\*8) 00009740  
130 FORMAT(1H0,20H IMPACT LONGITUDE = ,D25.18,5X,12H LATITUDE = ,D25.100009750  
\*8) 00009760  
140 FORMAT(1H0,1X,5H KZ = ,15) 00009770  
150 FORMAT(1H ,4X,3B3"LOWEST ELEVATION ANGLE PRINTED OUT" ,D12.4) 00009780  
RETURN 00009790  
END 00009800

**Listing of the Sample Input for the Program**



**Sample Output for the Cobra Talon Trajectory Program**

TIME	RADIUS	LATITUDE	LONGITUDE	HEIGHT	VELOCITY	RSEA LEVEL	DENSITY
0.	0.325640000	0.0	0.425000000	0.2	0.400000000	0.6	0.209256000
0.1000	0.213858002	0.0	0.425319000	0.2	0.460162080	0.6	0.209256400
0.2000	0.214451515	0.0	0.425629000	0.2	0.519511470	0.6	0.209256000
0.3000	0.215036918	0.0	0.425931500	0.2	0.578051859	0.6	0.209256400
0.4000	0.215614258	0.0	0.426223500	0.2	0.635255792	0.6	0.209256400
0.5000	0.216183607	0.0	0.426507700	0.2	0.690520142	0.6	0.209256400
0.6000	0.216744947	0.0	0.426837000	0.2	0.748279480	0.6	0.209256400
0.6800	0.217298342	0.0	0.427151600	0.2	0.798846490	0.6	0.209256400
0.7000	0.217298342	0.0	0.427315000	0.2	0.841943420	0.6	0.209256400
0.8000	0.217388400	0.0	0.427503950	0.2	0.858742342	0.6	0.209256400
0.9000	0.218381442	0.0	0.427563300	0.2	0.912501913	0.6	0.209256400
1.0000	0.218911156	0.0	0.427807200	0.2	0.965416262	0.6	0.209256400
1.1000	0.219433948	0.0	0.428243500	0.2	0.102334340	0.6	0.209256400
1.2000	0.219947216	0.0	0.428272000	0.2	0.112304621	0.6	0.209256400
1.3000	0.220453592	0.0	0.428494200	0.2	0.122742888	0.6	0.209256400
1.4000	0.220952227	0.0	0.4287099	0.2	0.124242124	0.6	0.209256400
1.5000	0.221443158	0.0	0.428913500	0.2	0.125941840	0.6	0.209256400
1.6000	0.221926432	0.0	0.4291120	0.2	0.126700310	0.6	0.209256400
1.7000	0.222402480	0.0	0.4293050	0.2	0.121867281	0.6	0.209256400
1.8000	0.222870480	0.0	0.4294899	0.2	0.121575460	0.6	0.209256400
1.9000	0.223350452	0.0	0.4296675	0.2	0.121283766	0.6	0.209256400
2.0000	0.223783292	0.0	0.4298383	0.2	0.120993322	0.6	0.209256400
2.1000	0.224228598	0.0	0.4301030	0.2	0.120703995	0.6	0.209256400
2.2000	0.224666352	0.0	0.4301619	0.2	0.120412826	0.6	0.209256400
2.3000	0.225096656	0.0	0.4303126	0.2	0.120127826	0.6	0.209256400
2.4000	0.225194752	0.0	0.4304565	0.2	0.119841054	0.6	0.209256400
2.5000	0.225934848	0.0	0.4305946	0.2	0.119555131	0.6	0.209256400
2.6000	0.226342810	0.0	0.4307263	0.2	0.119270011	0.6	0.209256400
2.7000	0.226433540	0.0	0.4308515	0.2	0.118985710	0.6	0.209256400
2.8000	0.227336521	0.0	0.4309780	0.2	0.118702314	0.6	0.209256400
2.9000	0.227522336	0.0	0.4311837	0.2	0.118137713	0.6	0.209256400
3.0000	0.227900812	0.0	0.4312912	0.2	0.117856561	0.6	0.209256400
3.1000	0.228271974	0.0	0.4313858	0.0	0.117576159	0.6	0.209256400
3.2000	0.22863584	0.0	0.4313859	0.2	0.117576159	0.6	0.209256400
3.3000	0.228924256	0.0	0.4314740	0.2	0.117296162	0.6	0.209256400
3.4000	0.229341753	0.0	0.4315575	0.2	0.117017960	0.6	0.209256400
3.5000	0.229683843	0.0	0.4316345	0.2	0.116739222	0.6	0.209256400
3.6000	0.231018714	0.0	0.4317050	0.2	0.116461633	0.6	0.209256400
3.7000	0.231343812	0.0	0.431761934	0.0	0.116184713	0.6	0.209256400
3.8000	0.231666848	0.0	0.4318310	0.2	0.115908515	0.6	0.209256400
3.9000	0.231980135	0.0	0.4318853	0.2	0.115632830	0.6	0.209256400
4.0000	0.232271427	0.0	0.4321040	0.2	0.115383680	0.6	0.209256400
4.1000	0.232486330	0.0	0.4321150	0.2	0.115083662	0.6	0.209256400
4.2000	0.232858315	0.0	0.4321210	0.2	0.114809880	0.6	0.209256400
4.3000	0.233230314	0.0	0.4321230	0.2	0.114809880	0.6	0.209256400
4.4000	0.233479753	0.0	0.4321263	0.2	0.113178979	0.6	0.209256400
4.5000	0.233722135	0.0	0.4321266	0.2	0.112900650	0.6	0.209256400
4.6000	0.233957599	0.0	0.4321213	0.2	0.112701968	0.6	0.209256400
4.7000	0.234186032	0.0	0.4321110	0.2	0.112370732	0.6	0.209256400
4.8000	0.234467865	0.0	0.4321044	0.2	0.249296044	0.7	0.209256400
5.0000	0.234711968	0.0	0.4321044	0.2	0.247011968	0.7	0.209256400
5.1000	0.234929604	0.0	0.4321044	0.2	0.249296044	0.7	0.209256400

TIME	RADIUS	LATITUDE	LONGITUDE	HEIGHT	VELOCITY	R(SEA LEVEL)	DENSITY
5.2000	0.23446218522D 08	0.432 9560 02	0.112022910 03	0.251510214D 07	0.1261818032D 05	0.20925640000 08	0.
5.3000	0.23446218522D 08	0.432 7510 02	0.11183313D 03	0.2316545790 07	0.12571460864D 05	0.20925640000 08	0.
5.4000	0.2348293245D 08	0.432 4950 02	0.111566792D 03	0.2557292570 07	0.12493238496D 05	0.20925640000 08	0.
5.5000	0.2350229835D 08	0.432 1880 02	0.111299713D 03	0.2577343420 07	0.1249151312D 05	0.20925640000 08	0.
5.6000	0.2352233592D 08	0.43198310 02	0.111033067D 03	0.259669942D 07	0.1245199668D 05	0.20925640000 08	0.
5.7000	0.235410164D 08	0.4319242D 02	0.110666840D 03	0.26636147D 07	0.1243704846D 05	0.20925640000 08	0.
5.8000	0.235589715D 08	0.43188670 02	0.110501922D 03	0.26333052D 07	0.1237704849D 05	0.20925640000 08	0.
5.9000	0.235762435D 08	0.4318660D 02	0.110356503D 03	0.266067042D 07	0.1234161668D 05	0.20925640000 08	0.
6.0000	0.235928325D 08	0.431793D 02	0.10920571D 03	0.266719308D 07	0.1230756355D 05	0.20925640000 08	0.
6.1000	0.236087532D 08	0.43172980 02	0.109705913D 03	0.27988832D 07	0.122448828D 05	0.20925640000 08	0.
6.2000	0.2362393315D 08	0.4316643D 02	0.10941622D 03	0.298293950 07	0.122435795D 05	0.20925640000 08	0.
6.3000	0.236384505D 08	0.4315940D 02	0.109717683D 03	0.21281046D 07	0.122136537D 05	0.20925640000 08	0.
6.4000	0.236522734D 08	0.4315187D 02	0.10984088D 03	0.272663888D 07	0.121851504D 05	0.20925640000 08	0.
6.5000	0.2366541284D 08	0.431436D 02	0.1095025D 03	0.23977974D 07	0.121322048D 05	0.20925640000 08	0.
6.6000	0.236778736D 08	0.4313537D 02	0.10887884D 03	0.25223376D 07	0.121322048D 05	0.20925640000 08	0.
6.7000	0.236896416D 08	0.4312639D 02	0.108125254D 03	0.27640144D 07	0.121078387D 05	0.20925640000 08	0.
6.8000	0.23701072552D 08	0.4311693D 02	0.107662924D 03	0.298345D 07	0.122448704D 05	0.20925640000 08	0.
6.9000	0.237111202D 08	0.43110D 02	0.107662884D 03	0.2856802D 07	0.120683304D 05	0.20925640000 08	0.
7.0000	0.2372083232D 08	0.4309628D 02	0.10739125D 03	0.29519241D 07	0.120431336D 05	0.20925640000 08	0.
7.1000	0.2372986049D 08	0.4308568D 02	0.1077734D 03	0.28022038D 07	0.12043744D 05	0.20925640000 08	0.
7.2000	0.237382448D 08	0.430743D 02	0.1086643D 03	0.2825646D 07	0.1200702916D 05	0.20925640000 08	0.
7.3000	0.237458656D 08	0.4306245D 02	0.1065254D 03	0.2822254D 07	0.1198102914D 05	0.20925640000 08	0.
7.4000	0.237528435D 08	0.4305012D 02	0.106294675D 03	0.2820336D 07	0.119765457D 05	0.20925640000 08	0.
7.5000	0.23759133956D 08	0.43037310 02	0.1064158D 03	0.285349862D 07	0.119634278D 05	0.20925640000 08	0.
7.6000	0.237647105D 08	0.430243D 02	0.1077386D 03	0.283011572D 07	0.119507725D 05	0.20925640000 08	0.
7.7000	0.2376968224D 08	0.43012427D 02	0.10513769D 03	0.28404236D 07	0.119414413D 05	0.20925640000 08	0.
7.8000	0.2377739312D 08	0.4296414D 02	0.105253876D 03	0.284829139D 07	0.119325730D 05	0.20925640000 08	0.
7.9000	0.23777493985D 08	0.429833D 02	0.10494171D 03	0.2849878D 07	0.1192512672D 05	0.20925640000 08	0.
8.0000	0.2378038445D 08	0.4296615D 02	0.104735644D 03	0.28574743D 07	0.119191008D 05	0.20925640000 08	0.
8.1000	0.2378258244D 08	0.4295010D 02	0.10445284D 03	0.28594940D 07	0.119144958D 05	0.20925640000 08	0.
8.2000	0.2378411294D 08	0.4293426D 02	0.104216082D 03	0.285847283D 07	0.119113134D 05	0.20925640000 08	0.
8.3000	0.237849552D 08	0.4291776D 02	0.10395028D 03	0.285031513D 07	0.119092196D 05	0.20925640000 08	0.
8.4000	0.23785115648D 08	0.4291668D 02	0.10369811D 03	0.285947638D 07	0.1190219216D 05	0.20925640000 08	0.
8.5000	0.2378459545D 08	0.4288312D 02	0.10343932D 03	0.285956551D 07	0.11910303D 05	0.20925640000 08	0.
8.6000	0.2378339552D 08	0.428658D 02	0.10380651D 03	0.28575555D 07	0.119128118D 05	0.20925640000 08	0.
8.7000	0.2378151328D 08	0.4284657D 02	0.10292088D 03	0.28587344D 07	0.119122037D 05	0.20925640000 08	0.
8.8000	0.237787950 8D	0.428258D 02	0.102663624D 03	0.286331004D 07	0.119202968D 05	0.20925640000 08	0.
8.9000	0.2377757528D 08	0.4288181D 02	0.102405247D 03	0.28606531D 07	0.119288708D 05	0.20925640000 08	0.
9.0000	0.23771779881D 08	0.4276774D 02	0.102188717D 03	0.28545310D 07	0.1191920676D 05	0.20925640000 08	0.
9.1000	0.2376717088D 08	0.4276774D 02	0.10188717D 03	0.2845310D 07	0.1194667296D 05	0.20925640000 08	0.
9.2000	0.237618015D 08	0.427463D 02	0.101650547D 03	0.28324102D 07	0.1195771088D 05	0.20925640000 08	0.
9.3000	0.23755938D 08	0.427254D 02	0.10132424D 03	0.281926886D 07	0.119715888D 05	0.20925640000 08	0.
9.4000	0.237492549D 08	0.4270356D 02	0.10111134D 03	0.282616420D 07	0.119840214D 05	0.20925640000 08	0.
9.5000	0.237419158D 08	0.426881D 02	0.100862284D 03	0.281627673D 07	0.119929298D 05	0.20925640000 08	0.
9.6000	0.23733895D 08	0.426583D 02	0.100598248D 03	0.280425609D 07	0.12015983D 05	0.20925640000 08	0.
9.7000	0.23725192D 08	0.426351D 02	0.10030220D 03	0.2795519D 07	0.1203407792D 05	0.20925640000 08	0.
9.8000	0.23715838D 08	0.426119D 02	0.100082191D 03	0.27916371D 07	0.12035794D 05	0.20925640000 08	0.
9.9000	0.237057312D 08	0.425868D 02	0.99824515D 02	0.27091210D 07	0.12044800D 05	0.20925640000 08	0.
10.0000	0.236949734D 08	0.4255626D 02	0.995680889D 02	0.27893356D 07	0.120967924D 05	0.20925640000 08	0.
10.1000	0.236835305D 08	0.4253675D 02	0.99307974D 02	0.27589056D 07	0.121204942D 05	0.20925640000 08	0.
10.2000	0.236714164D 08	0.4251095D 02	0.990498635D 02	0.27576156D 07	0.121455988D 05	0.20925640000 08	0.
10.3000	0.2365858592D 08	0.4248464D 02	0.987916787D 02	0.273294598D 07	0.1217208752D 05	0.20925640000 08	0.

TIME	RADIUS	LATITUDE	LONGITUDE	HEIGHT	VELOCITY	RISEA LEVEL	DENSITY
10.4860	0.23645083250	0.8	0.42457840	0.2	0.9853343230	0.2	0.20925640000 0.8
10.5000	0.23631892480	0.8	0.42430530	0.2	0.8827511420	0.2	0.12229237760 0.5
10.5000	0.23616013120	0.8	0.42402710	0.2	0.9801671550	0.2	0.20925640000 0.8
10.5000	0.2360044480	0.8	0.42374380	0.2	0.975822330	0.2	0.20925640000 0.8
10.8000	0.23584185920	0.8	0.42345540	0.2	0.9749962880	0.2	0.2658545280 0.7
10.8000	0.23567235480	0.8	0.42216190	0.2	0.9724092280	0.2	0.2658545280 0.7
11.0000	0.2354993520	0.8	0.42286310	0.2	0.9698209280	0.2	0.2623952070 0.7
11.0000	0.23531621120	0.8	0.42255920	0.2	0.9672312960	0.2	0.2605621240 0.7
11.1000	0.2351233920	0.8	0.42225500	0.2	0.9646402170	0.2	0.2586593120 0.7
11.1000	0.2349251200	0.8	0.42193560	0.2	0.9602476130	0.2	0.256682160 0.7
11.1000	0.2347219500	0.8	0.42161580	0.2	0.959453370	0.2	0.254645490 0.7
11.1000	0.23450981440	0.8	0.42129070	0.2	0.958573050	0.2	0.2525341370 0.7
11.1000	0.2342170240	0.8	0.42096120	0.2	0.9542594040	0.2	0.2503531300 0.7
11.1000	0.2340666080	0.8	0.42062430	0.2	0.95169595320	0.2	0.248102640 0.7
11.1000	0.2338351250	0.8	0.42028290	0.2	0.9490575870	0.2	0.2457811290 0.7
11.1000	0.2335941120	0.8	0.41993610	0.2	0.9464534400	0.2	0.2433901080 0.7
11.1000	0.2333929560	0.8	0.41953700	0.2	0.9438469880	0.2	0.2419268900 0.7
12.0000	0.23309613120	0.8	0.41922570	0.2	0.9412381180	0.2	0.2383973180 0.7
12.1000	0.23285512950	0.8	0.41886210	0.2	0.9386267130	0.2	0.2357953120 0.7
12.2000	0.23256665880	0.8	0.418494280	0.2	0.9360126840	0.2	0.2331226910 0.7
12.3000	0.2322943360	0.8	0.41811780	0.2	0.93313958910	0.2	0.23076762170 0.7
12.4000	0.2320291520	0.8	0.41737310	0.2	0.9307762170	0.2	0.22705651480 0.7
12.5000	0.23172393560	0.8	0.41735500	0.2	0.9281535740	0.2	0.2246795320 0.7
12.6000	0.23142599720	0.8	0.416655970	0.2	0.9226988280	0.2	0.221482170 0.7
12.7000	0.2311816740	0.8	0.41615540	0.2	0.9202665680	0.2	0.215596160 0.7
12.8000	0.23090816170	0.8	0.41574510	0.2	0.9176307200	0.2	0.212425940 0.7
12.9000	0.23063999200	0.8	0.41532860	0.2	0.9149191340	0.2	0.20981840480 0.7
13.0000	0.23041747350	0.8	0.41490600	0.2	0.9123482750	0.2	0.2058686800 0.7
13.1000	0.2295046140	0.8	0.41447720	0.2	0.9097013500	0.2	0.2024821470 0.7
13.2000	0.2291581680	0.8	0.41404220	0.2	0.9070504830	0.2	0.1993023160 0.7
13.3000	0.2288055680	0.8	0.41360380	0.2	0.904395070	0.2	0.1954916760 0.7
13.4000	0.228451320	0.8	0.41081560	0.2	0.9017363320	0.2	0.1927692440 0.7
13.5000	0.22807744640	0.8	0.412669870	0.2	0.8997028560	0.2	0.1918871200 0.7
13.6000	0.22770243520	0.8	0.41223790	0.2	0.8973321720	0.2	0.188210470 0.7
13.7000	0.2273209920	0.8	0.4117750	0.2	0.8902950520	0.2	0.1860363970 0.7
13.8000	0.22693041250	0.8	0.41129640	0.2	0.8891547960	0.2	0.176740130 0.7
13.9000	0.2265335680	0.8	0.41081560	0.2	0.8883725440	0.2	0.172769280 0.7
14.0000	0.2261289120	0.8	0.4103500	0.2	0.8855852600	0.2	0.164606510 0.7
14.1000	0.2257173600	0.8	0.41983330	0.2	0.8829928060	0.2	0.16466721490 0.7
14.2000	0.22529776640	0.8	0.419335170	0.2	0.8802950520	0.2	0.1604136590 0.7
14.3000	0.2248101760	0.8	0.41882300	0.2	0.875918460	0.2	0.156146710 0.7
14.4000	0.22443679720	0.8	0.41830720	0.2	0.8748830330	0.2	0.1476803780 0.7
14.5000	0.2240515280	0.8	0.4178410	0.2	0.8712168470	0.2	0.14616502400 0.7
14.6000	0.22354779560	0.8	0.41725360	0.2	0.8694480120	0.2	0.1428938280 0.7
14.7000	0.2230895640	0.8	0.41671570	0.2	0.8667214970	0.2	0.1332567100 0.7
14.8000	0.2226255640	0.8	0.4161730	0.2	0.8639887740	0.2	0.1336816670 0.7
14.9000	0.2222152560	0.8	0.41561720	0.2	0.861946690	0.2	0.1289615050 0.7
15.0000	0.2218672720	0.8	0.41505640	0.2	0.8585040640	0.2	0.1241651880 0.7
15.1000	0.2214561600	0.8	0.41448780	0.2	0.8557517560	0.2	0.119292140 0.7
15.2000	0.22106962720	0.8	0.41391120	0.2	0.8522925950	0.2	0.1143422120 0.7
15.3000	0.22069022640	0.8	0.41332650	0.2	0.85022264060	0.2	0.1093151950 0.7

TIME	RADIUS	LATITUDE	LONGITUDE	WEIGHT	VELOCITY	RISE LEVEL	DENSITY	
15, 6000	0.219677445560	0.6	0.40273370	0.2	0.84474530170	0.2	0.15463862240	0.5
15, 7000	0.219159235200	0.8	0.40213200	0.2	0.84467252620	0.2	0.15581411360	0.5
15, 8000	0.218633207000	0.8	0.40152300	0.2	0.8418839310	0.2	0.15680277760	0.5
15, 9000	0.218107934800	0.8	0.40112000	0.2	0.8394004820	0.2	0.15780460000	0.5
15, 9800	0.217675788000	0.8	0.4007278020	0.2	0.8362839370	0.2	0.15881984640	0.5
16, 1000	0.217244250000	0.8	0.4003471040	0.2	0.8334710400	0.2	0.15984837120	0.5
16, 1800	0.216812800000	0.8	0.399899830	0.2	0.8306516280	0.2	0.16089031040	0.5
16, 2800	0.216450358400	0.8	0.399516160	0.2	0.82782820	0.2	0.1618457360	0.5
16, 3800	0.216088660000	0.8	0.399184600	0.2	0.824985330	0.2	0.1628461630	0.5
16, 4800	0.215311261800	0.8	0.39768240	0.2	0.824985330	0.2	0.163801472320	0.5
16, 5800	0.214729675200	0.8	0.3970110	0.2	0.821389160	0.2	0.1648073520	0.5
16, 6000	0.21441401600	0.8	0.39632860	0.2	0.8192385320	0.2	0.1651937100	0.5
16, 6800	0.213542432000	0.8	0.39563740	0.2	0.816418590	0.2	0.1663038880	0.5
16, 7800	0.212936332800	0.8	0.39493640	0.2	0.8135445560	0.2	0.16742798760	0.5
16, 8800	0.2113223360	0.8	0.39422550	0.2	0.8106605950	0.2	0.1685565920	0.5

TIME	R-DOT	LAT,-DOT	LONG,-DOT	R-DOT DOT	LAT,-DOT DOT	LONG,-DOT DOT
0.	0.100494530 05	0.5398007-02	-0.520255D-01	-0.226787923D 02	-0.2500559D-04	0.3704917D-04
0.1000	0.995185430 04	-0.5241970-02	-0.518055D-01	-0.225755D-02	-0.24602AD-04	0.363649D-04
0.2000	0.98204597D 04	-0.59552D-02	-0.515898D-01	-0.224123164D 02	-0.2421372D-04	0.356940D-04
0.3000	0.96851449D 04	-0.495138D-02	-0.51373D-01	-0.223721555D 02	-0.238353D-04	0.350361D-04
0.4000	0.9555577 8D 04	-0.48094949-02	-0.511691D-01	-0.222339580D 02	-0.23439088D 04	0.3439088D-04
0.5000	0.94222272D 04	-0.46977-02	-0.50964D-01	-0.21778063D 02	-0.23375783D 04	0.337375783D 04
0.6000	0.928439561D 04	-0.453216D-02	-0.507689D-01	-0.22635344D 02	-0.2276193D-04	0.3313664D-04
0.7000	0.91521551D 04	-0.439661D-02	-0.505689D-01	-0.21991625D 02	-0.2242445D-04	0.3252695D-04
0.8000	0.902554188D 04	-0.426305D-02	-0.503680D-01	-0.21966521D 02	-0.2209677D-04	0.3192843D-04
0.9000	0.88904 4999 04	-0.413142D-02	-0.50183D-01	-0.21819705D 02	-0.217789D-04	0.3134073D-04
1.0000	0.876379468D 04	-0.401668D-02	-0.49915D-01	-0.217250857D 02	-0.2146995D-02	0.3076355D-04
1.1000	0.863373048D 04	-0.3873777-02	-0.498146D-01	-0.2139676D 02	-0.2119886D-02	0.3019657D-04
1.2000	0.85011161D 04	-0.374763D-02	-0.49635D-01	-0.2156862D 02	-0.2082507D-04	0.2963949D-04
1.3000	0.83701798D 04	-0.362321D-02	-0.49458D-01	-0.21449123D 02	-0.205922D-04	0.2909204D-04
1.4000	0.82444 334D 04	-0.35047D-02	-0.49286D-01	-0.213949182D 02	-0.203287D-04	0.2855392D-04
1.5000	0.811827564D 04	-0.337935D-02	-0.49162D-01	-0.21316764D 02	-0.200500D-04	0.2802487D-04
1.6000	0.79916715D 04	-0.325982D-02	-0.48944D-01	-0.21239864D 02	-0.197347D-04	0.2750462D-04
1.7000	0.78639411D 04	-0.314182D-02	-0.48786D-01	-0.21167443D 02	-0.19543AD-04	0.269923D-04
1.8000	0.7735627 7D 04	-0.302534D-02	-0.48625D-01	-0.210912030D 02	-0.192952D-04	0.2648954D-04
1.9000	0.76129557D 04	-0.291024D-02	-0.48468D-01	-0.210192123D 02	-0.190569D-04	0.2599422D-04
2.0000	0.74839347D 04	-0.279659D-02	-0.48313D-01	-0.20987486D 02	-0.188277D-04	0.2550674D-04
2.1000	0.735936D 04	-0.26843D-02	-0.48162D-01	-0.208797886D 02	-0.186037D-04	0.2502686D-04
2.2000	0.7235833 8D 04	-0.257333D-02	-0.480134D-01	-0.208123102D 02	-0.183853D-04	0.245544D-04
2.3000	0.71015795D 04	-0.246366D-02	-0.47865D-01	-0.207482916D 02	-0.181739D-04	0.2408912D-04
2.4000	0.69887468D 04	-0.235523D-02	-0.47724D-01	-0.206817120D 02	-0.179666D-04	0.2363082D-04
2.5000	0.68697459D 04	-0.224802D-02	-0.47583D-01	-0.206165504D 02	-0.177692D-04	0.231730D-04
2.6000	0.67314928D 04	-0.214199D-02	-0.47442D-01	-0.20567873D 02	-0.175365D-04	0.227343D-04
2.7000	0.661212943D 04	-0.203713D-02	-0.47311D-01	-0.204964302D 02	-0.173876D-04	0.2229585D-04
2.8000	0.649148972D 04	-0.193333D-02	-0.47186D-01	-0.204373793D 02	-0.172047D-04	0.2186354D-04
2.9000	0.63603915D 04	-0.183763D-02	-0.47048D-01	-0.203196976D 02	-0.170285AD-04	0.2143728D-04
3.0000	0.624643069D 04	-0.172892D-02	-0.46921D-01	-0.203233401D 02	-0.168569D-04	0.2101669D-04
3.1000	0.612515548D 04	-0.162833D-02	-0.46796D-01	-0.202682899D 02	-0.1666954D-04	0.2060220D-04
3.2000	0.60137867D 04	-0.152868D-02	-0.466724D-01	-0.202145300D 02	-0.16529.5D-04	0.2019350D-04
3.3000	0.588575758D 04	-0.142997D-02	-0.46554D-01	-0.201620440D 02	-0.16326AD-04	0.1978929D-04
3.4000	0.57617616D 04	-0.133220D-02	-0.46436D-01	-0.201108174D 02	-0.16202D-04	0.1939075D-04
3.5000	0.56424729D 04	-0.123531D-02	-0.46325D-01	-0.20008336D 02	-0.1604UAD-04	0.189972D-04
3.6000	0.552402918D 04	-0.113930D-02	-0.462087D-01	-0.200120784D 02	-0.1593174D-04	0.186087D-04
3.7000	0.54009990D 04	-0.104412D-02	-0.45920D-01	-0.19745700D 02	-0.1516904D-04	0.163733D-04
3.8000	0.52845228D 04	-0.949762D-02	-0.45920D-01	-0.19981961D 02	-0.150533D-04	0.1601554D-04
3.9000	0.5161705D 04	-0.856188D-03	-0.45880D-01	-0.19830417D 02	-0.149646264D 02	0.156615D-04
4.0000	0.50497344D 04	-0.733377D-03	-0.45783D-01	-0.19830417D 02	-0.148256D-04	0.153146D-04
4.1000	0.49212912D 04	-0.671303D-03	-0.456788D-01	-0.19862412D 02	-0.147135D-04	0.149680D-04
4.2000	0.48053525D 04	-0.579940D-03	-0.45595D-01	-0.19745700D 02	-0.1463381D-04	0.146218D-04
4.3000	0.46811914D 04	-0.489266D-03	-0.45482D-01	-0.19704356D 02	-0.145499D-04	0.142822D-04
4.4000	0.45618556D 04	-0.392577D-03	-0.45383D-01	-0.19646264D 02	-0.1449453D-04	0.1394600D-04
4.5000	0.44521331D 04	-0.398887D-03	-0.45244D-01	-0.19263313D 02	-0.14256D-04	0.131460D-04
4.6000	0.43356742D 04	-0.22138D-03	-0.45205D-01	-0.19591393D 02	-0.147135D-04	0.131460D-04
4.7000	0.42161444D 04	-0.1329857D-03	-0.45148D-01	-0.19530464D 02	-0.1463381D-04	0.131460D-04
4.8000	0.40992375D 04	-0.45451D-04	-0.45028D-01	-0.19588241D 02	-0.145499D-04	0.131460D-04
4.9000	0.3981923 1D 04	-0.416219D-04	-0.44941D-01	-0.19840809D 02	-0.144962D-04	0.131460D-04
5.0000	0.386511766D 04	-0.129117D-03	-0.44865D-01	-0.19512014D 02	-0.143281D-04	0.131460D-04
5.1000	0.37485 544D 04	-0.214102D-03	-0.44780D-01	-0.194193764D 02	-0.1428945D-04	0.13128299D-04

## TIME

## LAT., -DUT

## LONG., -DUT

## R-DOT DOT

## LONG., -DUT

## LAT., -DUT

TIME	R-DOT	LAT., -DUT	LONG., -DUT	R-DOT DOT	LAT., -DUT	LONG., -DUT
5.2000	0.36320283.70	0.4	-1.2995980-03	-0.447013D-01	-0.19388574D-02	-0.142094AD-04
5.3000	0.3515842121D-04	-0.4	-1.38462370-03	-0.446245D-01	-0.193588526D-02	-0.1413285D-04
5.4000	0.3399774750	0.4	-1.691980-03	-0.445497D-01	-0.19330133D-02	-0.1405952D-04
5.5000	0.3283877470	0.4	-1.55344D-03	-0.444768D-01	-0.19302426D-02	-0.139894D-04
5.6000	0.3168143220	0.4	-1.637780-03	-0.444056D-01	-0.19275758D-02	-0.1382525D-04
5.7000	0.305256140	0.4	-1.204200D-03	-0.43367D-01	-0.19205057D-02	-0.1388880D-04
5.8000	0.293714530	0.4	-1.83390D-03	-0.42694D-01	-0.192254358D-02	-0.137981D-04
5.9000	0.282185940	0.4	-1.88604D-03	-0.42044D-01	-0.192450580D-02	-0.1374062D-04
6.0000	0.270671596D	0.4	-1.98283D-03	-0.41444D-01	-0.19261590D-02	-0.1370733D-04
6.1000	0.25917316D	0.4	-1.10524D-02	-0.40788D-01	-0.19179450D-02	-0.136861D-04
6.2000	0.24768265D	0.4	-1.13190D-02	-0.40189D-01	-0.19136626D-02	-0.1358603D-04
6.3000	0.23620265D	0.4	-1.2138D-02	-0.39608D-01	-0.19116882D-02	-0.1350509D-04
6.4000	0.22474224D	0.4	-1.29439D-02	-0.39045D-01	-0.190980632D-02	-0.1349762D-04
6.5000	0.2132883.1D	0.4	-1.137526D-02	-0.38500D-01	-0.19060223D-02	-0.1345785D-04
6.6000	0.20184558D	0.4	-1.98589D-02	-0.37973D-01	-0.19033376D-02	-0.1342085D-04
6.7000	0.19041261D-02	-0.4	-1.53632D-02	-0.37463D-01	-0.190245D-02	-0.133666D-04
6.8000	0.1789887.9D	0.4	-1.61654D-02	-0.36971D-01	-0.19032437D-02	-0.1335929D-04
6.9000	0.16757322D	0.4	-1.6658D-02	-0.36497D-01	-0.1901836D-02	-0.133266D-04
7.0000	0.15616681D	0.4	-1.7647D-02	-0.36039D-01	-0.1900525D-02	-0.133081D-04
7.1000	0.144767324D	0.4	-1.85620D-02	-0.35599D-01	-0.18993086D-02	-0.132772D-04
7.2000	0.13337592D	0.4	-1.93580D-02	-0.35176D-01	-0.18981851D-02	-0.1325732D-04
7.3000	0.121988824D	0.4	-1.21529D-02	-0.34770D-01	-0.18971532D-02	-0.1323961D-04
7.4000	0.11060855D	0.4	-1.29468D-02	-0.34382D-01	-0.18962147D-02	-0.1322462D-04
7.5000	0.992338324D	0.5	-1.213399D-02	-0.34010D-01	-0.18953666D-02	-0.1321229D-04
7.6000	0.87863595D	0.5	-1.25324D-02	-0.33655D-01	-0.18946146D-02	-0.1320262D-04
7.7000	0.76498333D	0.3	-1.23243D-02	-0.33317D-01	-0.1893526D-02	-0.1319561D-04
7.8000	0.65136344D	0.3	-1.24159D-02	-0.32996D-01	-0.18918851D-02	-0.13124D-04
7.9000	0.5377753.8D	0.3	-1.24973D-02	-0.32696D-01	-0.18929035D-02	-0.1318951D-04
8.0000	0.42421345D	0.3	-1.25987D-02	-0.3243D-01	-0.189251689D-02	-0.131941D-04
8.1000	0.31067155D	0.3	-1.26492D-02	-0.32132D-01	-0.18922134D-02	-0.1319394D-04
8.2000	0.19714476D	0.3	-1.27828D-02	-0.31878D-01	-0.189201215D-02	-0.132009D-04
8.3000	0.83627515D	0.2	-1.281743D-02	-0.3164D-01	-0.18919042D-02	-0.1320887D-04
8.4000	-1.298855747D	0.2	-1.285671D-02	-0.31418D-01	-0.18918825D-02	-0.1322202A-04
8.5000	-1.14340165D	0.3	-1.29568D-02	-0.31214D-01	-0.18919523D-02	-0.1323431D-04
8.6000	-0.256292575D	0.3	-1.34553D-02	-0.31025D-01	-0.18921132D-02	-0.1325097D-04
8.7000	-0.37455384D	0.3	-1.32509D-02	-0.30854D-01	-0.18923558D-02	-0.1327026D-04
8.8000	-0.19714476D	0.3	-1.31878D-02	-0.3054D-01	-0.189201215D-02	-0.132009D-04
8.9000	-0.484007312D	0.3	-1.31178D-02	-0.3025D-01	-0.18919042D-02	-0.1320887D-04
9.0000	-1.59758221D	0.3	-1.30496D-02	-0.3006D-01	-0.18918851D-02	-0.1322202A-04
9.1000	-1.7118634D	0.3	-1.30159D-02	-0.3038D-01	-0.18936123D-02	-0.13344U1D-04
9.2000	-0.94482424D	0.3	-1.34474D-02	-0.30332D-01	-0.18942897D-02	-0.1337391D-04
9.3000	-0.105222515D	0.4	-1.32508D-02	-0.30243D-01	-0.1895001D-02	-0.134064RD-04
9.4000	-0.11660131D	0.4	-1.316562D-02	-0.30176D-01	-0.18958025D-02	-0.1344175D-04
9.5000	-0.12798335D	0.4	-1.30838D-02	-0.3014D-01	-0.18966944D-02	-0.1347972D-04
9.6000	-0.139372532D	0.4	-1.30651D-02	-0.30074D-01	-0.18976843D-02	-0.1352041D-04
9.7000	-0.150768395D	0.4	-1.30452D-02	-0.30051D-01	-0.18987648D-02	-0.1356383D-04
9.8000	-1.162171974D	0.4	-1.30255D-02	-0.30045D-01	-0.189993795D-02	-0.13610U2D-04
9.9000	-1.17358135D	0.4	-1.3014D-02	-0.30055D-01	-0.19012044D-02	-0.136589D-04
10.0000	-1.1850U237D	0.4	-1.2975D-02	-0.30082D-01	-0.190255642D-02	-0.1371074D-04
10.1000	-0.19643159D	0.4	-1.2950D-02	-0.30125D-01	-0.190401886D-02	-0.1376532D-04
10.2000	-1.27869237D	0.4	-1.2926D-02	-0.30185D-01	-0.19055652D-02	-0.1382275D-04
10.3000	-0.21931831D	0.4	-1.2904D-02	-0.303556D-01	-0.19072110D-02	-0.1388305D-04

TIME	R-DOT	LAT.+-DOT	LONG.+-DOT	R-DOT.DOT	LAT.+-DOT.DOT	LONG.+-DOT.DOT
10.4000	-0.2307775260	0.4	1.450973D-012	0.430467D-011	-0.1910784220	0.2
10.5000	-0.2422479740	0.4	1.459402D-012	0.430595D-011	-0.1912714910	0.2
10.6000	-0.253329750	0.4	1.467872D-012	0.430742D-011	-0.1914474230	0.2
10.7000	-0.2652259750	0.4	1.476386D-012	0.430902D-011	-0.1916886940	0.2
10.8000	-0.276323960	0.4	1.484947D-012	0.431081D-011	-0.191909400	0.2
10.9000	-0.2882543450	0.4	1.493555D-012	0.431278D-011	-0.1921440280	0.2
11.0000	-0.299792010	0.4	1.502214D-012	0.431491D-011	-0.1923830170	0.2
11.1000	-0.31134580	0.4	1.510923D-012	0.431742D-011	-0.192634740	0.2
11.2000	-0.32206415D	0.4	1.519887D-012	0.431971D-011	-0.1928969680	0.2
11.3000	-0.334488345D	0.4	1.528506D-012	0.432238D-011	-0.1931610650	0.2
11.4000	-0.3460866250	0.4	1.537382D-012	0.432522D-011	-0.1934513420	0.2
11.5000	-0.3570271JD	0.4	1.546318D-012	0.432824D-011	-0.1937438760	0.2
11.6000	-0.3693553770	0.4	1.555316D-012	0.433144D-011	-0.1940467450	0.2
11.7000	-0.3809885280	0.4	1.564377D-012	0.433482D-011	-0.194360330	0.2
11.8000	-0.3926297920	0.4	1.573504D-012	0.433839D-011	-0.1946838240	0.2
11.9000	-0.404351800	0.4	1.582699D-012	0.434214D-011	-0.195012080	0.2
12.0000	-0.416621880	0.4	1.591964D-012	0.434607D-011	-0.1953632780	0.2
12.1000	-0.4279794580	0.4	1.601301D-012	0.435019D-011	-0.1957191310	0.2
12.2000	-0.43958740	0.4	1.610713D-012	0.435450D-011	-0.1960858620	0.2
12.3000	-0.4513251320	0.4	1.620202D-012	0.435899D-011	-0.1964655770	0.2
12.4000	-0.463245560	0.4	1.629770D-012	0.436368D-011	-0.1968521820	0.2
12.5000	-0.474415410	0.4	1.639420D-012	0.436856D-011	-0.1972523840	0.2
12.6000	-0.4867950650	0.4	1.649154D-012	0.437364D-011	-0.1976637000	0.2
12.7000	-0.4986675130	0.4	1.658975D-012	0.437891D-011	-0.1980864440	0.2
12.8000	-0.5105657600	0.4	1.668843D-012	0.438439D-011	-0.198497740	0.2
12.9000	-0.52249233D	0.4	1.678886D-012	0.439006D-011	-0.1989667120	0.2
13.0000	-0.5344419130	0.4	1.688982D-012	0.439593D-011	-0.1994244860	0.2
13.1000	-0.5464244140	0.4	1.699175D-012	0.440201D-011	-0.1998944980	0.2
13.2000	-0.5584294590	0.4	1.70468D-012	0.440830D-011	-0.200379850	0.2
13.3000	-0.570465719D	0.4	1.719864D-012	0.441479D-011	-0.200869950	0.2
13.4000	-0.5825340990	0.4	1.730365D-012	0.442150D-011	-0.20137355D	0.2
13.5000	-0.594631850	0.4	1.749750D-012	0.443284D-011	-0.20189667120	0.2
13.6000	-0.606721850	0.4	1.751696D-012	0.443556D-011	-0.2024237790	0.2
13.7000	-0.6189235640	0.4	1.762532D-012	0.444291D-011	-0.2029715150	0.2
13.8000	-0.6311185790	0.4	1.773486D-012	0.445049D-011	-0.2035251160	0.2
13.9000	-0.6433433130	0.4	1.784561D-012	0.445829D-011	-0.20421500430	0.2
14.0000	-0.65561732D	0.4	1.795760D-012	0.446632D-011	-0.2046829040	0.2
14.1000	-0.667902561D	0.4	1.807087D-012	0.447458D-011	-0.205280810	0.2
14.2000	-0.6802445450	0.4	1.818545D-012	0.447935D-011	-0.205893610	0.2
14.3000	-0.692621680	0.4	1.830138D-012	0.449180D-011	-0.206513310	0.2
14.4000	-0.7050261850	0.4	1.841870D-012	0.450077D-011	-0.207153880	0.2
14.5000	-0.717477310	0.4	1.853744D-012	0.450998D-011	-0.207808360	0.2
14.6000	-0.7299662170	0.4	1.865764D-012	0.451943D-011	-0.208465820	0.2
14.7000	-0.7424932160	0.4	1.877935D-012	0.452914D-011	-0.209159420	0.2
14.8000	-0.7550633150	0.4	1.890259D-012	0.453910D-011	-0.209856300	0.2
14.9000	-0.767673130	0.4	1.92742D-012	0.454932D-011	-0.210569280	0.2
15.0000	-0.78032350	0.4	1.95387D-012	0.45598UD-011	-0.211297320	0.2
15.1000	-0.79332370	0.4	1.982800D-012	0.457055D-011	-0.212049950	0.2
15.2000	-0.815774720	0.4	1.94184D-012	0.458156D-011	-0.2128005480	0.2
15.3000	-0.831466910	0.4	1.954345D-012	0.460442D-011	-0.2135762360	0.2
15.4000	-0.844293220	0.4	1.967686D-012	0.461627D-011	-0.214368921	0.2
15.5000	-0.844293220	0.4	1.9812147D-012	0.461627D-011	-0.21517170720	0.2

TIME	R-DOT	LAT.-DOT	LONG.-DOT	R-DOT DOT	LAT.-DOT DOT	LONG.-DOT DOT
15, 6000	-0, 857228537D 04	-0, 994932D-02	*0, 462840D-01	-0, 216002768D 02	-0, 2302634D-04	-0, 2047154D-04
15, 7000	-0, 870139110D 04	-0, 100885D-01	*0, 464083D-01	-0, 216845689D 02	-0, 233579D-04	-0, 2076333D-04
15, 8000	-0, 883251368D 04	-0, 102296D-01	*0, 465356D-01	*0, 21706134D 02	-0, 236986D-04	-0, 2146368D-04
15, 9000	-0, 896389950D 04	-0, 103729D-01	*0, 466659D-01	-0, 21858406D 02	-0, 240465D-04	-0, 2177286D-04
16, 0000	-0, 909981857D 04	-0, 105162D-01	*0, 467993D-01	-0, 21980812D 02	-0, 244085D-04	-0, 2249116D-04
16, 1000	-0, 922677056D 04	-0, 106658D-01	*0, 469358D-01	-0, 22035676D 02	-0, 247782D-04	-0, 2301888D-04
16, 2000	-0, 935938715D 04	-0, 108156D-01	*0, 470755D-01	-0, 22132328D 02	-0, 251582D-04	-0, 2355632D-04
16, 3000	-0, 949356965D 04	-0, 109677D-01	*0, 472165D-01	-0, 2228102D 02	-0, 255487D-04	-0, 24103D-04
16, 4000	-0, 952612956D 04	-0, 111222D-01	*0, 473648D-01	-0, 223251355D 02	-0, 259502D-04	-0, 2466166D-04
16, 5000	-0, 976027979D 04	-0, 112791D-01	*0, 475145D-01	-0, 2242441D 02	-0, 263650D-04	-0, 253022D-04
16, 6000	-0, 989512934D 04	-0, 114386D-01	*0, 4766776D-01	-0, 225250736D 02	-0, 267874D-04	-0, 2510986D-04
16, 7000	-0, 1010105934D 05	-0, 11606D-01	*0, 478242D-01	-0, 22629161D 02	-0, 272289D-04	-0, 264054D-04
16, 8000	-0, 10666935D 05	-0, 117653D-01	*0, 47984D-01	-0, 22735481D 02	-0, 276724D-04	-0, 2700383D-04
16, 9000	-0, 103033987D 05	-0, 119327D-01	*0, 481482D-01	-0, 228236438D 02	-0, 2811514D-04	-0, 2753514D-04

TIME (MIN)	SLANT RANGE(FT)	SL RAY RATE(SEC)	SL RANGE RATE(SEC)	18.30000 SENSORS RATE(SEC)	18.30000 SENSORS RATE(SEC)	0.58333 TH(SEC)	0.58333 TH(SEC)	AZ RATE(DEG/SEC)
5.8 .05	0.10519 36322D	.8	-.3711478711600 .04	0.473968973860	0.1	0.181852303D	0.2	-0.64926D-01
5.9 .05	0.1055972J25400	.8	-.368289589200 .04	0.475159556434D	0.1	0.17947579D	0.2	-0.65231D-01
6.0 .05	0.105577139J0 .06	-.365440071350 .04	0.472618687D	0.1	0.17424564D	0.2	-0.6536D-01	
6.1 .05	0.1051586754300	.18	-.362616190127D .04	0.469675993040D	0.1	0.17008324D	0.2	-0.65841D-01
6.2 .05	0.104941943380	.18	-.359810571760 .04	0.463204194135D	0.1	0.166123614D	0.2	-0.66146D-01
6.3 .05	0.104 .18	-.3572468679379D .04	0.463688679379D	0.1	0.162145684D	0.2	-0.66451D-01	
6.4 .05	0.104513522138D	.18	-.3542256J859780 .04	0.4614717119961D	0.1	0.1581794597	0.2	-0.66756D-01
6.5 .05	0.1043 .18	-.351483525001D .04	0.459495621811D	0.1	0.15134951D	0.2	-0.67061D-01	
6.6 .05	0.104 .18	-.348731492157D .04	0.457912273545D	0.1	0.150102180D	0.2	-0.67365D-01	
6.7 .05	0.10436833233J0	.08	-.3459888141042D .04	0.456635445904D	0.1	0.1440512171D	0.2	-0.67669D-01
6.8 .05	0.10436765538D0	.16	-.343251210827D .04	0.455598617777D	0.1	0.141981954D	0.2	-0.67972D-01
6.9 .05	0.103471419952D	.18	-.34519J260122D .04	0.455087391068D	0.1	0.13784567D	0.2	-0.68274D-01
7.0 .05	0.102 .18	-.337789496230D .04	0.454811586655D	0.1	0.133789051D	0.2	-0.68576D-01	
7.1 .05	0.103 .66	-.3356 .06	-.3356 .06	0.454812299639D	0.1	0.1296855457D	0.2	-0.68877D-01
7.2 .05	0.102659855210	.08	-.3323353645 .04	0.45268101697D	0.1	0.12553837D	0.2	-0.69177D-01
7.3 .05	0.102667276579D	.16	-.3295697J5448D .04	0.455610759668D	0.1	0.121364255D	0.2	-0.69476D-01
7.4 .05	0.102473034769	.16	-.326685758876D .04	0.455794943761D	0.1	0.117186776D	0.2	-0.69773D-01
7.5 .05	0.102 .75	-.324110940274D .04	0.458517280777D	0.1	0.1129914776D	0.2	-0.70070D-01	
7.6 .05	0.102 .81438867D	.16	-.321357681966D .04	0.446223844349D	0.1	0.108778434D	0.2	-0.70365D-01
7.7 .05	0.101889425812D	.16	-.318588711295D .04	0.46221862225D	0.1	0.104747736D	0.2	-0.70658D-01
7.8 .05	0.10169917583D	.16	-.315805911243D .04	0.464904190446D	0.1	0.10029477D	0.2	-0.70950D-01
7.9 .05	0.10151453115D	.08	-.313 .07	0.467743352622D	0.1	0.96037555D	0.1	-0.71240D-01
8.0 .05	0.10123532535D	.16	-.310192171403D .04	0.472942438137D	0.1	0.915067786D	0.1	-0.71529D-01
8.1 .05	0.1013823J571D	.16	-.30735113571D .04	0.47515902191D	0.1	0.8745021591D	0.1	-0.71815D-01
8.2 .05	0.101754568994D	.16	-.304499489980D .04	0.4784313J3805D	0.1	0.83329168D	0.1	-0.72099D-01
8.3 .05	0.101772868 .04	-.3161319873D	0.04	0.48227J233266D	0.1	0.787984784D	0.1	-0.7382D-01
III-145	8.4 .05	0.10 .59275537D	.18	-.298703J20589D	0.4	0.74471777D	0.1	-0.72661D-01
8.5 .05	0.10 .51449J9 .5D	.18	-.29576315839D	0.4	0.49245598408D	0.1	0.7002939D-01	-0.72939D-01
8.6 .05	0.10 .237584329D	.18	-.2927793J39244D	0.4	0.497854058764D	0.1	0.65645523D	0.1
8.7 .05	0.10 .63 .54	-.2897788J987D	0.4	0.50362633435D	0.1	0.61235265D	0.1	-0.73486D-01
8.8 .05	0.9987J1-5160 .07	-.283669927026D	0.4	0.50983J253966D	0.1	0.524286244D	0.1	-0.73756D-01
8.9 .05	0.99 .997189735139D	.07	-.286674421616D	0.4	0.516441862529D	0.1	0.47935848D	0.1
9.0 .05	0.99549752979D	.07	-.280556841473D	0.4	0.52352633925D	0.1	0.45285244D	0.1
9.1 .05	0.9932321896D	.17	-.2773838442579D	0.4	0.53766798223D	0.1	0.45285244D	0.1
9.2 .05	0.99 .997168447451D	.17	-.27418J1970389D	0.4	0.538449983423D	0.1	0.39579316D	0.1
9.3 .05	0.99 .233128391D	.17	-.276922647454D	0.4	0.54659 .864272D	0.1	0.34519806D	0.1
9.4 .05	0.9889174578 .5D	.17	-.2676256738916D	0.4	0.55513J331013D	0.1	0.300408723D	0.1
9.5 .05	0.9873217731565D	.07	-.260831539411D	0.4	0.5734845775D	0.1	0.20942026D	0.1
9.6 .05	0.98545396578D	.07	-.25738293043D	0.4	0.583188757205D	0.1	0.16187122D	0.1
9.7 .05	0.984191654517D	.07	-.253852350691D	0.4	0.59335J910433D	0.1	0.11849116D	0.1
9.8 .05	0.982627928678D	.07	-.2502616133053D	0.4	0.603941633567D	0.1	0.726464566D	0.0
9.9 .05	0.981115524985D	.07	-.246667644692D	0.4	0.614951590482D	0.1	0.266600104D	0.0
10.0 .05	0.979564924565D	.07	-.242888874364D	0.4	0.62635J386376D	0.1	0.359805697D	0.0
10.1 .05	0.978186433947D	.07	-.239+8J295377D	0.4	0.638221561063D	0.1	0.359343262D	0.0
10.2 .05	0.9767449387D	.07	-.23522156017D	0.4	0.65492582027D	0.1	0.76042D-01	-0.77182D-01
10.3 .05	0.975317531 .2D	.07	-.231285300102D	0.4	0.66319J837229D	0.1	0.358879521D	0.0
10.4 .05	0.97391793726D	.07	-.22726216980D	0.4	0.676338627617D	0.1	0.77610D-01	-0.77610D-01
10.5 .05	0.972942319547D	.07	-.22316843070D	0.4	0.688988J8159386D	0.1	0.357948229D	0.0
10.6 .05	0.971119J9 .1D	.07	-.21898811458D	0.4	0.70388J1536000D	0.1	0.357012038D	0.0
10.7 .05	0.9696451938 .0D	.07	-.21471513042D	0.4	0.71830J749964D	0.1	0.356742176D	0.0
10.8 .05	0.9685337337544D	.07	-.210363237123D	0.4	0.733167674352D	0.1	0.356071176D	0.0

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TIME(MIN)	SLANT RANGE(FT)	SL RANGE LATITUDE(SEC)	LONGITUDE(SEC)	ROTATION RATE(SEC)	TYPE(W)	0.58331
	SL	RANGE	ROT	TYPE	(W/SEC)	AZimuth (deg)
						AZ Rate (deg/sec)
11.0 0.0	966 3921	740 17	-2 391 7621	22127D 04	0.748474054029D 01	0.35559066D 03
11.1 0.0	964 3172	14 17	-2 1379 7584	35D 04	0.764221498817D 01	0.35515877D 03
11.2 0.0	953522845341D 07	-1 196 746 179205D 04	0.78041164297D 01	0.35465164D 03		
11.3 0.0	962455615 28D 07	-1 192 13931292D 04	0.797045262283D 01	0.354176386D 03		
11.4 0.0	961 31988 462D 07	-1 187180665207D 04	0.814124131700D 01	0.353700147D 03		
11.5 0.0	96 155316D 07	-1 18224355130D 04	0.83168136399D 01	0.353224954D 03		
11.6 0.0	959 3217 351D 07	-1 17719996003D 04	0.84962 163571D 01	0.35274484D 03		
11.7 0.0	958 64374 59D 07	-1 172 047214654D 04	0.868038893615D 01	0.35226837D 03		
11.8 0.0	956 8311892D 07	-1 1667826 604D 04	0.886905810058D 01	0.35178597D 03		
11.9 0.0	955 31221426D 07	-1 161403452328D 04	0.905219579345D 01	0.351305292D 03		
12.0 0.0	954 21256837D 07	-1 155907057566D 04	0.925981642502D 01	0.350825832D 03		
12.1 0.0	954 21256837D 07	-1 15029070722D 04	0.9461912 4878D 01	0.35034161D 03		
12.2 0.0	95329797972D 07	-1 144581687296D 04	0.96586772977D 01	0.35085866D 03		
12.3 0.0	952478194762D 17	-1 136687715798D 04	0.98795 4 8121D 01	0.349375043D 03		
12.4 0.0	95166378 26D 07	-1 132695593512D 04	0.10 949818829D 02	0.348890767D 03		
12.5 0.0	95 886103913D 07	-1 126572850134D 04	0.10314892587D 02	0.348408767D 03		
12.6 0.0	95 45372574D 07	-1 120316831455D 04	0.105392359369D 02	0.34792045D 03		
12.7 0.0	949442578799D 07	-1 11392486113D 04	0.10767926791D 02	0.34743389D 03		
12.8 0.0	948778351 38D 07	-1 7394388436D 04	0.11701021846D 02	0.346947865D 03		
12.9 0.0	948 5412851 07	-1 6722708951D 04	0.112385639960D 02	0.3446460867D 03		
13.0 0.0	9475715611D 07	-1 939772466132D 03	0.114803624091D 02	0.34597331D 03		

TIME(MIN)	AZ ROOT(DEG/SEC/SEC)	ELEVATION(DEG)	EL RATE(SEC/SEC)	EL ROOT(SEC/SEC/SEC)	REFINRY ANGLE	HEADING
5.8000	-0.23287610.03	6.66837550.00	-0.2830312D-01	-0.11195350480D-03	0.2575250	0.268740.03
5.9000	-0.145691620.03	7.83616420.00	0.2162890D-01	-0.111286159158D-03	0.2579930	0.2684250.03
6.0000	-0.249565510.03	8.99990244.00	0.2694967D-01	-0.113624130424D-03	0.2584630	0.26822770.03
6.1000	-0.1595550.01	9.159550.01	0.2826540D-01	-0.114466749193D-03	0.2589350	0.2681290.03
6.2000	-0.26853369D-03	9.13150770.01	0.2756765D-01	-0.115341964040D-03	0.2679810	0.2679810.03
6.3000	-0.27869058D-03	7.14664530.01	0.2498164D-01	-0.11616704829D-03	0.2598840	0.2678330.03
6.4000	-0.28934348D-03	7.16136460.01	0.218204D-01	-0.11702361560D-03	0.2603610	0.2676860.03
6.5000	-0.30532956D-03	7.17566270.01	0.2347731D-01	-0.11784421511D-03	0.260840D	0.2675390.03
6.6000	-0.31234330.03	6.18953630.01	0.2276741D-01	-0.118749581460D-03	0.2613200	0.2673920.03
6.7000	-0.32478240.03	7.20298250.01	0.2205231D-01	-0.11961904248D-03	0.2618020	0.2672450.03
6.8000	-0.33781560.03	7.21599810.01	0.2333197D-01	-0.12049250283D-03	0.2622850	0.2670990.03
6.9000	-0.3516484D-03	7.22857980.01	0.2160639D-01	-0.12136957002D-03	0.2627690	0.2669530.03
7.0000	-0.366321180D-03	7.24072470.01	0.1987553D-01	-0.12250239031D-03	0.2632540	0.2668070.03
7.1000	-0.38192170.03	6.25242940.01	0.1919398D-01	-0.123134266639D-03	0.2637400	0.2666610.03
7.2000	-0.39848513D-03	6.26369090.01	0.1839791D-01	-0.124021498873D-03	0.2642280	0.2665150.03
7.3000	-0.1617739D-03	7.27450950.01	0.1765112D-01	-0.12401163148D-03	0.2647160	0.2663700.03
7.4000	-0.4351245D-03	6.28487110.01	0.1689897D-01	-0.12580463744D-03	0.2652060	0.2662250.03
7.5000	-0.5554314D-03	6.29478350.01	0.161446D-01	-0.12669964401D-03	0.2656960	0.2660800.03
7.6000	-0.47724348D-03	7.30423980.01	0.1537857D-01	-0.127597750567D-03	0.2661870	0.2659350.03
7.7000	-0.50082369D-03	7.31326360.01	0.1461029D-01	-0.12849627144D-03	0.2666780	0.2657900.03
7.8000	-0.526366541D-03	7.32177110.01	0.1383661D-01	-0.129396913723D-03	0.2671760	0.2656450.03
7.9000	-0.55414464D-03	7.32983960.01	0.1305752D-01	-0.130298740514D-03	0.2676630	0.2655040.03
8.0000	-0.58448195D-03	7.33743900.01	0.1227302D-01	-0.131201378014D-03	0.2681560	0.2663570.03
8.1000	-0.61768270.03	6.3445664D-01	0.1148314D-01	-0.13210443886D-03	0.2686490	0.2652130.03
8.2000	-0.6447728D-03	7.35121770.01	0.1087714D-01	-0.13300527286D-03	0.2691430	0.2650960.03
8.3000	-0.69519052D-03	7.35739040.01	0.9887018D-02	-0.13391026875D-03	0.2696360	0.2649250.03
8.4000	-0.10814396D-02	6.3841896D-01	0.9708050D-02	-0.1348162691D-03	0.2701340	0.2647810.03
8.5000	-0.14662984D-03	6.36308100.01	0.9269275D-02	-0.13571268069D-03	0.2706240	0.2643720.03
8.6000	-0.7917244D-03	6.36828263D-01	0.8269275D-02	-0.1361201378014D-03	0.2706240	0.2643720.03
8.7000	-0.8456445D-03	7.37300310.01	0.7452302D-02	-0.136611501098D-03	0.2711170	0.2644940.03
8.8000	-0.9571261D-03	6.37722800.01	0.669942D-02	-0.137508019120D-03	0.2716110	0.2643500.03
8.9000	-0.992119527D-03	6.3809579D-01	0.5802102D-02	-0.138041832163D-03	0.2721040	0.2642070.03
9.0000	-0.10814396D-02	6.3841896D-01	0.4989127D-02	-0.139292215586D-03	0.2725960	0.2646630.03
9.1000	-0.1187334D-02	6.3869119D-01	0.4130711D-02	-0.140178827794D-03	0.2730890	0.2639200.03
9.2000	-0.13149773D-02	6.391454D-01	0.3268990D-02	-0.14106010979D-03	0.2735840	0.2637770.03
9.3000	-0.14719834D-02	6.3908631D-01	0.2457991D-02	-0.141963882728D-03	0.274720	0.2636340.03
9.4000	-0.1669545D-02	6.3920690.01	0.1593746D-02	-0.14280917061D-03	0.2754620	0.2634910.03
9.5000	-0.22769571D-02	6.39296260.01	0.7292336D-03	-0.14367435762D-03	0.2750520	0.2633480.03
9.6000	-0.27781251D-02	6.3925932D-01	0.1023073D-02	-0.143873164D-03	0.27632050	0.2627750.03
9.7000	-0.35583437D-02	6.3917249D-01	0.1884894D-02	-0.144938198681D-03	0.2763020	0.2630620.03
9.8000	-0.1942206D-02	6.3903303D-01	0.73753575D-02	-0.146223588658D-03	0.2762204	0.2629190.03
9.9000	-0.80765968D-02	6.3884063D-01	0.26764738D-02	-0.14705598255D-03	0.2762614	0.26261610.03
10.0000	-0.22032059D-01	6.3859499D-01	0.4593256D-02	-0.14868997842D-03	0.2774860	0.2627750.03
10.1000	-0.30295162D-01	6.3829582D-01	0.5433902D-02	-0.1494900306D-03	0.2779690	0.2624900.03
10.2000	-0.899822D-01	6.3794285D-01	0.101073D-02	-0.1494900306D-03	0.2784510	0.2623470.03
10.3000	-0.52632986D-02	6.3753575D-01	0.1884894D-02	-0.150277593679D-03	0.2789320	0.2622040.03
10.4000	-0.3212529D-02	6.3707429D-01	0.723710D-02	-0.15105189584D-03	0.2794140	0.2620610.03
10.5000	-0.80765968D-02	6.3655581D-01	0.8465546D-02	-0.152557012910D-03	0.2798890	0.2619180.03
10.6000	-0.22032059D-01	6.3598714D-01	0.9976359D-02	-0.153286120600D-03	0.2803650	0.2617750.03
10.7000	-0.1973338D-02	6.3536093D-01	0.1089822D-02	-0.153998218199D-03	0.2813120	0.2616320.03
10.8000	-0.17036746D-02	6.3467972D-01	0.1182430D-01	-0.15469206935D-03	0.2817830	0.2613460.03
10.9000	-0.149753889D-02	6.3394193D-01	0.1275449D-01	-0.155367689140D-03	0.2822520	0.2612020.03

TIME (MIN) AZ RATE (DEG/SEC) ELEVATION (DEG)  
 11.0000 0.13348263D-02 0.3314865D-01  
 11.1000 0.1202919D-02 0.3229921D-01  
 11.2000 0.10937558D-02 0.3139337D-01  
 11.3000 0.1001844D-02 0.3043092D-01  
 11.4000 0.9232577D-03 0.2941163D-01  
 11.5000 0.8554177D-03 0.2833532D-01  
 11.6000 0.7965111D-03 0.2720171D-01  
 11.7000 0.74366794D-03 0.2601082D-01  
 11.8000 0.697652D-03 0.2476226D-01  
 11.9000 0.6553181D-03 0.2345559D-01  
 12.0000 0.61763063D-03 0.2209179D-01  
 12.1000 0.5834519D-03 0.2066954D-01  
 12.2000 0.5522749D-03 0.1918912D-01  
 12.3000 0.52375108D-03 0.1765039D-01  
 12.4000 0.49739725D-03 0.1605326D-01  
 12.5000 0.47308565D-03 0.1439763D-01  
 12.6000 0.45053239D-03 0.1268342D-01  
 12.7000 0.42953913D-03 0.1091056D-01  
 12.8000 0.40993563D-03 0.978993D-01  
 12.9000 0.39157962D-03 0.7186688D-01  
 13.0000 0.37434271D-03 0.5239618D-01

EL RATE (DEG/SEC)  
 -0.1361867D-01 -0.13602306254D-03  
 -0.1466673D-01 -0.15665750018D-03  
 -0.155852D-01 -0.15726996283D-03  
 -0.165392D-01 -0.1578593582181D-03  
 -0.176278D-01 -0.15842468441D-03  
 -0.184497D-01 -0.158964774252D-03  
 -0.1937031D-01 -0.159478544683D-03  
 -0.2032865D-01 -0.159964874820D-03  
 -0.218983D-01 -0.1604226285D-03  
 -0.222367D-01 -0.160850663280D-03  
 -0.2324998D-01 -0.1612762539D-03  
 -0.248858D-01 -0.161612950304D-03  
 -0.248858D-01 -0.161612950304D-03  
 -0.2515927D-01 -0.161944871208D-03  
 -0.261184D-01 -0.16224241357D-03  
 -0.271610D-01 -0.1625440316D-03  
 -0.280182D-01 -0.162729663589D-03  
 -0.2903878D-01 -0.1629170408D-03  
 -0.295392D-01 -0.163065285155D-03  
 -0.3003675D-01 -0.163173308285D-03  
 -0.3101549D-01 -0.16323992371D-03  
 -0.319475D-01 -0.163263983312D-03  
 -0.329428D-01 -0.163263983312D-03

END OF OUTPUT

REENTRY ANGLE  
 0.261059D-03 0.26120D-03  
 0.283185D-03 0.26916D-03  
 0.283485D-03 0.26916D-03  
 0.284109D-03 0.266629D-03  
 0.284567D-03 0.261485D-03  
 0.285024D-03 0.260344D-03  
 0.285778D-03 0.261197D-03  
 0.285130D-03 0.26053D-03  
 0.285130D-03 0.25699D-03  
 0.28636D-03 0.25309D-03  
 0.288827D-03 0.253765D-03  
 0.288272D-03 0.25621D-03  
 0.28714D-03 0.254747D-03  
 0.288153D-03 0.253331D-03  
 0.288590D-03 0.25186D-03  
 0.289125D-03 0.25941D-03  
 0.28956D-03 0.25896D-03  
 0.289885D-03 0.250751D-03  
 0.290312D-03 0.25605D-03  
 0.290335D-03 0.256459D-03  
 0.291155D-03 0.256313D-03  
 0.291573D-03 0.228167D-03

RADAR PARAMETER DIFFERENCES (PERTURBED-NOMINAL)

TIME MINUTES	SL RANGE FEET	SL RANGE RATE FEET/SEC.	SL RANGE RATE DOT FEET/SEC/SEC	AZIMUTH DEGREES	AZIMUTH DEGREES	AZIMUTH DEGREES	AZIMUTH RATE DEGREES/SEC	AZIMUTH RATE DEGREES/SEC
<b>AZIMUTH RATE DOT</b>								
<b>ELEVATION RATE</b>								
<b>DEGREES/SEC</b>								
5.800	0.10165396160 U4 0.27758921950-U6	0.27061306880 01 0.615572732D-02	-0.4704566608D-02 0.1956923872D-04	0.4218425600D-02 0.2768749184D-07	0.1907269232D-04	0.1907269232D-04	0.2876867456D-07	0.2876867456D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
5.900	0.10326905680 U4 0.28778493765-U6	0.267733136UD 01 0.6273647552D-02	-0.4895430976D-02 0.1973860000D-04	0.4333619968D-02 0.2985705780D-07	0.1932539136D-04	0.1932539136D-04	0.2876867456D-07	0.2876867456D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.000	0.10486652300 U4 0.2986701340-U6	0.264738288UD-01 0.6392603456D-02	-0.5087620992D-02 0.199147248D-04	0.4450329289D-02 0.2985705780D-07	0.1957761872D-04	0.1957761872D-04	0.2985705780D-07	0.2985705780D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.100	0.10644568540 U4 0.310903880-U6	0.2616227184D 01 0.6512633504D-02	-0.5281175296D-02 0.2008689760D-04	0.4568580144D-02 0.3095127136D-07	0.1982921936D-04	0.1982921936D-04	0.3095127136D-07	0.3095127136D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.200	0.10800582720 U4 0.3227816192D-06	0.2584005952D 01 0.66337379456D-02	-0.5476142784D-02 0.2028591232D-04	0.4688278400D-02 0.3205442144D-07	0.20088007328D-04	0.20088007328D-04	0.3205442144D-07	0.3205442144D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.300	0.10954626080 U4 0.3561671949D-06	0.2550560576D 01 0.6756078464D-02	-0.5672572096D-02 0.2048154832D-04	0.4809509248D-02 0.3315826048D-07	0.2033009040D-04	0.2033009040D-04	0.3315826048D-07	0.3315826048D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.400	0.11106626420 U4 0.3515628000D-06	0.2515952064D 01 0.6879571328D-02	-0.5870511744D-02 0.2068383168D-04	0.4932237120D-02 0.3426933888D-07	0.2057905040D-04	0.2057905040D-04	0.3426933888D-07	0.3426933888D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.500	0.1125651392D 04 0.3660780672D-06	0.24801112296D 01 0.7004297792D-02	-0.6070010048D-02 0.2089278336D-04	0.5056455616D-02 0.353811969D-07	0.208826920485D-04	0.208826920485D-04	0.353811969D-07	0.353811969D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.600	0.1140421584D 04 0.3828373152D-06	0.2443088736D 01 0.7130299048D-02	-0.627115008D-02 0.2210841824D-04	0.518215796D-02 0.364966028D-07	0.2107353680D-04	0.2107353680D-04	0.364966028D-07	0.364966028D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.700	0.1154966000 U4 0.4039841728D-06	0.2404855592D 01 0.7257612160D-02	-0.6473874368D-02 0.243307448D-04	0.5309335296D-02 0.3761090112D-07	0.2131876608D-04	0.2131876608D-04	0.3761090112D-07	0.3761090112D-07
<b>ANGULAR SEPARATION IN RADAR BEAM = ,</b>								
6.800	0.1169274980 U4 0.4216828928D-06	0.2365398848D 01 0.7386283384D-02	-0.667835296D-02 0.2152976640D-04	0.543797980D-02 0.3872863136D-07	0.2156247328D-04	0.2156247328D-04	0.3872863136D-07	0.3872863136D-07

		ANGULAR SEPARATION IN RADAR BEAM = ,	0.9172173312D-02	
6.900	0.1181348336D 04	0.2324711072D 01	-0.6884544320D-02	0.55668081600D-02
	0.4421251254D-06	0.7516342784D-02	0.2179547904D-04	0.396431936D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.354086912D-02		
7.000	0.1197171376D 04	0.2282780704D 01	-0.7092547584D-02	0.5699630336D-02
	0.4655530556D-06	0.7647839488D-02	0.2203187264D-04	0.4095352768D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.9538093824D-02		
7.100	0.121739216D 04	0.2239596832D 01	-0.730390336D-02	0.5832614784D-02
	0.4911655351D-06	0.7780810560D-02	0.2228892896D-04	0.4206221024D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.972421760UD-02		
7.200	0.122404400D 04	0.2195148256D 01	-0.7514116928D-02	0.5967022656D-02
	0.5193275210D-06	0.7915295872D-02	0.2254262432D-04	0.4316624064D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.9912480512D-02		
7.300	0.1237078448D 04	0.2149423584D 01	-0.7727770944D-02	0.6102841088D-02
	0.5513787207D-06	0.8151335232D-02	0.2280492608D-04	0.4426628160D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1010290392D-01		
7.450	0.1249834496D 04	0.2102411056D 01	-0.7943594816D-02	0.6240056064D-02
	0.5847478848D-06	0.8188968192D-02	0.2303794888D-04	0.4535553732D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1029550872D-01		
7.500	0.1262604912D 04	0.254n98880D 01	-0.8161029888D-02	0.6378652336D-02
	0.6229954016D-06	0.8328233856D-02	0.2334918240D-04	0.4643830016D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.104903140BD-01		
7.600	0.1274481134D 04	0.2u04474464D 01	-0.8380715968D-02	0.6518615488D-02
	0.6655587692D-06	0.8469171264D-02	0.2363303392D-04	0.4750954816D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1068733872D-01		
7.700	0.1286355872D 04	0.1953526064D 01	-0.8602491904D-02	0.6659927488D-02
	0.7134208256D-06	0.861181908D-02	0.2391928448D-04	0.4857163776D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1088660000D-01		
7.800	0.1297920816D 04	0.1901240464D 01	-0.8826394624D-02	0.6802571136D-02
	0.7673955840D-06	0.875621526D-02	0.2421386080D-04	0.4961760704D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1108811440D-01		
7.900	0.1319168112D 04	0.1847605024D 01	-0.9052459648D-02	0.6946527936D-02
	0.8285285636D-06	0.8902397824D-02	0.2451668064D-04	0.5065158528D-07
	ANGULAR SEPARATION IN RADAR BEAM = ,	0.1129189696D-01		
8.000	0.1321089207D 04	0.1792606512D 01	-0.9280720512D-02	0.7091778240D-02
				0.2431505312D-04

0.898304832D-06 0.950403840D-02 0.2462165344D-04 0.5167024000D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1149796192D-01

8.100 0.133676356D 0.4 0.173623156D 0.01 -0.951208960D-02 0.7238301568D-02 0.2452546476D-04  
0.9200269824D-05 0.9200269824D-02 0.251346768D-04 0.5267019200D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1170632192D-01

8.200 0.1341921264D 0.4 0.167846752D 0.01 -0.9743954688D-02 0.7386076480D-02 0.2473222016D-04  
0.1071373544D-05 0.9352031872D-02 0.255364064D-04 0.5364802176D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1191698896D-01

8.300 0.1350815351D 0.4 0.1619299872D 0.01 -0.9978984832D-02 0.7535080512D-02 0.2493515424D-04  
0.117948944D-05 0.9505725056D-02 0.257842366D-04 0.546095483QD-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1212997312D-01

8.400 0.136034992D 0.4 0.155871504D 0.01 -0.102163244D-01 0.7685290368D-02 0.2513409856D-04  
0.1301437681D-05 0.966138432UD-02 0.2610889504D-04 0.5954570112D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.12345288384D-01

8.500 0.1369516992D 0.4 0.1496699296D 0.01 -0.105599592D-01 0.7836681472D-02 0.2532490376D-04  
0.1459452532D-05 0.9819042944D-02 0.2644491168D-04 0.5645664446D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1256292880D-01

8.600 0.1378307504D 0.4 0.1433238432D 0.01 -0.1069801896D-01 0.7989228608D-02 0.2551939648D-04  
0.1642561824D-05 0.9978733952D-02 0.2648632128D-04 0.5734064896D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1272829156D-01

8.700 0.1386712928D 0.4 0.1368318333D 0.01 -0.1094241024D-01 0.8142905280D-02 0.25705419A4D-04  
0.1866083248D-05 0.1866083248D-01 0.1866083248D-01 0.273295904D-04 0.5819965632D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.130052424D-01

8.800 0.1396724512D 0.4 0.1301924784D 0.01 -0.118918352D-01 0.8297684552D-02 0.2586668144D-04  
0.2143144736D-05 0.1803043396D-01 0.1803043396D-01 0.2748464928D-04 0.5902628416D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1322992236D-01

8.900 0.1402332992D 0.4 0.1234043328D 0.01 -0.113834912D-01 0.8453537472D-02 0.2606340992D-04  
0.2492710304D-05 0.1947031480D-01 0.1947031480D-01 0.2784120480D-04 0.5982053952D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1345696048D-01

9.000 0.1416306064D 0.4 0.1164659744D 0.01 -0.1168991424D-01 0.8610435556D-02 0.2623505920D-04  
0.294402256D-05 0.1863844344D-01 0.1863844344D-01 0.282242496D-04 0.6058053248D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1368634640D-01

9.100 0.1416306064D 0.4 0.1193759616D 0.01 -0.119388192D-01 0.876834032D-02 0.2640160446D-04  
0.3537652832D-05 0.1808087528D-01 0.1808087528D-01 0.2856809856D-04 0.6130435664D-07

ANGULAR SEPARATION IN RADAR BEAM # 0.1391808840D-01

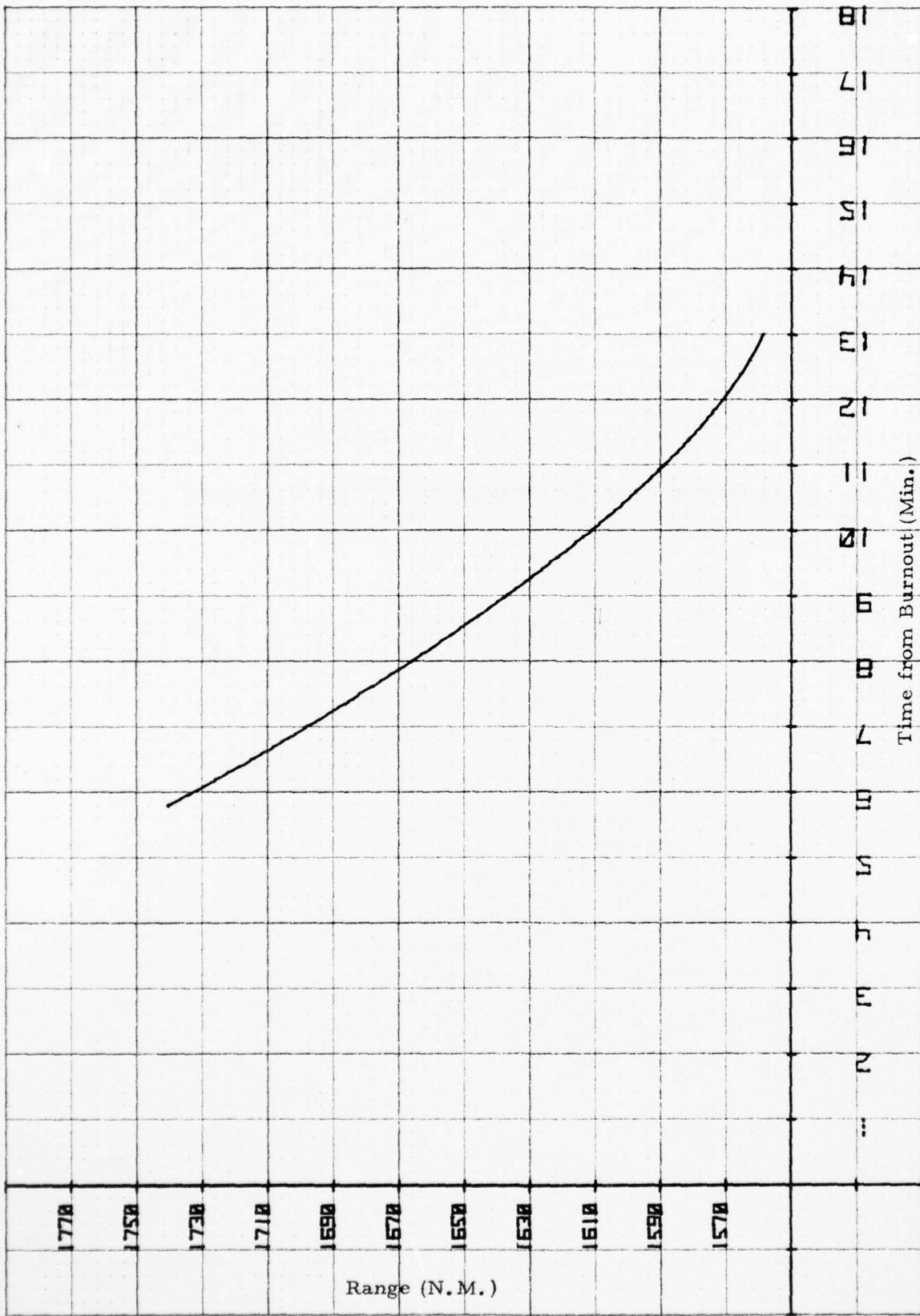
9.26	0.226518330	0.12328344D 01	-0.1220025152D-01	0.8927244160D-02	0.2656287488D-04
9.30	0.14285587360	0.947351744D 00	*0.1245901868D-01	0.9087091840D-02	0.2671873312D-04
	0.54891123340-U5	0.1115601680D-01	0.2031189504D-04	0.6263363584D-07	
9.4.0	0.14340171520	0.8718153856D 00	*0.1272017472D-01	0.9247857792D-02	0.2686902592D-04
	0.7196369280-U5	0.1133301920D-01	0.2968953024D-04	0.6323510336D-07	
9.5.0	0.1439017521D	0.4	0.7947049344D 00	*0.1298370608D-01	0.9409508608D-02
	0.9840101888D-U5	0.1151229808D-01	0.3007064320D-04	0.6379418880D-07	0.2701359616D-04
9.6.0	0.14435502560	0.4	0.71600161568D 00	*0.1324959456D-01	0.9572009216D-02
	0.14395352360-U4	0.1169387328D-01	0.3045495744D-04	0.6430322944D-07	0.2715222912D0-04
9.7.0	0.144760624	D 04	0.6357050880D 00	-0.1351781767D-01	0.9735324160D-02
	0.2321506272D-U4	0.1187776336D-01	0.3584218176D-04	0.6476196672D-07	0.2728498688D-04
9.8.0	0.14511756360	0.4	0.5537877888D 00	*0.1378834704D-01	0.9899416832D-02
	0.44011712540-U4	0.1206398460D-01	0.3123201184D-04	0.6517197248D-07	0.2741154560D-04
9.9.0	0.1454248528D	0.4	0.470240496D 00	-0.106114928D-01	0.1006425008D-01
	0.1152626944D-03	0.1225255216D-01	0.3162412928D-04	0.6552551360D-07	0.2753180320D-04
10.0.0	0.1456815360	0.4	0.3850044784D 00	-0.133361856D-01	0.1022978568D-01
	0.8264761152D-U3	0.1244347824D-01	0.3201820160D-04	0.658222688D-07	0.2764560224D-04
10.1.0	0.1458865744D	0.4	0.2982017920D 00	*0.1461341120D-01	0.1039598488D-01
	0.169334514 D-U2	0.1263677376D-01	0.3413885224D-04	0.6606003456D-07	0.2775299168D-04
10.2.0	0.1460393360	0.4	0.2096843120D 00	-0.1489277520D-01	0.1056280776D-01
	0.1412686734D-U3	0.1263244736D-01	0.3281080960D-04	0.6623660920D-07	0.2785359296D-04
10.3.0	0.146137872	D 04	0.1194843616D 00	*0.1517422046D-01	0.1073021440D-01
	0.4779776934D-U4	0.1303650512D-01	0.3320860632D-04	0.6635163200D-07	0.2794744460D-04
10.4.0	AP SEPARATION IN RADAR BEAM = ,				
	0.1687991600D-01				

10.400 0.14518208480 0.4 0.2758965216D-01 -0.1545768352D-01 0.1089816336D-01 0.2803439840D-04  
 0.2357014454D-04 0.1323095152D-01 0.3360688800D-04 0.639731072D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1714141312D-01  
 10.500 0.1461706454D 0.4 -0.661171646D-01 \*0.157430376D-01 0.1106661328D-01 0.2811434720D-04  
 0.1396570648D-04 0.1333378800D-01 0.3400524352D-04 0.6637513920D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1740507360D-01  
 10.600 0.1461025216D 0.4 -0.1613312208D 0.0 \*0.1603037424D-01 0.1423552144D-01 0.2618719040D-04  
 0.9135584000D-05 0.133901376D-01 0.3440325568D-04 0.6628290176D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1762086976D-01  
 10.700 0.1459766848D 0.4 -0.2583798176D 0.0 \*0.1631944000D-01 0.1140484512D-01 0.2825262848D-04  
 0.6480029152D-05 0.1384662544D-01 0.3480049024D-04 0.6611653632D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1793877168D-01  
 10.800 0.1457950120D 0.4 -0.3571679488D 0.0 \*0.166101952D-01 0.1157454080D-01 0.2831117248D-04  
 0.4805893952D-05 0.14056661712D-01 0.3519649920D-04 0.6567385280D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1620874736D-01  
 10.900 0.1455477522D 0.4 -0.4577053568D 0.0 \*0.1690255392D-01 0.1174456448D-01 0.2836213152D-04  
 0.3699780544D-05 0.1426898016D-01 0.3559081920D-04 0.6555268160D-07  
 11.0 154 ANGULAR SEPARATION IN RADAR BEAM # , 0.1848076256D-01  
 11.000 0.145245194D 0.4 -0.5600015104D 0.0 \*0.1719639456D-01 0.1191487136D-01 0.2840564160D-04  
 0.2932466656D-05 0.1448370272D-01 0.3598297248D-04 0.6515087680D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1875478080D-01  
 11.100 0.1448753776D 0.4 -0.66460648832D 0.0 \*0.1749160672D-01 0.1208541712D-01 0.28444162696D-04  
 0.2379334016D-05 0.1470077052D-01 0.3637246752D-04 0.6466632768D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1903076352D-01  
 11.200 0.1444452816D 0.4 -0.7699032960D 0.0 \*0.1778866720D-01 0.1225615568D-01 0.2847002304D-04  
 0.1968078352D-05 0.1492016608D-01 0.3675876968D-04 0.6409696064D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1930866912D-01  
 11.300 0.1439511376D 0.4 -0.8745239168D 0.0 \*0.180856320D-01 0.1242704208D-01 0.2849077632D-04  
 0.1654435104D-05 0.1544186880D-01 0.3714144800D-04 0.6343889344D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1956845488D-01  
 11.400 0.1433919041D 0.4 -0.969329536D 0.0 \*0.1838419472D-01 0.1259802976D-01 0.2850383872D-04  
 0.1410092496D-05 0.1565585488D-01 0.375188064D-04 0.6269015168D-07  
 ANGULAR SEPARATION IN RADAR BEAM # , 0.1987007424D-01  
 11.500 0.14276645576D 0.4 -0.198135904D 0.1 \*0.1868357184D-01 0.1276907264D-01 0.2850917024D-04  
 0.1216265128D-05 0.159209776D-01 0.378935508D-04 0.6185067392D-07

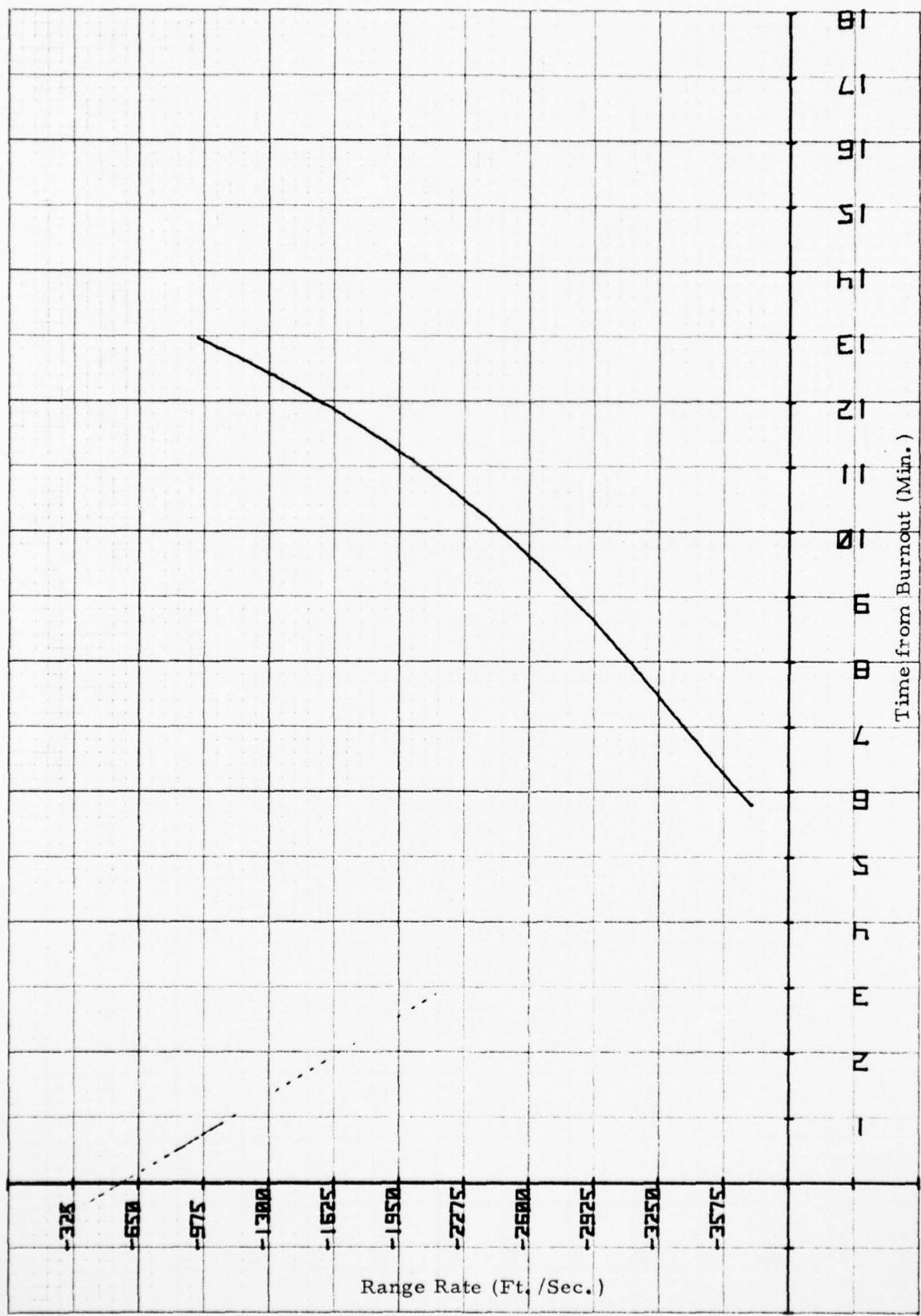
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11.600	0.1426737728D 04 0.1066108320D-05	-0.1211137168D 01 0.1582056688D-01	-0.1898361680D-01 0.3826189920D-04 0.6091675904D-07
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2043861904D-01	
11.700	0.1413127350D 04 0.9325814272D-05	-0.1325940304D 01 0.1605122864D-01	-0.1928416192D-01 0.3862435520D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2072544032D-01	
11.800	0.1416828000D 04 0.8271928128D-06	-0.134254776UD 01 0.1628404624D-01	-0.1958513088D-01 0.3898033440D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2101388736D-01	
11.900	0.1395813216D 04 0.7391783424D-06	-0.1560960928D 01 0.1651897856D-01	-0.1988603776D-01 0.3932242888D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2130390128D-01	
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ANGULAR SEPARATION IN RADAR BEAM #	,	0.2159542112D-01	
12.100	0.137535408D 04 0.6018945560D-06	-0.1803024272D 01 0.1699500776D-01	-0.2048767632D-01 0.4000341164D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2168838336D-01	
12.200	0.1364445648D 04 0.5478453535D-06	-0.1927031248D 01 0.1723600480D-01	-0.2078788992D-01 0.4032743072D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2218272096D-01	
12.300	0.1352574888D 04 0.501211168D-06	-0.252657552D 01 0.1747891776D-01	-0.2108740464D-01 0.4064189568D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2247836512D-01	
12.400	0.1339810128D 04 0.467138556D-06	-0.218007824UD 01 0.1772368720D-01	-0.2138598800D-01 0.4094616416D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2277524416D-01	
12.500	0.132632944D 04 0.425330320D-06	-0.230928704UD 01 0.1797024992D-01	-0.2168339840D-01 0.4123986240D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2307328256D-01	
12.600	0.131205132D 04 0.3942517952D-06	-0.2440276192D 01 0.1821853920D-01	-0.219738400D-01 0.415250528D-04
ANGULAR SEPARATION IN RADAR BEAM #	,	0.2337240320D-01	
12.700	0.1297056180D 04 0.3668008736D-06	-0.2573036288D 01 0.1846848384D-01	-0.2227368544D-01 0.4179126048D-04
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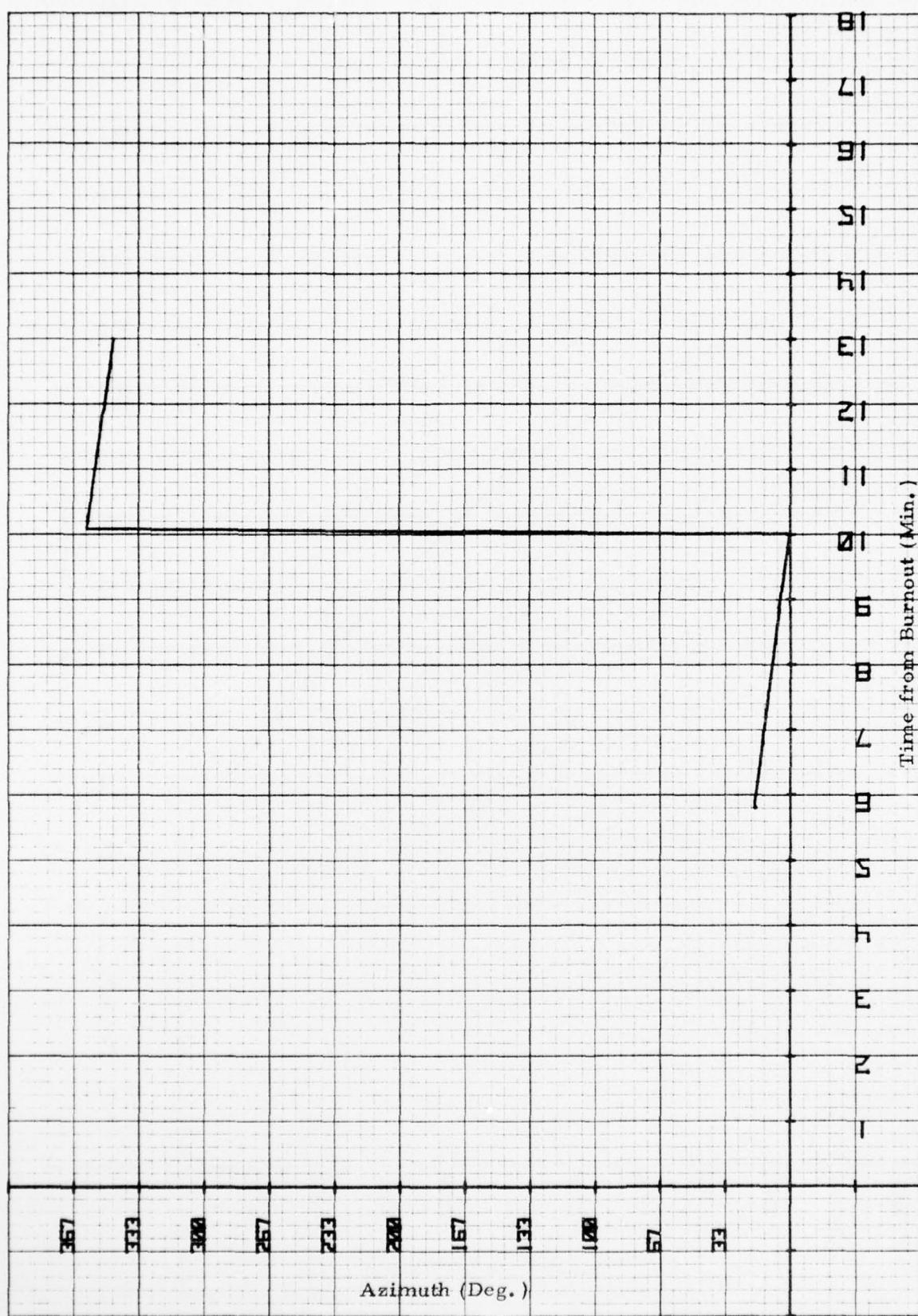
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0.3424306080D-06    0.187200864D-01    0.42048185280-04	0.41715102080-07
ANGULAR SEPARATION IN RADAR BEAM = ,	0.2397356672D-01
12.900    0.126455192D 04    -0.2843824224D 01    -0.228561680D-01	0.15143346880D-01    0.2776919104D-04
0.321701424D-06    0.1897303504D-01    0.4229451088D-04	0.39407681560D-07
ANGULAR SEPARATION IN RADAR BEAM = ,	0.2427544064D-01
13.000    0.1247085824D 04    -0.2981825216D 01    -0.2314374304D-01	0.1930963632D-01    0.2765940928D-04
0.3012415838D-06    0.1922747952D-01    0.4252086624D-04	0.3689197536D-07
ANGULAR SEPARATION IN RADAR BEAM = ,	0.2457805792D-01

Plots from the Sample Output (for the first trajectory)

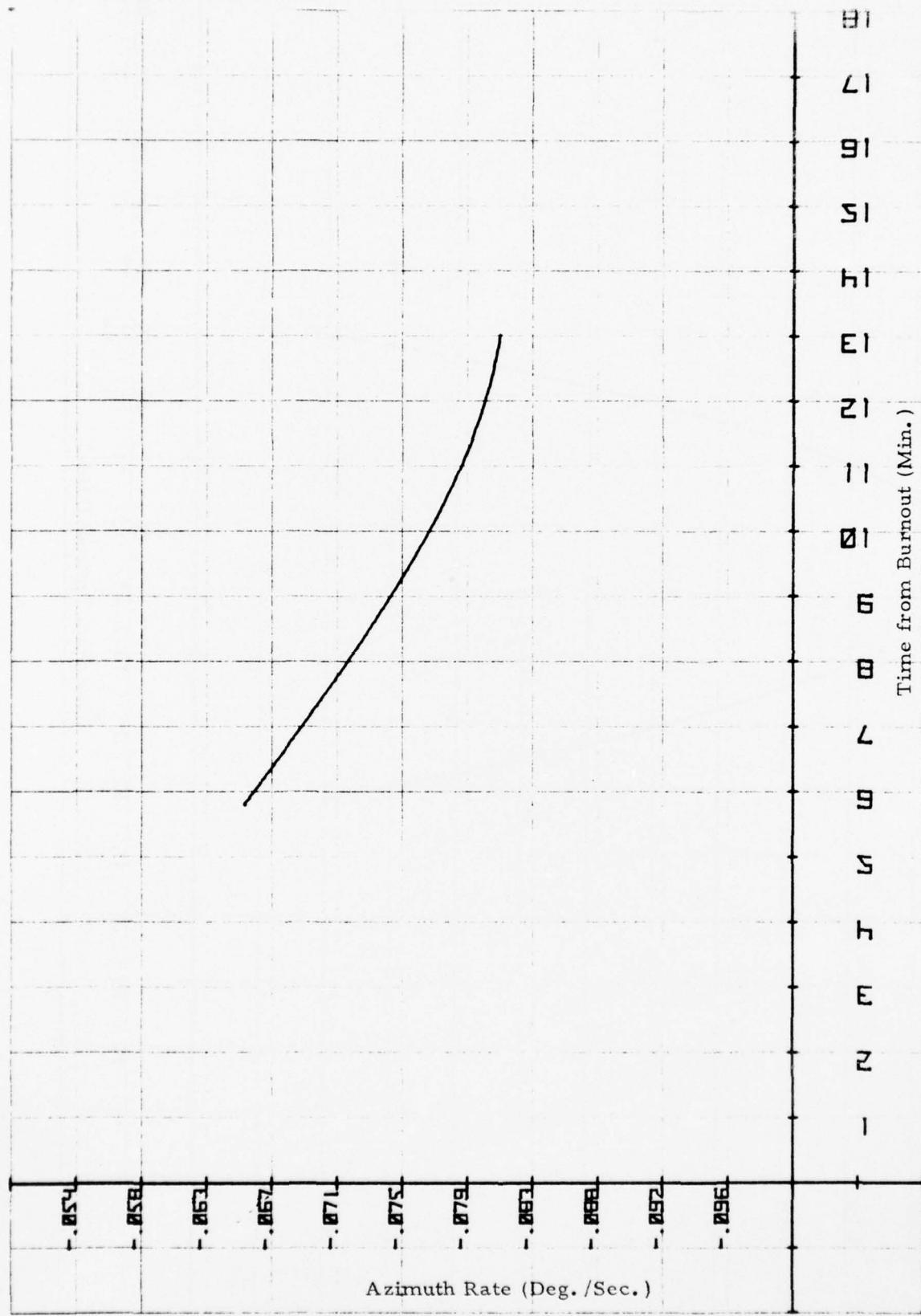


III-158

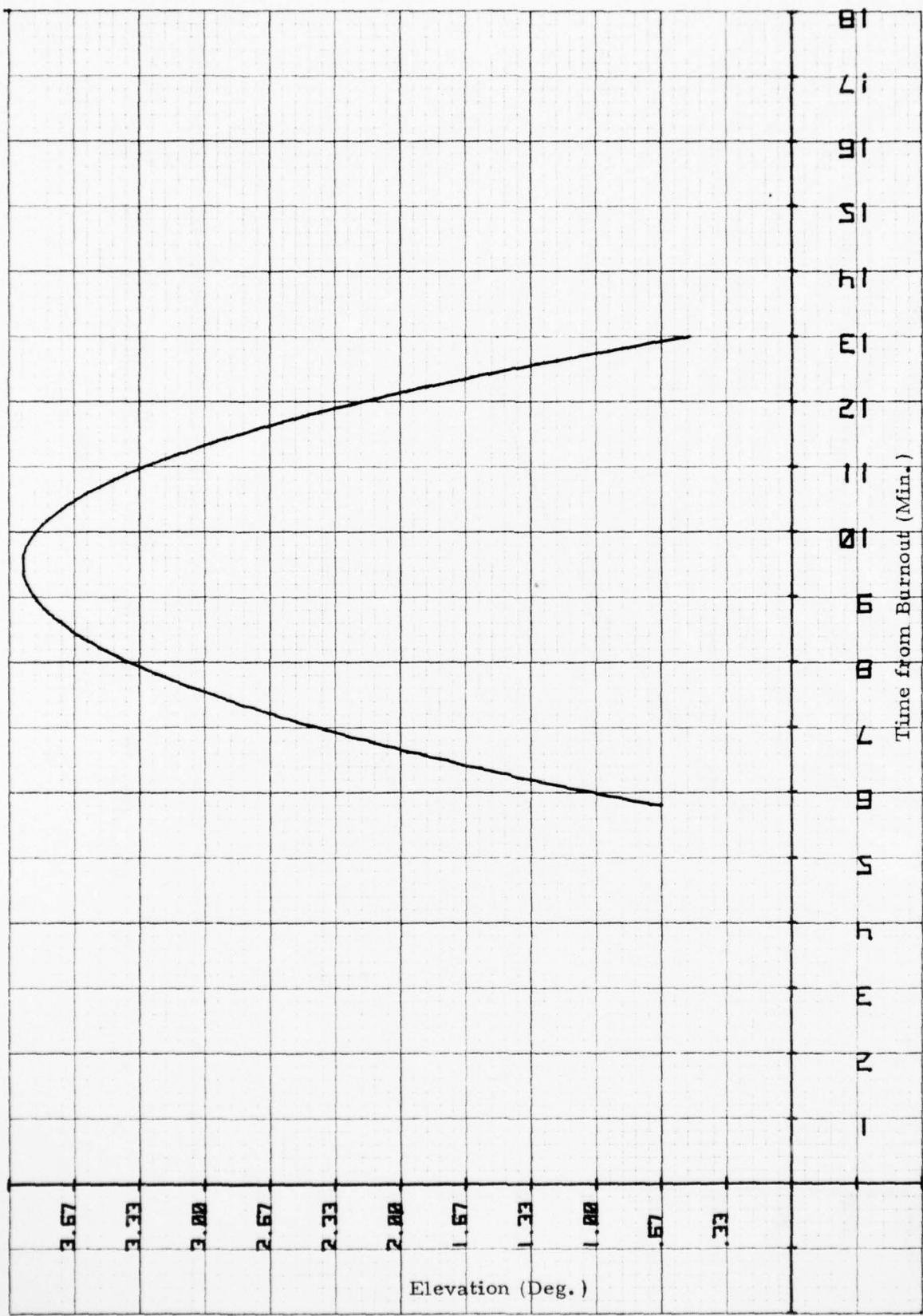




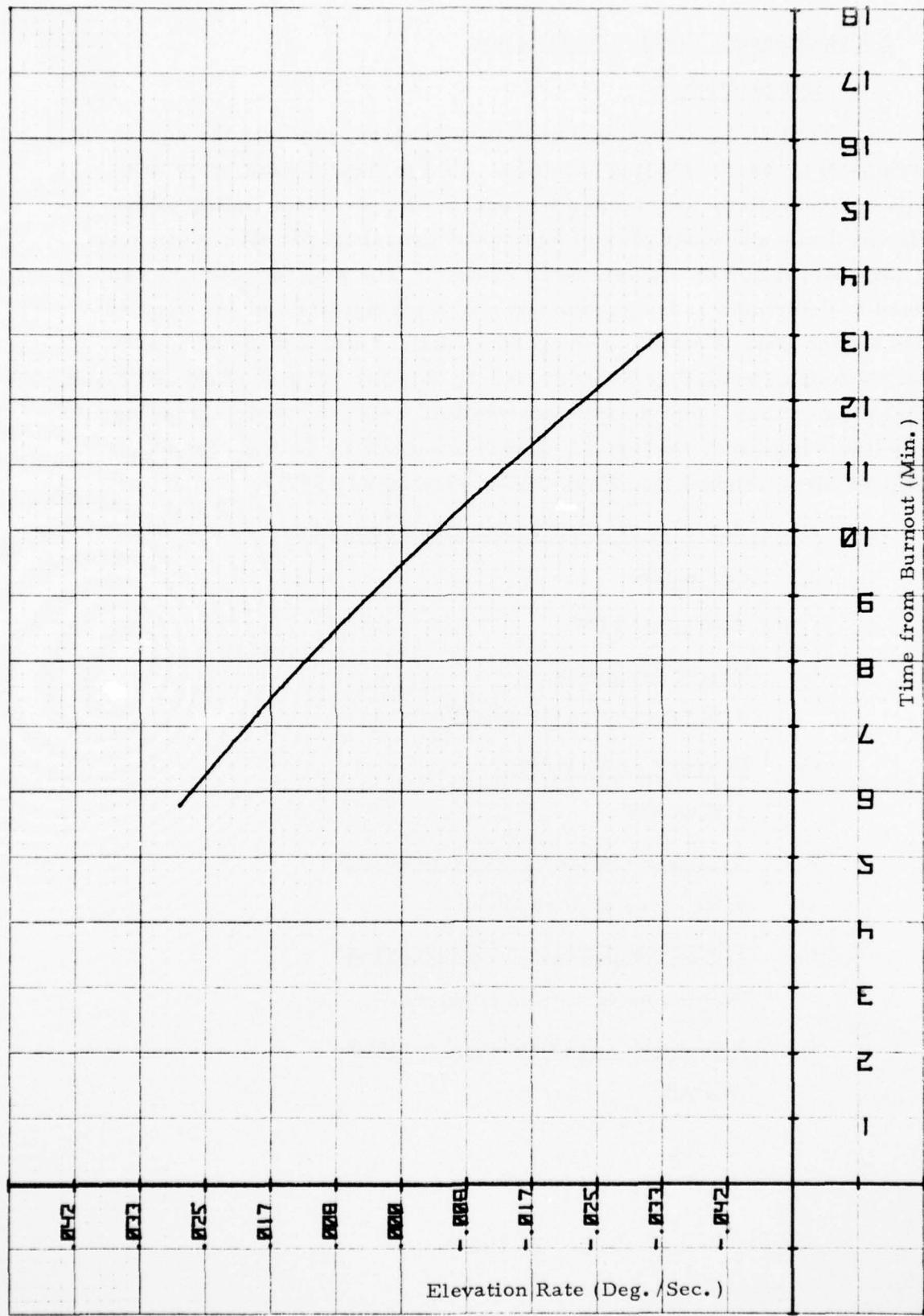
HEWLETT-Packard 970-1006



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D. Nodal Crossing Prediction Program

1. Introduction

The Nodal Crossing Prediction Program predicts the equatorial crossings of an earth-orbiting satellite. Two to three weeks prior to a satellite observation, the computer program can provide a listing of the predicted times and longitudes of equatorial crossings for all passes suitable for observation by a given radar system. The program outputs can be used to determine radar acquisition and tracking data and are used as inputs for the Orbit Prediction Program. Orbital element inputs for the Nodal Crossing Prediction Program can be obtained from the SPACETRACK orbital element set. For further information, refer to "Nodal Crossing Prediction Program", by John C. Cleary and Paul E. Brown, 1st Lt., Technical Memorandum No. EMA-TM-66-9, March 1967.

2. Computer Program Operating Environment

a. Computer

Honeywell 6180.

b. Source Language

FORTRAN Y under GCOS.

c. Memory Requirement

17K words

d. Typical Processing Time Required

0.001 hrs. (3.6 seconds)

e. Peripheral Equipment Requirement

No disc or tape files required.

f. Non-system Subroutines Required

CLEAR

### 3. Inputs

The following set of input parameters are required for the execution of the Nodal Crossing Prediction Program.

#### NAMELIST IN1

NCASE - Number of cases to be run.

#### NAMELIST IN2

HED - Array containing the heading for the output. The dimension of HED is 24.

#### NAMELIST IN3

NTYPE - Switch for selecting orbital elements type to be input.

=1 SPACETRACK or Smithsonian elements used as inputs.

=2 NASA elements.

NREV0 - First revolution of satellite to be examined for visibility from radar. The revolutions are counted from epoch time of the SPACETRACK bulletin.

NREV1 - Last revolution of satellite to be examined for visibility from radar.

#### NAMELIST IN4

BGT - Epoch time of nodal crossing bulletin in decimal days.  
BGT=39125-T where 39125 is January 1, 1966 in Julian Days  
and T is the epoch time.

XM0 - Mean anomaly in degrees.

RA0 - Right ascension of ascending node in degrees.

OMEGA0 - Argument of perigee (degrees).

E - Orbit eccentricity.

A - Mean motion (revolutions/day).

#### NAMELIST IN5

B - Rate of change of A (revolutions/day<sup>2</sup>).

RA1 - Rate of change of RA0 (degrees/day).

OMEGA1 - Rate of change of OMEGA0 (degrees/day).

GHA0 - Greenwich hour angle of Aries at midnight, 30 December of the previous year.

### NAMELIST IN6

ZLAM1 - Longitude of northbound nodal crossings that will give a Zenith pass at the radar (degrees).

ZLAM2 - Longitude of southbound nodal crossings that will give a Zenith pass at the radar (degrees).

DLAMDA - Longitude interval of nodal crossings that will give usable passes at the radar (degrees).

CHR - Difference between local time and Greenwich time.

= 4.0 EDT

= 5.0 EST

#### 4. Output

Output from the Nodal Crossing Prediction Program first consists of a list of the input parameters. This is followed by a listing of the nodal crossing data in the following form:

<u>Variable Name</u>	<u>Units</u>	<u>Description</u>
HED	None	Heading for output as input.
BGT	Decimal Days	Epoch time of nodal crossing bulletin.
NREV0, NREV1	None	Pass number. Indicates the first through last revolution of the satellite to be examined for visibility from the radar.
ZLAM1	Degrees	Longitude of northbound nodal crossings that will give a Zenith pass at the radar.
ZLAM2	Degrees	Longitude of southbound nodal crossings that will give a Zenith pass at the radar.
DLAMDA	Degrees	Longitude interval of nodal crossings that will give usable passes at the radar.
NDAY	Days	Day of year of nodal crossing.
NHR	Hours	Hour of day of nodal crossing.
MIN	Minutes	Minute of hour of nodal crossing.
NSEC	Seconds	Second of minute of nodal crossing.

<u>Variable Name</u>	<u>Units</u>	<u>Description</u>
PLAMDA	Degrees	Longitude of nodal crossing.

The printout produced from the variables HED through DLAMDA above serves as a heading for each page of nodal crossing data printed out. The nodal crossing times and longitude (variables NDAY through PLAMDA) are printed out in the order of ascending times on each page. Refer to the sample output.

AD-A033 657

PRC INFORMATION SCIENCES CO ROME N Y  
SPACE SURVEILLANCE SOFTWARE SUPPORT. VOLUME 1, PART 1, BOOK 1. --ETC(U)  
OCT 76 P R CONTI

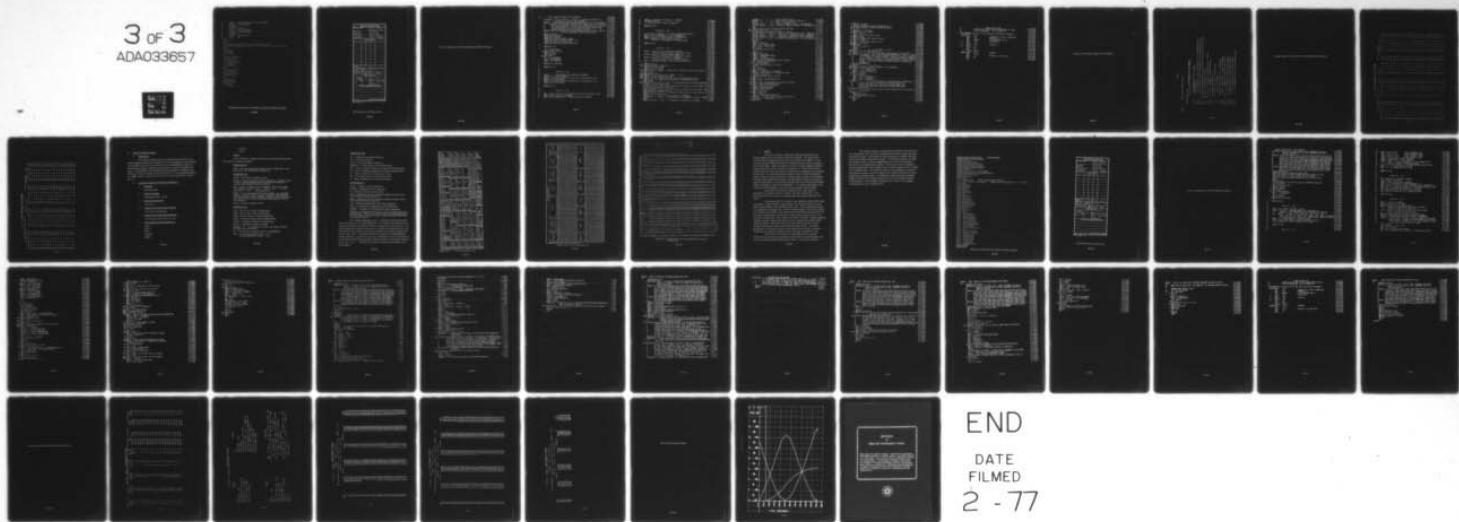
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RADC-TR-76-261-VOL-1-PT-1- NL

3 of 3  
ADA033657



END

DATE  
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2 - 77

```

$      IDENT    CLEARY,NEUFFER ,65121104RADC
$      USERID  CLEARY$THREE
$      LOADLOAD
$      OPTION   FORTRAN
$      SELECT   CLEARY/ONODAL
$      SELECT   CLEARY/OCLEAR
$      EXECUTE
$      LIMITS  20,20K,,10K
$      DATA     05

$IN1
  NCASE=1 $
$IN2
  HED(4)=3411 NODAL CROSSING PREDICTION PROGRAM,
  HED(14)=4711 SATELLITE NO. 049 - SPACETRACK - BLTN. 342 EDT$
$IN3
  NTYPE=1,
  NREVO=75,
  NREVI=460 $
$IN4
  BGT=118.03902403,
  MN10=203.7813,
  RAO=234.2461,
  SMEGAC=153.7564,
  E=0.0570891,
  A=12.76771656 $
$IN5
  D=0.255741E-03,
  RA1=-3.46557,
  SMEGA1=3.31952,
  GHA0=99.210 $
$IN6
  ZLAM1=134.2,
  ZLAM2=191.9,
  DLAMDA=50.0,
  CHR=4.0 $
$      ENDJOB

```

\*

#### Sample Job Stream for the Nodal Crossing Prediction Program

RADC 635/645 BATCH JOB				
SNUMB NUMBER 4/5/76	DATE 4/5/76	TIME 1115		
PROGRAMMER CONTI	TELEPHONE 339-1360			
RADC ENGINEER CLEARY	TELEPHONE 3573	SYMBOL OCSA		
TAPES ASSIGNED				
REEL NO.	WRITE	READ	DEN.	TITLE
PERIPHERALS ASSIGNED			<input checked="" type="checkbox"/> PRINTER <input type="checkbox"/> PUNCH	
<input checked="" type="checkbox"/> READER			<input type="checkbox"/> DISC. # OF LINKS _____	
<input type="checkbox"/> DRUM # OF LINKS _____				
CORE SIZE 20K	ACTIVITIES 1			
PROCESSOR TIME .01	ESTIMATED LINES OF PRINT 1,000			
TOTAL RUN TIME .01				
DECKS EXPECTED				
NO. OF BINARY DECKS None	NO. OF COMODECKS			
BMC	TAPE <input type="checkbox"/> DUMP <input type="checkbox"/> COPY			
FROM:	TO:	MODE <input type="checkbox"/> BCD <input checked="" type="checkbox"/> BINARY	NO. OF FILES	
SPECIAL OPERATOR INSTRUCTIONS				
(Use reverse side if required)				

RADC FORM 0-56 PREVIOUS EDITION WILL BE USED  
APR 69

HIS 6000 Batch Submittal Form

**Source Listing of the Nodal Crossing Prediction Program**

```

C NODAL CROSSING PREDICTION PROGRAM 00001000
C
C DIMENSION TO(1000),NDAY(1000),NHR(1000),MIN(1000),NSEC(1000), 00001010
C           XLAMDA(1000),PLAMDA(1000),HED(24) 00001020
C COMMON TU,NDAY,NHR,MIN,NSEC,XLAMDA,PLAMDA,HED,RAD,PI,NTYPE,NREV0, 00001030
C           NREV1,X,BGT,E,OMEGA1,OMEGA1,XM0,P,DELP,A,B,C,GHA0,GHA1,RA0, 00001040
C           RA1,ZLAM1,ZLAM2,PN,COSW,SINW,TERM,COSPH,SINPH,PHIP,DLAMDA, 00001050
C           XMP,TERM1,NPASS,REV,J,I,DAY,HOUR,YMIN,SEC,NPAGE,IPAGE, 00001060
C           JSTART,JEVD,NCOL,JC1,JC2,JC3,JC4,CHR,CDAY 00001070
C DOUBLE PRECISION GHA1,BGT,XM0,RA0,OMEGA0,E,A,B,RA1,OMEGA1,GHA0,P, 00001080
C           PN,TERM,TERM1,DELP,C,XMP,PI,RAD,DSQRT 00001090
C
C DATA BLANK/6H / 00001100
C NAMELIST/IN1/NCASE 00001110
C NAMELIST/IN2/HED 00001120
C NAMELIST/IN3/NTYPE,NREV0,NREV1 00001130
C NAMELIST/IN4/BGT,XM0,RA0,OMEGA0,E,A 00001140
C NAMELIST/IN5/B,RA1,OMEGA1,GHA0 00001150
C NAMELIST/IN6/ZLAM1,ZLAM2,DLAMDA,CHR 00001160
C
C READ(05,IN1) 00001170
C
C DO 51 N=1,NCASE 00001180
C 51 CALL CLEAR(TO,CDAY) 00001190
C DO 99 I=1,24 00001200
C HED(I)=BLANK 00001210
C 99 CONTINUE 00001220
C PI = 3.1415926536 00001230
C RAD = .0174532925 00001240
C GHA1 = 360.9856473 00001250
C
C READ(05,IN2,END=51) 00001260
C
C READ(05,IN3) 00001270
C
C READ(05,IN4) 00001280
C
C NAMELIST - IN3 00001290
C
C NTYPE = 1 - SPACETRACK OR SMITHSONIAN ELEMENTS 00001300
C NTYPE = 2 - NASA ELEMENTS 00001310
C NREV0 = FIRST REVOLUTION OF SATELLITE TO BE EXAMINED FOR 00001320
C VISIBILITY FROM RADAR 00001330
C NREV1 = LAST REVOLUTION OF SATELLITE TO BE EXAMINED FOR 00001340
C VISIBILITY FROM RADAR 00001350
C
C READ(05,IN4) 00001360
C
C NAMELIST - IN4 00001370
C
C BGT = EPOCH TIME OF NODAL CROSSING BULLETIN IN DECIMAL DAYS 00001380
C XM0 = MEAN ANOMALY IN DEGREES 00001390
C RA0 = RIGHT ASCENSION OF ASCENDING NODE IN DEGREES 00001400
C

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C OMEGA0 = ARGUMENT OF PERIGEE IN DEGREES          00001520
C E = ECCENTRICITY                                00001530
C A = MEAN MOTION IN REVOLUTIONS/DAY              00001540
C
C READ(05,IN5)
C
C NAMELIST - IN5
C
C B = RATE OF CHANGE OF A IN REVOLUTIONS/(DAY-SQUARED) 00001610
C RA1 = RATE OF CHANGE OF RA0 IN DEGREES/DAY          00001620
C OMEGA1 = RATE OF CHANGE OMEGA0 IN DEGREES/DAY        00001630
C GHA0 = GREENWICH HOUR ANGLE OF ARIES AT             00001640
C MIDNIGHT, 30 DECEMBER OF PREVIOUS YEAR            00001650
C
C READ(05,IN6)
C
C NAMELIST - IN6
C
C LAM1 = LONGITUDE OF NORTHEWARD CROSSING           00001720
C THAT WILL GIVE A ZENITH PASS AT THE RADAR          00001730
C LAM2 = LONGITUDE OF SOUTHWARD CROSSING             00001740
C THAT WILL GIVE A ZENITH PASS AT THE RADAR          00001750
C DLAMDA = LONGITUDE INTERVAL OF CROSSINGS          00001760
C THAT WILL GIVE USEABLE PASSES AT RADAR            00001770
C GMR = DIFFERENCE BETWEEN LOCAL AND GREENWICH TIME 00001780
C
C WRITE(06,9001)
9001 FORMAT(1H1,49X,'- INPUTS -')                  00001800
IF(N.GT.1) GO TO 998
9002 WRITE(06,9002) NCASE                         00001810
9003 FORMAT(//10X,'THIS IS RUN NUMBER   ',I2)       00001820
9004 WRITE(06,9004) (HED(I),I=1,24)                00001830
9005 FORMAT(//19X,'OUTPUT HEADING (HED)',/24X,12A6,/24X,12A6) 00001840
WRITE(06,9005) NTYPE,NREV ,NREV1,BGT,XMC,RA0,OMEGA0,E,A,B,
  *A1,OMEGA1                                         00001850
  *B1,OMEGA1                                         00001860
  *C1,OMEGA1                                         00001870
  *D1,OMEGA1                                         00001880
  *E1,OMEGA1                                         00001890
  *F1,OMEGA1                                         00001900
  *G1,OMEGA1                                         00001910
  *H1,OMEGA1                                         00001920
  *I1,OMEGA1                                         00001930
  *J1,OMEGA1                                         00001940
  *K1,OMEGA1                                         00001950
  *L1,OMEGA1                                         00001960
  *M1,OMEGA1                                         00001970
  *N1,OMEGA1                                         00001980
  *O1,OMEGA1                                         00001990
  *P1,OMEGA1                                         00002000
  *Q1,OMEGA1                                         00002010
  *R1,OMEGA1                                         00002020
  *S1,OMEGA1                                         00002030

```

```

*//19X,' E = ',F16.10,' ORBIT ECCENTRICITY',          00002040
*//19X,' A = ',F16.10,' MEAN MOTION IN REVOLUTIONS/DAY', 00002050
*//19X,' B = ',F16.10,' RATE IN CHANGE OF A',          00002060
*//19X,' RA1 = ',F16.10,' RATE OF CHANGE OF RAD IN DEGREES/DAY', 00002070
*//19X,'OMEGA1 = ',F16.10,'RATE OF CHANGE OF OMEGA IN DEGREES/DAY 00002080
*}
      WRITE(06,9006) GHAJ,ZLAM1,ZLAM2,DLAMDA,CHR           00002090
9006 FORMAT(/19X,'GAHJ = ',F16.10,                      00002100
*! GREENWICH HOUR ANGLE OF ARIES AT NIGHT',            00002110
*//19X,'ZLAM1 = ',F16.10,' LONGITUDE OF NORTHBOUND NODAL CROSSING',00002130
*//19X,'ZLAM2 = ',F16.10,' LONGITUDE OF SOUTHBOUND NODAL CROSSING',00002140
*//19X,'DLAMDA = ',F16.10,' LONGITUDE INTERVAL OF NODAL CROSSING',00002150
*//19X,'CHR = ',F16.10,' DIFFERENCE BETWEEN LOCAL TIME AND GREENWIC00002160
*! TIME',                                              00002170
*}
      DAY = CHR/24.0                                     00002180
      COSW = COS (OMEGA *RAD)                           00002200
      SINW = SIN (OMEGA *RAD)                           00002210
      M = 1D0/A                                         00002220
      IF (NTYPE.EQ.1) GO TO 6                          00002230
      M = A                                           00002240
      DELP = B                                         00002250
6 TERM = 1D0*E**2                                     00002260
      TERM = TERM*DSQRT(TERM)                           00002270
      TERM1 = E*COSW                                    00002280
      TERM1 = (1D0+TERM1)**2                            00002290
      PN = P*(1D0-OMEGA1*P*TERM/(360D0*TERM1))       00002300
7 IF (NTYPE.EQ.1) GO TO 9                          00002310
8 E = DELP*P/28800                                   00002320
C   2880 = 2*(1440 MIN IN A DAY)                   00002330
      DO TO 10                                         00002340
9 E = -B/A**3                                       00002350
      XM0 = XM0/360D0                                  00002360
10 COSPH = (COSW+E)/(1.0+E*COSW)                  00002370
      SINPH = SIGN (SQRT (1.0-COSPH**2)*SINW)        00002380
      IF(COSPH)<12.11.13                            00002390
11 PHIP = PI-SIGN (PI/2.0,SINPH)                  00002400
      DO TO 14                                         00002410
12 RMIP = ATAN (SINPH/COSPH)+PI                  00002420
      DO TO 14                                         00002430
13 PHIP = ATAN (SINPH/COSPH)+PI-SIGN (PI,SINPH)    00002440
14 XMP = (PHIP-E*SINPH)/(2D0*PI)                 00002450
      TERM = BGT+(1D0-XM0-XMP)*PN                  00002460
15 TERM1 = 360D0-RAJ+GHA1                         00002470
      NPASS = NREV1-NREV0+1                           00002480
      REV = NREV1-1                                  00002490
16 DO 18 I=1,NPASS                                 00002500
      REV = REV+1.0                                  00002510
      T0(I) = TERM+REV*PN+C*REV**2                 00002520
17 XLAMDA(I) = TERM1-RA1*(T0(I)-BGT)+GHA1*T0(I) 00002530
      XLAMDA(I) = AMOD(XLAMDA(I),360.)             00002540
18 CONTINUE                                         00002550

```

```

19 IF(20 I=1,NPASS
20 IF(ABS(XLAMDA(I)-ZLAM1)-DLAMDA)21,21,20
21 ZLAMDA(J1) = XLAMDA(I)
22 ZDAY(J) = T0(I)-CDAY
23 DAY = NDAY(J)
24 HOUR = (T0(I)-DAY)*24.0-CHR
25 MIN = (HOUR-FLOAT(NHR(J)))*60.0
26 SEC = (YMIN-FLAT(MIN(J)))*61.0
27 SEC(J) = SEC+.5
28 CONTINUE
29 PAGE = (J+99)/100
30 PAGE = 1
31 WRITE (6,1003)(HED(I),I=1,24)
1003 FORMAT(1H1,23X12A6/24X12A6//)
32 WRITE (6,1004)BGT,NREVU,NREV1,ZLAM1,ZLAM2,DLAMDA
1004 FORMAT(18X12HEPOCH TIME =F9.5,5H DAYS,37X8HPASS NO. 14,2R - 14/11X00002760
1 1UHLAMBDAZ1 =F8.3,22X1UHLAMBDAZ2 =F8.3,20X14HDELTA LAMBDA =00002770
2 F8.3 //3X3HDAY,1X3HHR.,1X4HMIN.,1X4HSEC.,1X6HLAMDA,6X3HDAY00002780
3 1X3HHR.,1X4HMIN.,1X4HSEC.,1X6HLAMDA,6X3HDAY,1X3HHR,1X4HMIN.00002790
4 1X4HSEC.,1X6HLAMDA,6X3HDAY,1X3HHR.,1X4HMIN.,1X4HSEC.,1X
5 6HLAMDA )
33 IF(NPAGE>28,28,29
34 WRITE (6,1005
1005 FORMAT(43X34HNO VISIBLE PASSES IN THIS INTERVAL )
35 JSTART = 100*(IPAGE-1)+1
36 JEND = MIN0(JSTART+99,J)
37 NCOL = (JEND-JSTART+4)/4
38 DO 32 I=1,NCOL
39 JC1 = JSTART+I-1
40 JC2 = MIN0(JC1+NCOL,J)
41 JC3 = MIN0(JC2+NCOL,J)
42 JC4 = MIN0(JC3+NCOL,J)
31 WRITE (6,1006)NDAY(JC1),NHR(JC1),MIN(JC1),NSEC(JC1),
1 PLAMDA(JC1),NDAY(JC2),NHR(JC2),MIN(JC2),NSEC(JC2),
2 PLAMDA(JC2),NDAY(JC3),NHR(JC3),MIN(JC3),NSEC(JC3),
3 PLAMDA(JC3),NDAY(JC4),NHR(JC4),MIN(JC4),NSEC(JC4),
4 PLAMDA(JC4)
1006 FORMAT(/I6,I4,I4,I4,F9.2,I9,I4,I4,I4,F9.2,I9,I4,I4,I4,F9.2,I9,I4,
1 I4,I4,F9.2 )
32 CONTINUE
33 PAGE = IPAGE+1
34 IF(IPAGE-NPAGE)>27,27,51
51 5CONTINUE
52 STOP
53 END

```

•	SUBROUTINE CLEAR	00001000	
•	SUBROUTINE TO SET FORTRAN LOCATIONS TO ZERO	00001010	
•	CALLING SEQUENCE - CALL CLEAR(X,Y)	00001020	
•		00001030	
•	THE PURPOSE OF CLEAR IS TO ZERO OUT LOCATIONS X THROUGH Y	00001040	
CLEAR	SAVE 1,4	00001050	
	LDA 2,1	ADDRESS OF X INTO A REGISTER	00001060
	SBA 3,1	ADDRESS OF Y	00001070
	TPL ORDER	Y IS GREATER THAN X	00001080
	LDX4 2,1	RESTORE X4	00001090
A2	STZ 1,4		00001100
	EAX4 1,4	INCRE X4	00001110
A1	BMPX4 3,1		00001120
	TNC A2		00001130
	TZE A2		00001140
	RETURN CLEAR		00001150
ORDER	LDX4 3,1	REORDER	00001160
	LDQ -1,DU		00001170
	ASQ A1	CHANGE A1 TO CMPM 2,1	00001180
	TRA A2		00001190
	END		00001200

**Listing of the Sample Input for the Program**

NCASE = 1      TOTAL NUMBER OF CASES TO BE RUN

- INPUTS -

OUTPUT HEADING (HED)      NODAL CROSSING PREDICTION PROGRAM

SATELLITE NO. U49      a SPACETRACK - ALTN. 342 EDT

NTYPE = 1      1-1-SPACETRACK OR SMITHSONIAN ELEMENTS

=2-NASA ELEMENTS

NEV = 75 FIRST REVOLUTION OF SATELLITE FROM EPOCH TIME OF THE SPACETRACK BULLETIN

NREV1 = 46 LAST REVOLUTION OF SATELLITE FROM EPOCH TIME OF THE SPACETRACK BULLETIN

33T = 118.690241800 HGT=39125=T(39125 IS JULIAN DAYS FOR JAN 1966,T IS THE EPOCH TIME

X4 = 21.3.7818.0000 MEAN ANOMALY IN DEGREES

RA = 234.2461.0000 RIGHT ASCENSION OF ASCENDING NODE IN DEGREES

OMEGA = 153.7564.0000 ARGUMENT OF PERIGEE IN DEGREES

E = C. 57089100.0 ORBIT ECCENTRICITY

A = 12.7677165632 MEAN MOTION IN REVOLUTIONS/DAY

3 = 0.255741 RATE IN CHANGE OF A

RA1 = -3.46557.0032 RATE OF CHANGE OF RA IN DEGREES/DAY

OMEGAI = 3.319520.0 RATE OF CHANGE OF OMEGA IN DEGREES/DAY

GAH = 99.210.00.0 GREENWICH HOUR ANGLE OF ARIES AT NIGHT

Z-AM1 = 134.2.00.0 LONGITUDE OF NORTHBOUND NODAL CROSSING

Z-AM2 = 191.89999962 LONGITUDE OF SOUTHBOUND NODAL CROSSING

D-AMDA = 50.0.00.0 LONGITUDE INTERVAL OF NODAL CROSSING

C-R = 4.0.0.0 DIFFERENCE BETWEEN LOCAL TIME AND GREENWICH TIME

**Sample Output for the Nodal Crossing Prediction Program**

SATELLITE NO. 849 - CROSSING PREDICTION PROGRAM

EPJD TIME = 116.062 DAYS

LAMBDAZI = 134.2

DAY	HR.	MIN.	SEC.	LAMBDA	DAY	HR.	MIN.	SEC.	LAMBDA	DAY	HR.	MIN.	SEC.	LAMBDA
124	2	29	.4	1.6.35	123	6	.1	.42	177.51	132	22	.38	.54	87.95
124	4	22	.64	134.86	126	7	.53	.21	206.02	133	1	.31	.32	116.45
124	6	15	.14	153.38	128	9	.45	.60	234.53	133	2	.24	.9	144.96
124	8	7	.54	191.69	129	0	.47	.9	102.61	133	4	.16	.47	173.46
124	10	2	.54	22.41	129	2	.39	.43	131.11	133	6	.9	.24	201.97
125	1	1	.22	95.52	129	4	.32	.27	159.62	133	8	.2	.2	230.47
125	2	54	.52	117.63	129	6	.25	.5	186.13	133	23	.3	.1	98.50
125	4	47	.11	145.55	129	8	.17	.44	216.64	134	0	.55	.35	127.00
125	6	39	.51	174.16	129	18	.51	.51	84.71	134	2	.48	.15	155.51
125	8	32	.71	2.2.57	13	1	.11	.37	113.21	134	4	.4	.53	184.01
125	10	25	.1	231.19	13	3	.4	.8	141.72	134	6	.35	.30	212.51
126	1	26	.25	99.19	13	4	.50	.47	170.23	134	8	.26	.7	241.02
126	3	19	.6	127.7	13	6	.47	.25	198.74	134	23	.27	.4	109.04
126	5	11	.45	156.22	13	8	.42	.3	227.24	135	1	.19	.41	137.54
126	7	4	.45	194.73	13	23	.43	.9	95.3	135	3	.12	.16	166.04
126	8	57	.4	213.24	131	1	.35	.47	125.61	135	5	.4	.55	194.55
126	10	49	.43	241.75	131	3	.24	.25	152.32	135	6	.57	.32	223.05
127	1	57	.57	1.9.65	131	5	.21	.3	180.82	135	21	.58	.26	91.06
127	3	43	.6	138.36	131	7	.13	.41	209.53	135	23	.51	.3	119.56
127	5	36	.15	156.87	131	9	.6	.19	237.64	136	1	.43	.43	148.06
127	7	28	.45	195.38	132	0	.7	.22	105.49	136	3	.36	.17	176.56
127	9	21	.64	223.69	132	1	.57	.60	131.37	136	5	.28	.53	205.06
128	0	22	.46	91.98	132	3	.62	.38	162.9	136	7	.21	.30	235.57
128	2	15	.4	12.49	132	5	.43	.15	191.4	136	22	.22	.22	101.57
128	4	8	.3	149.1	132	7	.37	.53	219.01	137	14	.59	.59	130.07

PASS NO. 75 - 460

DELTA LAMBDA = 50.000

NODAL CROSSING PREDICTION PROGRAM  
 SATELLITE NO. 049 - SPACETRACK - 3LTN. 342 EDT

EPJCH TIME = 118.089,2 DAYS

LAMBDAZI = 134.2 JU

PASS NO. 75 " 460  
 DELTA LAMBDA = 50.000

	LAMBDAZ2 = 191.900			LAMBDAZ1 = 191.900										
DAY	HR.	MIN.	SEC.	DAY	HR.	MIN.	SEC.	LAMBDA	DAY	HR.	MIN.	SEC.	LAMBDA	
141	20	35	59	96.9	144	21	46	33	128.11	148	0	49	9	187.68
141	22	28	34	125.39	144	23	39	8	156.60	148	2	41	42	216.17
142	0	21	9	153.89	145	1	31	42	185.10	148	19	34	43	112.55
142	2	13	44	192.38	145	3	24	16	213.59	148	21	27	16	141.04
142	4	6	19	21.87	145	20	17	24	110.1	148	23	19	49	169.52
142	5	58	54	239.37	145	22	9	58	136.49	149	1	12	22	198.01
142	20	59	34	107.32	146	0	2	32	166.98	149	3	4	55	226.49
142	22	52	9	135.81	146	1	55	6	195.47	149	18	5	20	94.38
143	0	44	44	164.3	146	3	47	40	223.96	149	19	57	53	122.87
143	2	37	18	192.80	146	18	48	11	91.87	149	21	50	26	151.35
143	4	29	53	221.29	146	20	4	45	120.36	149	23	42	59	179.84
143	19	30	31	89.23	146	22	33	18	148.85	15	1	35	32	208.32
143	21	23	5	117.72	147	0	25	52	177.34	15	3	28	5	236.81
143	23	15	40	146.22	147	2	18	26	205.83	15	16	28	27	104.68
144	1	8	15	174.71	147	4	1	61	234.31	15	20	21	0	133.17
144	3	0	49	23.2	147	19	11	29	102.22	15	22	13	33	161.65
144	4	53	24	231.69	147	21	4	2	130.71	151	0	6	5	190.14
144	19	53	59	99.62	147	22	56	35	159.19	151	1	58	38	218.62

E. Orbit Prediction Program

1. Introduction

The Orbit Prediction Program simulates the trajectory of an earth-orbiting satellite and computes the radar look angles for the satellite. The satellite trajectory is generated from the SPACETRACK orbital elements and parameters obtained from the Nodal Crossing Prediction Program. A description of the Orbit Prediction Program is contained in the document: "Nodal Crossing Prediction Program", Technical Memorandum No. EMA-TM-66-9, March 1967, by John C. Cleary and Paul E. Brown, 1st Lt.

2. Computer Program Operating Environment

a. Computer

Honeywell 6180

b. Source Language

FORTRAN Y under GCOS.

c. Memory Requirement

32K words

d. Typical Processing Time Required

0.005 hours (18 seconds)

e. Peripheral Equipment Requirement

Two disc files (file codes: 01, 02)

f. Non-system Subroutines Required

OUT1

OUT2

OUT3

PARALX

NEWT

CLEAR

OUT4

3. Inputs

The following set of input parameters is required for execution of the Orbit Prediction Program:

NAMELIST IN1

HED - Array containing the heading for the output from a program run. The dimension of HED is 24.

NAMELIST IN2

NRUN - Run number assigned to pass.

NPRLX - Used in original version of program, no longer valid. If not 0, a punched paper tape for parallax correction of a transportable station would be produced.

NDL - Number of passes to be computed. First the on time pass, then the one for  $\lambda + \Delta\lambda$ , then  $\lambda - \Delta\lambda$ ,  $\lambda + 2\Delta\lambda$  and finally  $\lambda - 2\Delta\lambda$ . Normally use 2.

NOPT - If = 0, Subroutine OUT3 is not called. If = any other number, Subroutine OUT3 is called to print out the satellite orbit look angles, range, azimuth, elevation, and also Subroutine OUT4 is called to place this look angle data on a file for later plotting.

NDCH - Program division check.

NAMELIST IN3

DAY - Day of year, nodal crossing time.

THR - Hour of day, nodal crossing time.

TMIN - Minute of hour, nodal crossing time.

TSEC - Second of minute, nodal crossing time.

AMDA0 - Longitude of nodal crossing (deg.).

BGT0 - Epoch time of nodal crossing.

DAMDA -  $\Delta\lambda$  (-.5 degrees is 2 min. early pass, which is normally the second pass).

DT - The interval in seconds between computations.

CHR - If converting GMT to EDT, = 4.0.

If converting GMT to EST, = 5.0.

#### NAMELIST IN4

W0 - Argument of perigee (degrees).  
E0 - Orbit eccentricity.  
ANCL - Orbit inclination (degrees).  
ASMTH - A, mean motion in revolutions/day.  
RA1 - Rate of change of right ascending node (degrees/day).  
W1 - Rate of change of argument of perigee (degrees/day).  
E1 - Rate of change of eccentricity, per day.  
A0 - Semi-major axis of orbit in earth radii.  
A1 - Rate of change of A0 in earth radii/day.

#### NAMELIST IN5

XLAT - Latitude of radar (degrees).  
XLONG - Longitude of radar (degrees).  
AD - Radius of earth at radar in Km.  
AZTH - Maximum allowed azimuth deviation of beam center from satellite position (degrees).  
ALTH - Maximum allowed elevation deviation of beam center from satellite position (degrees).  
ALO - Initial elevation angle of the pass (degrees).  
XLAT1 - Latitude of transportable station (degrees).  
XLONG1 - Longitude of transportable station (degrees).  
TDELAY - Transmitter time delay, used to compute the range mark number. This is a number that describes the setting of 5 switches at the transmitter to get a properly timed range mark for starting the pass.

The following page (Fig. III-3) represents the format for the six card element set from SPACETRACK. The orbital element parameters used in this program (NAMELIST IN4) are obtained from this card set. The orbital parameters needed in the program can also be obtained from the two card element set and hand calculation of required parameters missing from the set. Fig. III-4 illustrates this latest format for the SPACETRACK orbital elements. A punched card deck, containing the two card element set, as received by RADC from the Space Defense Center in Colorado is illustrated in Fig. III-5. The first card of the actual deck is the bottom card in the figure.

ELEMENT NUMBER		ELEMENT NUMBER		ELEMENT NUMBER		ELEMENT NUMBER		ELEMENT NUMBER		ELEMENT NUMBER		ELEMENT NUMBER		
SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	SATELLITE NUMBER	NAME	
1	C. SODORISOW	Y. R. GALE (INTERNATIONAL NAME)	A. EST. EL'EMENT NUMBER	2	REVOLUTIONS FROM LAUNCH AT EPOCH, N.	3	DATE OF LAUNCH	4	REFLECTIVITY FACTOR ( $T_{\alpha/\beta}$ )	5	BALLISTIC COEFFICIENT ( $C_D/A$ )	6	ELEMENT NUMBER	
7	SATELLITE NUMBER	MEAN ANOMALY (M) DEGREES AND RIGHT ASCENSION OF NODE ( $\Omega$ ) DEGREES RATIO	8	MEAN MOTION (n) REVOLUTIONS/DAY	9	ARGUMENT OF PERIGEE (W) DEGREES	10	INCLINATION DEGREES	11	ECCENTRICITY $e$	12	DISC. S./DAY	13	ELEMENT NUMBER
14	SATELLITE NUMBER	MEAN MOTION (n) REVOLUTIONS/DAY	15	MEAN MOTION (n) REVOLUTIONS/DAY	16	MEAN MOTION (n) REVOLUTIONS/DAY	17	MEAN MOTION (n) REVOLUTIONS/DAY	18	MEAN MOTION (n) REVOLUTIONS/DAY	19	MEAN MOTION (n) REVOLUTIONS/DAY	20	ELEMENT NUMBER
21	SATELLITE NUMBER	SEMI MAJOR AXIS (a) EARTH RADII	22	EARTH RADII/DAY	23	EARTH RADII/DAY	24	EARTH RADII/DAY	25	EARTH RADII/DAY	26	EARTH RADII/DAY	27	ELEMENT NUMBER
28	SATELLITE NUMBER	ANOMALISTIC PERIOD (P <sub>a</sub> )	29	DRAG TERM (C <sub>a</sub> ) DAYS/REV2	30	PERIGEE HEIGHT KILOMETERS	31	BURN INITIAL REVOLUTION NUMBER, N <sub>0</sub>	32	BURN LIFETIME DAYS	33	BULLETIN EXPIRATION YMDHMS	34	ELEMENT NUMBER
35	SATELLITE NUMBER	DIAG. TERM (C <sub>n</sub> ) DAYS/REV2	36	DIAG. REVOLUTION NUMBER (N <sub>D</sub> )	37	DIAG. TERM (C <sub>n</sub> ) DAYS/REV2	38	DIAG. REVOLUTION NUMBER (N <sub>D</sub> )	39	DIAG. TERM (C <sub>n</sub> ) DAYS/REV2	40	DIAG. REVOLUTION NUMBER (N <sub>D</sub> )	41	ELEMENT NUMBER

**Figure III-3.** Six Card Element Set

Figure III-4. Two Card Element Set

COPY AVAILABLE TO PGC DOES NOT  
PERMIT FURTHER COPIING OR REPRODUCTION

The page, although not completely legible, is included for information purposes only.

Figure III-5. Punched Data Deck Containing the Two Card Element Set

#### 4. Output

There are a number of different output quantities produced during a typical run of the Orbit Prediction Program. By means of Subroutine OUT1 the input heading for the run (variable name HED), the run and pass numbers (NRUN and M), the satellite rise time in hours, minutes, and seconds (MHR, IMIN, and ISEC), the nodal crossing longitude (AMBA), and the epoch time in days (BGT0) are printed out. This is followed by a listing of various radar parameters versus times of visibility of the satellite to the radar. The radar parameters listed are the elevation count period (ECP), azimuth count period (ACP), elevation angle in degrees and minutes (variable names MELD and MELM), azimuth angle in degrees and minutes (MAZD and MAZM), range in kilometers (R) and return time in milliseconds (RM), and Doppler in kilocycles (DOPLER). For further explanation of the count periods and Doppler refer to the last paragraph of this section.

Subroutine OUT2 produces printout of the input data and parameters associated with the recorder, director, and tracker. The printout from OUT2 occurs on a separate page following the printout from OUT1.

If Subroutine OUT3 is invoked, then additional output of the radar look angles, range, azimuth, and elevation, will be generated for various times of observation of the satellite by the radar. These observation times are separated by the input DT. First the input heading for the run is printed out (variable name HED). Then follows the run and pass number (NRUN and M), nodal crossing time in day of year, hour of day, minute of hour, and second of minute (DAY, THR, TMIN, and TSEC), the nodal crossing longitude (AMBA), and the satellite rise time in hours, minutes, and seconds (MHR, IMIN, and ISEC). After this follows a list of radar parameters versus satellite observation times, separated by intervals of DT. The radar parameters are azimuth in degrees and radians (AZ and AZR), elevation in degrees and radians (ALPH and ELR), and range in kilometers (R).

When NOPT is not equal to 0, Subroutine OUT4 is called. OUT4 will place the radar data printed out by OUT3 on a data file (file code 02) for use in producing off-line plots of range, azimuth, and elevation.

The outputs elevation count period and azimuth count period are the count periods to be set into the programmed antenna tracker elevation and azimuth clocks. These data are used to prepare a magnetic tape that controls an antenna programmed tracker. This tape has pulses recorded at the proper rates to control stepping motors which in turn, position synchros to command pointing angles. The data shown in the output are actually proportional to the required periods between pulses to be recorded on the program tape. The numbers shown are the settings to be entered into present counters to produce pulses at the required spacing for use in preparing the program tape. An additional column shows the requisite Doppler frequency corrections required due to the translational motion of the satellite. These Doppler frequencies are used to cut a Doppler compensator cam for a satellite pass.

```

0010$:IDENT:CLEARY,CONTI ,65121104RADC
0020$:USERID:CLEARYSTHREE .
0030$:LOWLOAD
0040$:OPTION:FORTRAN
0050$:SELECT:CLEARY/00RB
0060$:SELECT:CLEARY/OCLEAR
0065$:SELECT:CLEARY/00UT4
0070$:EXECUTE
0080$:LIMITS:10,32K,-5K,12000
0085$:PRMFL:02,R/W,L,CLEARY/STORE1
0086$:DISC:01,AIR,5L
0090$:DATA:05
0100 $INI
0110 HED(5)=30H   ORBIT PREDICTION PROGRAM ,
0120 HED(13)=54H 1 MIN EARLY   OBJECT NO. 2103 BLTN NO. 7  4/1/66      3
0130 $IN2
0140 NRUN=302,
0150 NPLX=0,
0160 NDL=1,
0170 NOPT=10,
0180 NDCH=-10 $
0190 $IN3
0200 DAY=91.0,
0210 THR=3.0,
0220 TMIN=32.0,
0230 TSEC=57.0,
0240 AMDA0=96.100,
0250 BGT0=36.3134,
0260 DAMDA=0.0,
0270 DT=5.0,
0280 CHR=4.0 $
0290 $IN4
0300 W0=53.070,
0310 E0=0.021690,
0320 ANCL=72.390,
0330 RAI=-2.52163,
0340 W1=-2.16126,
0350 ASMT0=15.67614,
0360 E1=-2.4600E-04,
0370 A0=1.05752,
0380 A1=-2.6600E-04 $
0390 $IN5
0400 XLAT=43.15250,
0410 XLONG=75.61722,
0420 AD=6365.30,
0430 AZTH=0.100,
0440 ALTH=0.100,
0450 XLAT1=0.0,
0460 XLONG=0.0,
0470 TDELAY=25.0 $
0480$:ENDJOB
0490***EOF

```

Sample Job Stream for the Orbit Prediction Program

**RADC FORM 0-56 PREVIOUS EDITION WILL BE USED**  
**APR 69**

## HIS-6000 Batch Submittal Form

III-190

**Source Listing of the Orbit Prediction Program**

```

C ORBIT PREDICTION - MAIN PROGRAM 00001000
DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500), 00001010
    THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750); 00001020
    HED(24),XLAM(5) 00001030
COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,ECP,HED,XLAM,T0,DT, 00001040
    CTO,AMDA,AMDA1,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD, 00001050
    SANCL,CANCL,SLAT,CLAT,RLONG,L,M,J,TH,AMDA,AMBA,E,V,PHIG, 00001060
    CTH,TH,DELL,SD,CD,CDL,SDL,COSB,SINE,TANALF,RSQ,COSAZ,TAZ, 00001070
    NN,N1,N2,XW,XL,XE,RAMDA,RW,CPO,PHIO,SP0,STH,X,SINAZ,RW1, 00001080
    SPHI,CON,AZTH,ALTH,AL0,I,IALS,JJ,KKIN#2,OPT,DELN,GAMN, 00001090
    MMIN,MSEC,DPLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1 00001100
COMMON NRUN,NPRlx,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CHR,PI,RA1, 00001110
    RAD,NA,VB,NC,ND,NE,RRATE,BGTO,A0,A1,XLAT1,XLONG1,TDELAY, 00001120
    DOPLER,V,INDX,TMTP,NERL,CTIME,ASMTA,RLONG1,SLAT1,GLAT1 00001130
NAMELIST/IN1/HED 00001140
NAMELIST/IN2/NRUN,NPRlx,NDL,NOPT,NDCH 00001150
NAMELIST/IN3/DAY,THR,TMIN,TSEC,AMDA,CGTO,DAMDA,DT,CHR 00001160
NAMELIST/IN4/W0,E0,ANCL,ASMTA,RA1,W1,E1,A0,A1 00001170
NAMELIST/IN5/X_AT,XLONG,AD,AZTH,ALTH,AL0,XLAT1,XLONG1, 00001180
*TDELAY 00001190
LOGICAL SL1 00001200
DATA EST,EDT/4H EST,4H EDT/,XRLY,XLTE/5HBARLY,4HLATE/ 00001210
DATA BLANK/6H / 00001220
1 CALL CLEAR(TM,INDX) 00001230
DO 99 II=1*24 00001240
HED(I)=BLANK 00001250
99 END Continue 00001260
PI = 3.1415926536 00001270
RAD = .0174532925 00001280
SL1 = .FALSE. 00001290
AB = 6378.174 00001300
2 READ(05,IN1,END=999) 00001310
00001320
READ(05,IN2) 00001330
00001340
NAMELIST - IN2 00001350
00001360
00001370
NRUN = RUN NUMBER ASSIGNED TO PASS 00001380
NPRlx = IF NOT 0, PUNCHED PAPER TAPE FOR PARALLELX 00001390
CORRECTION OF TRANSPORTABLE STATION WILL BE COMPUTED 00001400
NDL = NUMBER OF PASSES TO BE COMPUTED, FIRST THE ON TIME 00001410
PASS, THEN ONE FOR LAMDA+ DELTALAMDA, THEN LAMDA- DELTALAMDA, 00001420
LAMDA+2DELTALAMDA, THEN LAMDA- 2DELTALAMDA. NORMALLY USE 2 00001430
NOPT = 0, SUBROUTINE OUT 3 IS NOT CALLED 00001440
NOPT = ANY OTHER NUMBER, SUBROUTINE OUT3 IS CALLED 00001450
ALSO SUBROUTINE OUT4 IS CALLED FOR PLOTTING 00001455
READ(05,IN3) 00001460
00001470
00001480
00001490
00001500
NAMELIST - IN3

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C DAY = DAY OF YEAR           NODAL CROSSING TIME
C TMR = HOUR OF DAY          NODAL CROSSING TIME
C TMIN = MIN. OF HOUR        NODAL CROSSING TIME
C TSEC = SEC. OF MIN.         NODAL CROSSING TIME
C BMDAO = LONGITUDE OF NODAL CROSSING
C BTGTO = EPOCH TIME OF NODAL CROSSING
C DMDA = DELTA LAMDA (-.5DEGREES IS 2 MIN? EARLY PASS,
C WHICH IS NORMALLY THE SECOND PASS
C DT = 30.0, THE INTERVAL IN SECONDS BETWEEN COMPUTATIONS
C CWR = 4.0 IF CONVERTING GMT TO EDT
C BWR = 5.0 IF CONVERTING GMT TO EST

C READ(05,IN6)

C NAMELIST - IN4

C WO = ARGUMENT OF PERIGEE, DEGREES
C EO = ORBIT ECCENTRICITY
C ANCL = ORBIT INCLINATION, DEGREES
C ASMTH = A, MEAN MOTION, REVOLUTIONS/DAY
C BA1 = RATE OF CHANGE OF RIGHT ASCENDING NODE, DEGREES/DAY
C W1 = RATE OF CHANGE OF ARGUMENT OF PERIGEE IN DEGREES / DAY
C E2 = RATE OF CHANGE OF ECCENTRICITY, PER DAY
C X0 = SEMIMAJOR AXIS OF ORBIT IN EARTH RADII
C AE = RATE OF CHANGE OF AO IN EARTH RADII/DAY

C READ(05,IN5)

C NAMELIST - IN5

C MLAT = LATITUDE OF RADAR
C MLONG = LONGITUDE OF RADAR
C RD = EARTHS RADIUS AT RADAR IN KM
C AZTH = MAXIMUM ALLOWED AZIMUTH DEVIATION OF BEAM
C CENTER FROM SATELLITE POSITION
C ELTH = MAXIMUM ALLOWED ELEVATION DEVIATION OF BEAM
C CENTER FROM SATELLITE POSITION
C ALO = INITIAL ELEVATION ANGLE OF THE PASS
C MLAT1 = TRANSPORTABLE STATION LOCATION, LATITUDE
C MLONG1 = TRANSPORTABLE STATION LOCATION, LONGITUDE
C TDELAY = TRANSMITTER TIME DELAY, USED TO COMPUTE THE RANGE
C MARK NUMBER( A NUMBER THAT DESCRIBES THE SETTING OF
C 5 SWITCHES AT TRANSMITTER TO GET A PROPERLY TIMED
C RANGE MARK FOR STARTING THE PASS).

C TMTP = EST
C IF (CHR.EQ.4.) TMTP = EDT
C NDL = MIN(NDL,5)
C T0 = 3600.0+THR+60.0*TMIN+TSEC
C CT0 = DAY+(THR*CHR)/24.0+TMIN/1440.0+TSEC/86400.0-BGTO

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C      AMDA1 = 360.983-RA1          00002030
      86400 = SECONDS IN A DAY      00002040
      P = 86400.0/AS4TH          00002050
3      S4NCL = SIN (ANCL*RAD)      00002060
      C4NCL = COS (ANCL*RAD)      00002070
      SLAT = SIN (XLAT*RAD)      00002080
      CLAT = COS (XLAT*RAD)      00002090
4      XLONG = XLONG*RAD          00002100
      SLAT1 = SIN(XLAT1*RAD)      00002110
      CLAT1 = COS(XLAT1*RAD)      00002120
      XLONG1 = XLONG1*RAD          00002130
      B4MDA = AMDA1*RAD/86400.0    00002140
      BW1 = W1*RAD/86400.0        00002150
      L = 1                         00002160
      H = 1                         00002170
5      T = T0                      00002180
      E = E0+CT0+E1              00002190
      AMDA = AMDAO              00002200
      W = W0+W1*GT0+720.0        00002210
      A = AB*(A0+CT0*A1)        00002220
      W = AMOD(W,360.0)          00002230
      BW = W*RAD                00002240
      ERO = (E+COS (RW))/(1.0+E*COS (RW)) 00002250
      BPO = SIGN (SQRT (1.0-CP0**2),SIN (RW)) 00002260
      IF(CP0)501,500,502        00002270
500    PMIO = SP0*PI/2.0-PI       00002280
      GO TO 503                  00002290
501    PMIO = -PI*ATAN(SPU/CP0)   00002300
      GO TO 503                  00002310
502    PMIO = -AMOD(ATAN(SPO/CP0)+2.0*PI,2.0*PI) 00002320
503    CON= E*SP0+PHIG          00002330
6      KLM(1) = AMDA*RAD          00002340
      KLM(2) = (AMDA+DAMDA)*RAD  00002350
      KLM(3) = (AMDA-DAMDA)*RAD  00002360
      KLM(4) = (AMDA+2.0*DAMDA)*RAD 00002370
      KLM(5) = (AMDA-2.0*DAMDA)*RAD 00002380
7      TM(L) = T                00002390
      V = 2.0*PI*(T-T1)/P+CON    00002400
      IF(V.NE.0.0)GO TO 9        00002410
8      PMI(L) = 0.0              00002420
      GO TO 10                   00002430
9      PMIG = V/(1.0-E)          00002440
      CALL NEWT(PHIG,PHI(L),E,V) 00002450
10     STHI = SIN (PHI(L))      00002460
      CTH = (COS (PHI(L))-E)/(1.0-E*COS (PHI(L))) 00002470
      STH = SIGN (SQRT (1.0-CTH**2),SPHI) 00002480
      IF(CTH) 12,11,12          00002490
11     TM = PI-STH*PI/2.0       00002500
      GO TO 17                   00002510
12     TM = ATAN (STH/CTH)      00002520
      IF(TH) 13,13,16          00002530
13     TM = PI*(1.0-CTH) / 2.0  00002540

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14	IF(TH-THETA(L-1)) 14,17,17	00002550
14	TM = 2.0*PI	00002560
	GO TO 17	00002570
15	TM = TH + 3.5*PI+SIGN ((PI/2.0),CTH)	00002580
	GO TO 17	00002590
16	TM = TH+PI/2.0-SIGN ((PI/2.0),CTH)	00002600
17	THETA(L) = TH	00002610
	RHO(L) = A*(1.0-E*COS (PHI(L)))	00002620
18	DELL = RW*RW1*RT-T0)*THETA(L)	00002630
	SD = COS (D(L))	00002640
	SD = SIN (D(L))	00002650
	CDL= COS (DELL)	00002660
	SDL = SIN (DELL)	00002670
	UN = 0	00002680
	T(CD) 181,180,181	00002690
180	R = SIGN (PI/2.0,CANCL+SD)	00002700
	GO TO 182	00002710
181	R = ATAN (CANCL+SD/CD)	00002720
182	IF(X=CANCL) 183,19,19	00002730
183	R = X-SIGN (PI,X)	00002740
19	SE = SANCL-SLAT+SD*CLAT*CDL+CD+CANCL*CLAT*SDL+SD	00002750
	SINE = SQRT (1.0-COSE**2)	00002760
	IF(SINE,NE.0.) GO TO 20	00002770
	TANALF = 10.0E+30	00002780
	GO TO 21	00002790
20	TANALF = (COSE-AD/RHO(L))/SINE	00002800
21	IF(TANALF) 22,25,25	00002810
22	IF(SL1) GO TO 35	00002820
23	IF(M-1) 24,24,26	00002830
24	T = T+DT	00002840
	GO TO 7	00002850
25	BL1 = .TRUE.	00002860
26	RSQ = AD**2*RHO(L)**2-2.0*AD*RHO(L)*COSE	00002870
	IF(SINE) 28,27,29	00002880
27	COSAZ = 1.0	00002890
	GO To 29	00002900
28	COSAZ = (SANCL+SD-SLAT*COSE)/(CLAT*SINE)	00002910
29	SINAZ = SIGN (SQRT (1.0-COSAZ**2),(X=DELL))	00002920
	IF(COSAZ) 31,30,31	00002930
30	TAZ = SINAZ*PI/2.	00002940
	GO To 322	00002950
31	TAZ = ATAN (SINAZ/COSAZ)	00002960
	IF(TAZ) 320,32,321	00002970
32	TAZ = PI*(1.0-COSAZ)/2.0	00002980
	GO To 322	00002990
320	TAZ = TAZ+1.5*PI+SIGN ((PI/2.0),COSAZ)	00003000
	GO To 322	00003010
321	TAZ = TAZ+PI/2.0-SIGN ((PI/2.0),COSAZ)	00003020
322	AZ(L) = TAZ/RAD	00003030
	ACPH(L) = ATAN (TANALF)/RAD	00003040
	BL = SQRT (RSQ)	00003050
		00003060

83	L = L+1	00003070
	IF(M.LE.1)GO TO 34	00003080
	IF(TM(L).EQ.TM(L-1)+DT)GO TO 18	00003090
34	T = T+DT	00003100
	GO TO 7	00003110
35	BL1 = .FALSE.	00003120
	AMBA = XLAM(M)/RAD	00003130
	EARLY = (AMBA-AMDAO)*4.0	00003140
	NERLY = EARLY+SIGN(,5,EARLY)	00003150
	NERL = IABS(NERLY)	00003160
	ETIME = XRLY	00003170
	IF (NERLY.GT.,0) CTIME = XLTE	00003180
	BALL OUT1	00003190
	BALL OUT2	00003200
	IF (NOPT.NE.0) CALL OUT3	00003210
	IF(NOPT.NE.0)CALL OUT4	00003215
	IF(NPRLX.NE.0)CALL PARALX	00003220
	IF(M.GE.NDL)GO TO 1	00003230
	M = M+1	00003240
	L = 1	00003250
	GO TO 18	00003260
999	CONTINUE	00003270
	STOP	00003280
	END	00003290

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COUT1 ORBIT PREDICTION PROGRAM-SUBROUTINE OUT1          000033
SUBROUTINE OUT1          000033 5
DIMENSION TM('S'),AZ(15),ALPH(1500),R(1500),PHI(1500) 0000331
1     THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750), 0000332
2     HED(24),XLAM(5),ICP(750)          0000333
COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,XXX,HED,XLAM,TO,DT, 0000334
1     CT,AMDA,AMDA1,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD, 0000335
2     SANCL,CANCL,SLAT,CLAT,FLONG,L,W,J,T,W,AMDA,AMB,A,E,V,PHIG, 0000336
3     CTH,TH,DELL,SD,CD,CDL,SDL,COSE,SINE,TANALF,RSQ,COSAZ,TAZ, 0000337
4     NN,N1,N2,KW,XL,XE,AMDA,EW,CFO,PHIO,SPO,STH,X,SINAZ,RW1, 0000338
5     SPHI,CON,AZTH,ALTH,A1,I,IALS,JJ,KK,NO2,OPT,DELN,GAMN, 0000339
6     MMIN,MSEC,DPLR,DEN,DFN,TT,MHF,HR,IMIN,YMIN,ISEC,TMIN,J1 0000340
COMMON NRUN,NPRDX,NDL,NOPT,NDCH,DAY,THR,TSEC,AZTH,CHR,PI,RA1, 0000341
1     RA1,NA,NB,NC,ND,NE,RRATE,BGTO,A0,A1,XLAT1,XLONG1,TDELAY, 0000342
2     DOPLER,N,INDX,TMTP,NRL,CTIME,ASMTK,RLONG1,SLAT1,CLAT1 0000343
1     NN = L-1          0000344
DO 2 I=1,NN          0000345
IF (ALPH(I).LT.AL) GO TO 2          0000346
IALS = I          0000347
GO TO 3          0000348
2 CONTINUE          0000349
      WRITE(6,100) (HEI(I),I=1,24),NRUN,M,TMTP,AMBA,BGTO,NRFL,CTIME 0000350
1000 FORMAT(1H1,29Y12A6/3 X12A6 / 2X7HRUN NO.16,1H-I1,2X11HRISE TIME - 0000351
1     3X5H HRS,3X5H MIN,3X6H SEC. A4,2X8HLAMBDA=F8.3,5H DEG. 0000352
2     2X12H EPOCH TIME =F8.3,5H DAYS,2XI3,5H MIN. A6,4WPASS // 0000353
3     5 X32HORBIT NOT HIGH ENOUGH TO BE SEEN)          0000354
NOPT = 1          0000355
RETURN          0000356
3 DOPLER = .9.* (R(IALS-1)-R(IALS+1))/(TM(IALS+1)-TM(IALS-1)) 0000357
RRATE = .25*DOPLER          0000358
N = R(IALS)/.15+TDELAY          0000359
NA = N/1          0000360
IB = N-1          *NA          0000361
NB = (IB+1-1)/20 + 1          0000362
IC = IB-NB*2 0+3 0          0000363
IF (NB.GE.4) GO TO 4          0000364
NB = IB/2          0000365
IC = IB-NB*2 0          0000366
4 NC = IC/25          0000367
IC = IC-25 *NC          0000368
ND = IC/32          0000369
IC = IC-32*ND          0000370
NE = IC/4          0000371
5 JJ = 1          0000372
KK = IALS+2          0000373
6 DO 7 I=KK,NN-2          0000374
NO2 = (I+KK)/2-1          0000375
DELC = ALPH(NO2)-(ALPH(I)+ALPH(KK-2))/2.0          0000376
IF (ABS(DELN).GT.ALTH) GO TO 2          0000377
GAMN = AZ(NO2)-(AZ(I)+AZ(KK-2))/2.0          0000378
IF (ABS(GAMN).GE.150.0) GAMN = GAMN-STGN(180.0,GAMN)          0000379
          0000380

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    IF (ABS(GAMN),GT,AZTH/COS(RAD*ALPH(N02))) GO TO 8      00003811
7 CONTINUE          00003822
JJ = JJ-1          00003833
GO TO 9          00003844
8 ICP(JJ) = I      00003855
DEN = 3.0*(ALPH(I)-ALPH(KK-2))      00003866
ECP(JJ) = 1080.0*DT*FLOAT(I-KK+2)/DEN      00003877
DFN = 3.0*(AZ(I)*AZ(KK-2))      00003888
IF (ABS(DFN).GE.9.) DFN = DFN-SIGN(1080.0,DFN)      00003899
ACP(JJ) = 1080.0*DT*FLOAT(I-KK+2)/DFN      00003900
JJ = JJ+1          00003911
KK = I+2          00003922
GO TO 6          00003933
9 LLL = 0          00003944
TT = TM(IALS)      00003955
MHR = TT/360.0      00003966
MR = MHR          00003977
IMIN = ABS(TT-360.0*MR)/60.0      00003988
IMIN = IMIN          00003999
ISEC = ABS(TT-360.0*MR-60.0*YMIN)      00004000
MMIN = 0          00004011
MSEC = 0          00004022
INDX = IALS          00004033
MELD = ALPH(INDX)      00004044
MELM = (ALPH(INDX)-FLOAT(MELD))*60.0+.5      00004055
IF(MELM.LT.6.)GO TO 90      00004066
MELD = MELD+1      00004077
MELM = MELM-.5      00004088
90 MAZD = ABS(AZ(INDX))      00004099
MAZM = (ABS(AZ(INDX))-FLOAT(MAZD))*60.0+.5      00004100
IF(MAZM.LT.6.)GO TO 91      00004111
MAZD = MAZD+1      00004122
MAZM = MAZM-.5      00004133
91 MAZD = ISIGN(MAZD,AZ(INDX))      00004144
RM = R(INDX)/15.      00004155
10 IF(MOD(LLI,27).NE.0)GO TO 11      00004166
      WRITE(6,101)(HED(I),I=1,24),NRUN,N,MHR,IMIN,ISEC,TMTP,AMBA,BGTS,      00004177
      1 NERL,CTIME      00004188
1001 FORMAT(1H1,29X12A6/3 X12A6 / 2X7HRUN NO.I6,1H-I1, 2X11HRISE TIME -      00004199
      1 I3,5H HRS.I3,5H MIN.I3,5H SEC. A4, 2X8HLAMEDA =F8.3,5H DEG.      00004200
      2 2X12HEPOCH TIME =F8.3,5H DAYS, 2XI3,6H MIN. A6,4HPASS//      00004211
      3 7X4HTIME,1 X9HELEVATION,10X7HAZIMUTH,9X9HEL. ANGLE,7X      00004222
      4 9HAZ. ANGLE, 9X5HRANGE,15X7HDOPPLER 7X4HTIME/5X9HMIN. SEC.      00004233
      5 7X1HCNTG. PER.1.8X10HCNTG. PER.,7X9HDEG. MIN.7X9HMIN. SEC.      00004244
      6 6X3HKM.6X3HMS.,13X4HK.C.,7X9HMIN. SEC. )      00004255
      IF (LLL.EQ.1) WRITE(6,1002)MMIN,MSEC,MELD,MELM,MAZD,MAZM,R(INDX),      00004266
      1 RM,DOPLER      00004277
1002 FORMAT(I8,I4,I47,I5,I12,I4,F13.3,F9.3,F16.3)      00004288
11 LLL = LLL+1      00004299
INDX1 = INDX          00004300
INDX = ICP(LLI)      00004311
DOPLER = '9.* (R(INDX1)-R(INDX))/((TM(INDX)-TM(INDX1))      00004322

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12 HELD = ALPH(INDX) 000433
13 NELM = (ALPH(TNDR)-FLOAT(HELD))*60.0+.5 000434
14 MAZD = ABS(AZ(INDX)) 000435
15 MAZM = (ABS(AZ(INDX))-FLOAT(MAZD))*60.0+.5 000435
16 MAZQ = ISIGN(MAZD,AZ(INDX)) 000437
17 MM = R(INDX)/.5 000438
18 TT = TM(INDX)-TM(IALS) 000439
19 MMIN1 = TT/6.0 000440
20 ZMIN = MMIN1 000441
21 MSEC1 = ABS(TT-6.0.*ZMIN) 000442
22 MTMP = (6.0*(MMIN1+MMIN)+MSEC1+MSEC)/2 000443
23 MSEC2 = MOD(MTMP,6.) 000444
24 MMIN2 = (MTMP-MSEC2)/60 000445
25 MMIN = MMIN1 000446
26 MSEC = MSEC1 000447
27 WRITE(6,103)ECP(LLL),ACP(LLL),DOPPLER,MMIN2,MSEC2,MMIN,MSEC,HELD,
28 1 NELM,MAZD,MAZM,R(INDX),RM 000448
29 1003 FORMAT(F29.,F18.,F71.3,I8,I4/I8,I4,I47,I5,I12,I4,F13.3,F9.3) 000449
30 IF (LLL.LT.JJ) GO TO 10 000450
31 RETURN 000451
32 END 000452
33 000453

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COUT2 ORBIT PREDICTION PROGRAM-SUBROUTINE OUT2          00004543
C                                         00004545
SUBROUTINE OUT2                                         00004550
DIMENSION TM(15),AZ(15),ALPH(1500),R(1500),PHI(1500),      00004560
1     THETA(1500),BHT(1500),B(1500),ECP(750),ACP(750),      00004577
2     HED(24),XLAM(8)                                         00004583
COMMON TM,AZ,ALPH,R,PHI,THETA,BHT,ECP,HED,XLAM,T0,DT,      00004590
1     CT,AMDA,DAMDA,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,      00004610
2     SANCL,CANCL,SLAT,CFLAT,RLONG,L,M,J,T,W,AMDA,AMBA,E,V,PHIQ, 00004610
3     CTH,TH,DELL,SD,CD,CDL,SDL,COSF,SINF,TANALF,RSQ,COSAB,TAB, 00004620
4     NM,N1,N2,RW,XL,XE,RAMDA,RW,CPO,PHIQ,SPO,STH,X,SXNAZ,RWT, 00004630
5     SPHI,COM,XZTH,ALTH,ALO,I,JALS,JJ,KK,NO2,OPT,DELM,GAMN, 00004640
6     MMIN,MSEC,MDLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1  00004650
COMMON NRUN,NPRlx,NDL,NOPT,NDCH,DAY,THR,TSEC,ASMTM,CHR,PI,RA1, 00004660
1     RAD,NA,NC,ND,EE,RRATE,BGTO,AO,A1,XLAT1,XLONG1,TDELAY, 00004670
2     DOPPLER,N,INDX,TMP;NRNL,CTIME,ASMTM,RLONG1,SLAT1,CLAT1  00004680
1     ELMIS = ALPH(IALS)*17.7778                           00004690
2     RZMLS = AZ(IALS)*17.7778                           00004700
RELD = ALPH(IALS)                                         00004710
RELM = (ALPH(IALS)-FLOAT(MELD))*60.0+.5                00004720
RAZD = ABS(A2(TAIS))                                     00004730
RAZM = (ABS(AZ(IALS))-FLOAT(MAZD))*60.0+.5            00004740
RAZD = ISIGN(MAZD,AZ(IALS))                            00004750
RM = R(IALS)/150.                                         00004760
2     WRITE(6,1000)(HED(I),I=1,24)                         00004770
1000 FORMAT(1H1,29X12&6/3 X12A6 //)                   00004780
      WRITE(6,1001)NRUN,M,NRUN,M,MHR,IMIN,ISEC,ALPH(IALS),MHR,IMIN,ISEC, 00004790
1     AN(IALS),MELD,MELM,ELMIS,RM,MAZD,MAZM,ASMLS,R(IALS); 00004800
2     RM,RRATE,NA,NC,ND,NE                               00004810
1001 FORMAT(29X8HRECODER,58X8HDIRECTOR //10X4HDATE,63X4HDATE//10X 00004820
1     1HPASS NUMBER,I0,1H-I1,45X11HPASS NUMBER,I0,1H-I1//10X 00004830
2     9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3,5H SEC.,33X        00004840
3     13HOBJECT NUMBER//10X14HRISE ELEVATION F7.3,8H DEGREES,37X 00004850
4     9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3,5H SEC.,//10X       00004860
5     12HRISE AZIMUTH F9.3,8H DEGREES,37X14HRISE ELEVATION,I3, 00004870
6     5H DEG.,I3,7H MIN.,F11.5,5H MILS//10X11HRANGE AT T0,F10.5, 00004880
7     4H MS.,41X12HRISE AZIMUTH,I5,5H DEG.,I3,7H MIN.,F10.5, 00004890
8     5H MILS//76X11HRANGE AT T0,F8.1,4H KM.,F10.5,4H MS.,//76X 00004900
9     76HRANGE RATE AT T0,F10.5,5H US/S//76X19HRANGE MARK NUMBER 511) 00004910
3     WRITE(6,1002)NRUN,NPRlx,NDL,NOPT,NDCH,NRUN,M,DAY,TMR,TMIN,TSEC, 00004920
1     AMDA,BGT,DAMDA,DT,CHR,MHR,IMIN,ISEC,W0,E0,ANCL,ASMTM,RM, 00004930
2     RA1,W1,E1                                         00004940
1002 FORMAT(/////////3 X7HTRACKER,57X11HINPUT CARDS //10X4HDATE,52X 00004950
1     6HNRUN =I6, 9H NPRlx =I6,7H NDL =I4,8H NOPT =I4, 00004960
2     8H NDCH =I6//10X8HPASS NO,I8,1H-I1,38X5HDAY =F5,0,7H TMR = 00004970
3     F4,0,8H TMIN =F4, ,8H TSEC =F4,0,9H AMDAO =F0.3//10X 00004980
4     8HREEL NO.,52X6HBGTO =F9.4,9H DAMDA =F7.3,6H DT =F4,1, 00004990
5     7H CHR =F3.0//10X9HRISE TIME,I3,5H HRS.,I3,5H MIN.,I3, 00005000
6     5H SEC.,23X4HW0 =F9.4,6H E0 =F9.6,8H ANCL =F7.3, 00005010
7     9H ASMTM =F9.5/71 X11HRANGE AT T0,F10.5,4H MS.,35X6H RA1 = 00005020
8     F9.5,6H G1 =F9.5,6H E1 =FPE12.4)                  00005030
4     WRITE(6,1003)NA,NC,ND,NE,A,A1,RRATE,XLAT,XLONG,AD,ASMTM,ALTH, 00005040

```

```

1 AL01XLAT1 XLONG1 TDELAY 00005050
1003 FORMAT(/10X19H RANGE MARK NUMBER 51,37X4HA0 =F9.5,6H A1 =19E12.4 00005060
1 //10X16H RANGE RATE AT TQ, OFF 10.5,5H US/8,25X6HXLAT =F9.5, 00005070
2 9H XLONG =F9.5,6H AD =F8.2,8H AZTH =F7.3//1CX8MMBLIDIAL 00005080
3 53X6HALTH =F6.3,7H AL =F5.1,9H XLAT1 =F9.5,610H XLONG1 =00005090
4 F9.5//10X5HSTOP TIME,52X8NTDELAY =F7.2 ) 00005100
RETURN 00005110
END 00005120

```

RETURN  
END

```

COUT3 ORBIT PREDICTION PROGRAM-SUBROUTINE OUT3          00005130
C                                         00005135
SUBROUTINE OUT3          00005140
DIMENSION TM(1370),AZ(1500),ALPH(1500),R(1500),PHI(1500), 00005150
1     THETA(1500),RHO(1500),D(1500),ECP(750),ACP(750), 00005160
2     HED(24),XLAM(5)          00005170
COMMON TM,AZ,ALPH,R,PHI,THETA,RHO,D,ECP,ACP,ICP,HED,XLAM,T0,DT, 00005180
1     CTP,AMDA1,AMDA1,AMDA1,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD, 00005190
2     SANCL,CANCL,SLAT,CLAT,RLONG,L,M,J,TW,AMDA,AMBA,E,V,PHIG, 00005200
3     CTH,TH,DELL,SD,CD,CDL,SBL,COSE,SINE,TANALF,RSQ,COSAZ,TAZ, 00005210
4     NN,N1,N2,XW,XL,XE,RAMDA,RW,CP0,PH10,SP0,STH,X,SINAZ,RW1, 00005220
5     SPHI,CON,AZTH,ALTH,AL0,I,IALS,JJ,KK,NQ2,OPT,DELN,GAMN, 00005230
6     MMIN,MSSC,DPLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1 00005240
COMMON NRUN,NPRlx,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CHR,PI,RA1, 00005250
1     RAD,NA,NB,NC,ND,NE,RRATE,BGT0,A0,A1,XLAT1,XLONG1,TDELAY, 00005260
2     DOPLER,N,INDX,TMTP,NERL,CTIME,ASMTA,RLONG1,SLAT1,GLAT1 00005270
1 NSEC = TM(1)-TM(IALS)          00005280
IDT = DT          00005290
N1 = 1          00005300
2 N2=MIND(N1+48,NN)          00005310
WRITE(6,1000) THED(I),I=1,24,NRUN,M,NERL,CTIME,DAY,THR,TMIN,TSEC, 00005320
1     AMBA,MHR,IMIN,ISEC,TMTP          00005330
1000 FORMAT(1H1*29X12A6/30X12A6//5X8HPASS NO: I6*1H-I1,2H -,I2.6H MIN. 00005340
1     A6//25X29HNODAL CROSSING DATA - DAY NO.,F4.0,2H ,F4.0, 00005350
2     5H HRS.,F4.0,5H MIN.,F4.0,16H SEC. - LAMBDA = F9.3 //45X 00005360
3     11HRISE TIME -I4.5H HRS.,I4.5H MIN.,I4.5H SEC.,A4 // 9X 00005370
4     4HTIME,28X7HAZIMUTH,36X9HELEVATION,25X5HRANGE/9X4HSECT,17X, 00005380
5     7HDEGREES,15X7HRADIANS,15X7HDEGREES,15X7HRADIANS,16X3HKM, )00005390
3 DO 4 I=N1,N2          00005400
AZR = AZ(I)*RAD          00005410
ELR = ALPH(I)*RAD          00005420
WRITE(6,1001) NSEC,AZ(I),AZR,ALPH(I),ELR,R1)          00005430
1001 FORMAT(I13,F24.3,F22.5,F21.3,F23.5,F21.2)          00005440
NSEC = NSEC+IDT          00005450
4 CONTINUE          00005460
N1 = N2+1          00005470
IF(N1.LE.NN) GO TO 2          00005480
RETURN          00005490
END          00005500

```

COPRLX ORBIT PREDICTION PROGRAM-SUBROUTINE PARALX

```

C
      SUBROUTINE PARALX
      DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500),
     1          THETA(1500),RHO(1500),D(1500),B(1500),ACP(750),ACP(750),
     2          HED(24),XLAM(9)
      COMMON TM,BZ,ALPH,R,PHI,THETA,RHO,D,B(1500),ACP,ICR,HED,XLAM,T0,BT,
     1          CTO,AMDA2,AMDA1,DAMA2,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,
     2          SANCL,CANCL,SLAT,CLAT,RLONG,L3M,JATTW,AMDA,AMBATE,V,PHIG,
     3          CTH,TH,BELL,SD,CD,CDL,SDL,COSB,SINE,TANALF,RSQ,COSAZ,TAZ,
     4          NN,N1,N2,XW,XL,XE,RAMDA,RH,CP0,PHI0,SPO,STH,X,SINAZ,RW1,
     5          PHI,CON,AZTH7ALT,ALB,I,IALS,JJ,MK,NB2,OPT,DELN,GAMN,
     6          MHIN,MSEC,DPLR,DEN,DFN,TTSHHR,HR,IMIN,YMIN,ISEC,THIN,J1
      COMMON NRUN,NPRlx,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CHR,PI,RA1,
     1          RAD,NA,NB,NC,ND,NE,RRATE,BGTD,AD,A1,XLAT1,XLONG1,TDELAY,
     2          DOPLER,N,INDX,TMTP,NERL,CYTIME,ASHTH,RLONG1,SLAT1,GLAT1
      DIMENSION PAZ(600),PEL(600),EL(3750),AZ1(3250)
      EQUIVALENCE (EL,AZ),(AZ1,R(751))
      RT = 6.25*DT
      NRT = XPT
      XTRA = XPT-FLOAT(NRT)
      NX = 4000
      IF(XTRA.NE.0.0) NX = 1.0/XTRA+.3
      IDT = DT
      LT = L-1
      JTOT = L-IALS
      IF(JTOT.IDT.LE.60) GO TO 1
      WRITE(6,1000) VRJN,M
1000 FORMAT(9HOPASS NO. I7.1H-I1.23H LONGER THAN 60 MINUTES)
      JTOT = 600/IDT
      LT = IALS+JTOT-1
      DO 3 I=IALS,LT
      J = I-IALS+1
      TCON = TM(I)-T0
      DELL = XLAM(M)-RLONG1+RAMDA*TCON
      SD = COS(D(I)))
      SD = SIN(D(I)))
      CDL = COS(DELL)
      SDL = SIN(DELL)
      R = ATAN2(GANCL*SD,CD)
      COSE = SANCL*S_AT1*SD*CLAT1*CDL*CD+CANCL*CLAT1*SDL*SD
      SINE = SQRT(1.0-COSE**2)
      PEL(J) = ALPH(I)-ATAN2(COSE-AD/RHO(I),SINE)/RAD
      COSAZ = 1.0
      IF(SINE.NE.0.0) COSAZ = (SANCL*SD-CLAT1*COSE)/(CLAT1*SINE)
      SINAZ = SIGN(SQRT(1.0-COSAZ**2),R-X-DELL)
      MAZ(J) = AZ(I)-ATAN2(SINAZ,COSAZ)/RAD
      IF(ABS(PAZ(J)).GT.180.J)PAZ(J) = PAZ(J)-SIGN(360.0,PAZ(J))
      3 CONTINUE
      JT = JTOT-1
      R = 0
      T11 = TM(IALS)

```

```

4 DO 7 I=1,JT          00006020
J = I+IALS+1          00006030
T2 = TM(J)            00006040
T2 = T1+DT            00006050
DELAZ = (PAZ(I+1)-PAZ(I))/DT 00006060
DELEL = (PEL(I+1)-PEL(I))/DT 00006070
NRT1 = NPT            00006080
IF(MOD(I,NX),EQ.0) NPT1 = NP*T1+1 00006090
5 DO 6 J=1,NPT1       00006100
K = K+1              00006110
T22 = T11+.08         00006120
AZ1(K) = PAZ(I+1)-(T2-T11)*DELAZ 00006130
EL(K) = PEL(I+1)-(T2-T12)*DELEL 00006140
T21 = T12+.08         00006150
TF(T11.GE.T21) GO TO 7 00006160
6 CONTINUE             00006170
7 CONTINUE             00006180
WRITE(1)NRUN,M,K,MHR,IMIN,ISEC,AMBA 00006190
WRITE(1)(AZ1(I),EL(I),I=1,K)        00006200
RETURN                00006210
END                  00006220

```

G	NERT SATELLITE PREDICTION PROGRAM-SUBROUTINE NEHT#4/26/63	00006230
C		00006235
E	SOLUTION OF EQUATION - Q=X-P*USIN(X) - BY NEWTON-RAPHSON METHOD	00006240
S		00006245
D	ROUTINE NEHT(X,Y,P,Q)	00006250
E	I INITIAL GUESS	00006260
S	V SOLUTION	00006270
1	H = 0	00006280
	X = X	00006290
2	H = X-P*USIN(X)-Q	00006300
	FX = 1.0-P*USIN(X)	00006310
	G = FX/FPX	00006320
3	X = X-H	00006330
4	IF(ABS(H/X)<.000001) 7,7,5	00006340
5	NC = NC+1	00006350
	IF(NC=50) 3,2,6	00006360
6	CONTINUE	00006370
	GO TO 2	00006380
7	X = X	00006390
	RETURN	00006400
	END	00006410

	SUBROUTINE CLEAR	00001000
	SUBROUTINE TO SET FORTRAN LOCATIONS TO ZERO	00001010
	CALLING SEQUENCE - CALL CLEAR(X,Y)	00001020
	THE PURPOSE OF CLEAR IS TO ZERO OUT LOCATIONS X THROUGH Y	00001030
	CLEAR SAVE 1 <sub>0</sub> 4	00001040
	LDA 2 <sub>0</sub> 1	00001050
	SBA 3 <sub>0</sub> 1	00001060
	TPL ORDER	00001070
	LDX4 2 <sub>0</sub> 1	00001080
A2	STZ 0 <sub>0</sub> 4	00001090
	BA4 1 <sub>0</sub> 4	00001100
A2	CMPX4 3 <sub>0</sub> 1	00001110
	TNC A2	00001120
	TZE A2	00001130
	BRETURN CLEAR	00001140
ORDER	LDX4 3 <sub>0</sub> 1	00001150
	LDQ -1,DU	00001160
	ASQ A3	00001170
	TRA A2	00001180
	END	00001190
		00001200

```

COUT4   ORBIT PREDICTION PROGRAM-SUBROUTINE OUT4          00000050
C                                         00030055
      SUBROUTINE OUT4          00000060
      DIMENSION TM(1500),AZ(1500),ALPH(1500),R(1500),PHI(1500),    00000070
      THETA(1500),RH0(1500),D(1500),BCP(150),ACP(750),    00000080
      HED(24),XLAM(5)          00000090
      COMMON TM,AZ,ALPH,R,PHI,THETA,RH0,D,BCP,ACP,ICR,MED,XLAM,T0,BT,    00000100
      CTO,AMDA,AMDA1,AMDA2,W0,W1,E0,E1,ANCL,A,P,XLAT,XLONG,AD,    00000110
      SANGL,CANCL,SLAT,GLAT,GLONG,L,M,J,TWIA,AMBA,AMBA,E,V,PHIB,    00000120
      CYH,TH,DELL,SD,CD,CDL,SDL,COSE,SINE,TANALF,RSQ,COSAZ,TAZ,    00000130
      NN,N1,N2,XW,XL,XE,RAMDA,RW,CP0,PHI0,SM0,STH,X,SINAZ,RW1,    00000140
      SPHI,CON,AZTHJALTH,AL0,I,IALS,JJJ,KK,NO2OPT,DELN,GAMN,    00000150
      MMIN,MSEC,DPLR,DEN,DFN,TT,MHR,HR,IMIN,YMIN,ISEC,TMIN,J1    00000160
      COMMON NRUN,NPRlx,NDL,NOPT,NDCH,DAY,THR,TSEC,AZMTH,CHR,PI,RA1,    00000170
      RADNA,VB,NC,ND,NE,RRATE,BGT0,TA0,A1,XLAT1,XLONG1,TDELAY,    00000180
      DOPLER,V,INDX,THMP,NERL,CTIME,ASMT,H,RLONG1,SLAT1,GLAT1    00000190
      TPN,NN,EQ,0)RETURN
      NSEC = TM(1)-TM(IALS)          00000210
      TOT=DT          00000220
      ENDIND 2          00000230
      WRITE(02)NSEC,DT,NN          00000240
      WRITE(02)(R(IP),IP=1,NN)          00000250
      WRITE(02)(AZ(IP),IP=1,NN)          00000260
      WRITE(02)(ALPH(IP),IP=1,NN)          00000270
      RETURN          00000280
      END          00000290
***EOF          00000310

```

Sample Output for the Orbit Prediction Program

ORBIT PREDICTION PROGRAM									
RUN NO.		RISE TIME - 1 MIN. EARLY		OBJECT NO. 2108 BLTN No. 7		4/1/66 SEC. 47		EPOCH TIME = 06.016 DAYS	
TIME MIN. SEC. 0 0		ELEVATION CNGT. PER. 0 0		AZIMUTH CNGT. PER. 0 0		EL. ANGLE DEG. MIN. 0 0		AZ. ANGLE DEG. MIN. 352 32	
0 40	4539.	3092.	2440.	1951.	1536.	9 56	396 51	1778.261	11.895
1 10	4116.	3557.	1251.	1662.	1365.	11 48	17 54	1998.423	10.643
1 40	3758.	3521.	1062.	1062.	1062.	13 42	24 11	1424.434	9.496
2 10	3665.	910.	796.	708.	708.	15 31	31 30	1266.489	8.443
2 30	4254.	6769.	737.	737.	737.	17 5	39 53	1171.894	7.813
2 50	54337.	680.	1418.	1418.	1418.	18 33	54 1	1088.538	7.297
3 10	-727.	-4669.	983.	1154.	1154.	18 34	68 44	936.690	6.795
3 30	5 0	-3928.	1811.	2282.	2282.	17 12	82 18	995.569	6.446
4 0	6 30	-4093.	2919.	5 27	5 27	15 46	9 9	1058.128	6.177
4 30	5 40	-3928.	1811.	1811.	1811.	14 8	96 56	1135.823	6.245
5 0	6 0	-4644.	2282.	2282.	2282.	12 26	102 43	1225.727	8.172
6 0	6 30	-3998.	1418.	1418.	1418.	9 56	109 46	1378.044	9.197
6 40	7 0	-4269.	2919.	2919.	2919.	7 36	115 18	1545.585	10.304
7 0	-4644.	3770.	5 27	5 27	5 27	5 27	119 41	1723.716	11.491
7 30	-5130.	-5693.	2 51	2 51	2 51	124 15	1972.364	13.149	-118.108
8 10	-5693.	3770.	0 37	0 37	0 37	127 47	2229.388	14.863	-122.086
8 50	-6637.	-26.	-26.	-26.	-26.	0 0	0 0	4235.837	8.55
9 0									

1 MIN EARLY

OBJECT NO. 2108 BLTN NO. 7 4/1/66

RECORDED

DATE

PASS NUMBER 302-1

RISE TIME 12 HRS. 4 MIN. 47 SEC.

RISE ELEVATION 35.03 DEGREES

RISE AZIMUTH 352.53 DEGREES

RANGE AT T0 13.54135 MS.

RANGE AT T0 13.54135 MS.

DIRECTOR

DATE

PASS NUMBER 302-1

OBJECT NUMBER

RISE TIME 12 HRS. 4 MIN. 47 SEC.

RISE ELEVATION 0 DEG. 0 MIN. 0.04861 MILS

RISE AZIMUTH 352 DEG. 32 MIN. .6267.21478 MILS

RANGE AT T0 2031.2 MM. 13.54135 MS.

RANGE RATE AT T0 -0.30566 US/S

RANGE MARK NUMBER 11620

TRACKER

DATE

PASS NO. 302-1

REEL NO.

RISE TIME 12 HRS. 4 MIN. 47 SEC.

RANGE AT T0 13.54135 MS.

RANGE MARK NUMBER 11620

RANGE RATE AT T0 -0.3566 US/S

HELIDIAL

STOP TIME

INPUT CARDS

NRUN = 302 NPLX = 0 NDL = 1 NOPT = 10 NDCH = -10  
DAY = 91. THR = 8. TMIN = 32. TSEC = 57. ANDAO = 96.100  
BGT0 = 86.0164 DANDA = 0. DT = 5.0 CHR = 4.  
W0 = 58.0700 E0 = 0.021690 ANCL = 72.090 ASMTH = 15.67614  
RA1 = -2.52168 W1 = -2.14126 E1 = -2.4600E-04  
AO = 1.05752 A1 = -2.6640E-04  
XLAT = 43.15250 XLONG = 0. AD = 6365.30 AZTH = 0.100  
ALTH = 0.100 AL0 = 0. XLAT1 = 0. XLONG1 = 0.  
TDELAY = 25.00

1 MIN EARLY      OBJECT NO. 2988 BLTN NO. 4/1966

PASS NO. 302-1 - 0 MIN. EARLY

NODAL CROSSING DATA - DAY NO. 91.    8. HRS. 32. MIN. 57. SEC. - LAMBDA = 96.100

RISE TIME - 12 HRS., 4 MIN. 47 SEC. EDT

TIME SEC.	AZIMUTH	ELEVATION	RANGE KM.	
			DEGREES	RADIANS
352.30	6.15282	0.003	0.0005	2031.20
353.011	6.16121	0.316	0.00552	1999.07
353.517	6.16986	0.634	0.0106	1967.08
354.019	6.17880	0.956	0.01669	1935.21
354.447	6.18802	1.283	0.02239	1903.50
355.093	6.19754	1.615	0.02818	1871.94
355.557	6.20738	1.951	0.03406	1840.54
356.240	6.21755	2.293	0.04002	1809.31
356.442	6.22808	2.640	0.04608	1778.26
357.166	6.23896	2.993	0.05224	1747.41
358.112	6.25024	3.351	0.05849	1716.75
358.882	6.26192	3.715	0.06484	1686.32
359.475	6.27401	4.085	0.07130	1656.11
359.96	6.0342	4.461	0.07786	1626.14
7.0	0.01642	4.843	0.08453	1596.42
7.5	0.02994	5.232	0.09131	1566.78
8.0	0.04398	5.627	0.09821	1537.83
8.5	0.05856	6.028	0.10522	1508.97
9.0	0.07372	6.437	0.11234	1480.44
9.5	5.127	6.851	0.11958	1452.26
10.0	6.167	7.273	0.12693	1424.43
10.5	7.045	7.701	0.13440	1397.00
11.0	8.063	8.135	0.14199	1369.97
11.5	9.123	8.576	0.14868	1343.38
12.0	1.228	9.023	0.15748	1317.25
12.5	11.379	9.476	0.16538	1291.61
13.0	12.78	9.934	0.17338	1266.49
13.5	13.829	10.397	0.18146	1241.92
14.0	15.132	10.864	0.18961	1217.94
14.5	16.191	0.28782	0.19783	1194.99
15.0	17.96	11.335	0.20609	1171.89
15.5	19.382	11.808	0.21437	1149.90
16.0	21.954	12.282	0.22266	1128.45
16.5	0.24135	12.757	0.23092	1107.18
17.0	15.132	13.231	0.23913	1088.54
17.5	0.26411	13.701	0.24725	1069.77
18.0	24.182	14.167	0.25525	1051.93
18.5	25.933	14.625	0.26308	1035.06
19.0	27.710	15.074	0.27070	1019.21
19.5	29.575	15.510	0.27806	1001.42
20.0	31.57	15.932	0.28511	990.75
20.5	33.55	16.336	0.29180	978.24
21.0	35.56	16.719	0.29806	966.94
21.5	37.697	17.077	0.30384	956.89
22.0	39.884	17.409	0.30910	948.12
22.5	42.129	0.73529	0.31377	940.88
23.0	44.425	0.77537	0.31781	934.60
23.5	46.769	0.81627	0.32118	929.90
24.0	49.152	0.85787	0.32384	926.61

1 MIN EARLY

ORBIT PREDICTION PROGRAM  
OBJECT NO. 2108 ALTN NO. 4/1/66

PASS NO. 302-1 - 0 MIN. EARLY

NODAL CROSSING DATA - DAY NO. 91. , 8. HRS. 32. MIN. 57. SEC. - LAMBDA \* 96.100

RISE TIME - 12 HRS., 4 MIN. 47 SEC. EDT

TIME SFC.	AZIMUTH DEGREES	AZIMUTH RADIANs	ELEVATION DEGREES	ELEVATION RADIANs	RANGE KM.
245	56.472	0.98562	18.665	0.32577	924.73
251	58.940	1.02870	18.733	0.32694	924.28
255	61.449	1.07179	18.756	0.32736	925.26
261	63.868	1.11471	18.737	0.32792	927.66
265	66.311	1.15734	16.674	0.32593	931.48
271	68.727	1.19951	18.570	0.32411	936.69
275	71.111	1.24111	18.426	0.32160	943.27
281	73.453	1.28199	18.255	0.31843	951.19
285	75.748	1.32206	18.028	0.31465	960.42
291	77.992	1.36121	17.779	0.31030	970.93
295	8.178	1.39938	17.500	0.30544	982.65
301	82.34	1.36448	17.195	0.30010	995.57
305	84.367	1.47248	16.886	0.29436	1019.62
311	86.364	1.5734	16.516	0.28266	1024.76
315	88.294	1.54103	16.149	0.28185	1040.95
321	9.157	1.57354	15.167	0.27518	1058.13
325	91.953	1.488	15.372	0.26830	1076.25
331	93.681	1.63505	14.968	0.26124	1095.27
335	95.344	1.66406	14.556	0.25405	1115.15
341	96.941	1.69194	14.118	0.24675	1135.82
345	98.476	1.71872	13.116	0.23939	1157.26
351	99.949	1.74443	13.292	0.23198	1179.42
355	1.1.362	1.76910	12.665	0.22456	1212.25
361	1.2.718	1.79277	12.441	0.21713	1225.73
365	1.4.019	1.81547	12.317	0.20973	1249.80
371	1.5.266	1.83724	11.595	0.20236	1274.44
375	1.6.463	1.85813	11.175	0.19504	1299.62
380	1.7.611	1.87817	10.759	0.18779	1325.30
385	1.8.713	1.89740	10.347	0.18059	1351.45
391	1.9.770	1.91585	9.940	0.17348	1378.04
395	1.1.785	1.93356	9.536	0.16644	1415.06
401	111.760	1.95158	9.138	0.15949	1432.47
405	112.696	1.96692	8.745	0.15263	1460.24
411	113.596	1.98262	8.357	0.14586	1488.37
415	114.461	1.99772	7.974	0.13918	1516.82
421	115.293	2.01224	7.597	0.13259	1545.59
425	116.093	2.02621	7.225	0.12610	1574.64
431	116.864	2.03966	6.858	0.11970	1603.97
435	117.66	2.05262	6.497	0.11339	1633.55
441	118.321	2.06510	6.141	0.10718	1663.38
445	119.011	2.07713	5.790	0.10105	1693.44
451	119.676	2.08874	5.444	0.09501	1723.72
455	120.317	2.09994	5.103	0.08906	1754.19
461	120.937	2.11075	4.767	0.08319	1784.86
465	121.535	2.12119	4.435	0.07711	1815.72
471	122.114	2.13128	4.106	0.07170	1846.74
475	122.673	2.14144	3.786	0.06648	1877.93
481	123.213	2.15048	3.468	0.06053	1909.26
485	123.737	2.15961	3.154	0.05505	1940.75

1 MIN EARLY    OBJECT NO. 2108 BLTN NO. 7    4/1/66

ORBIT PREDICTION PROGRAM

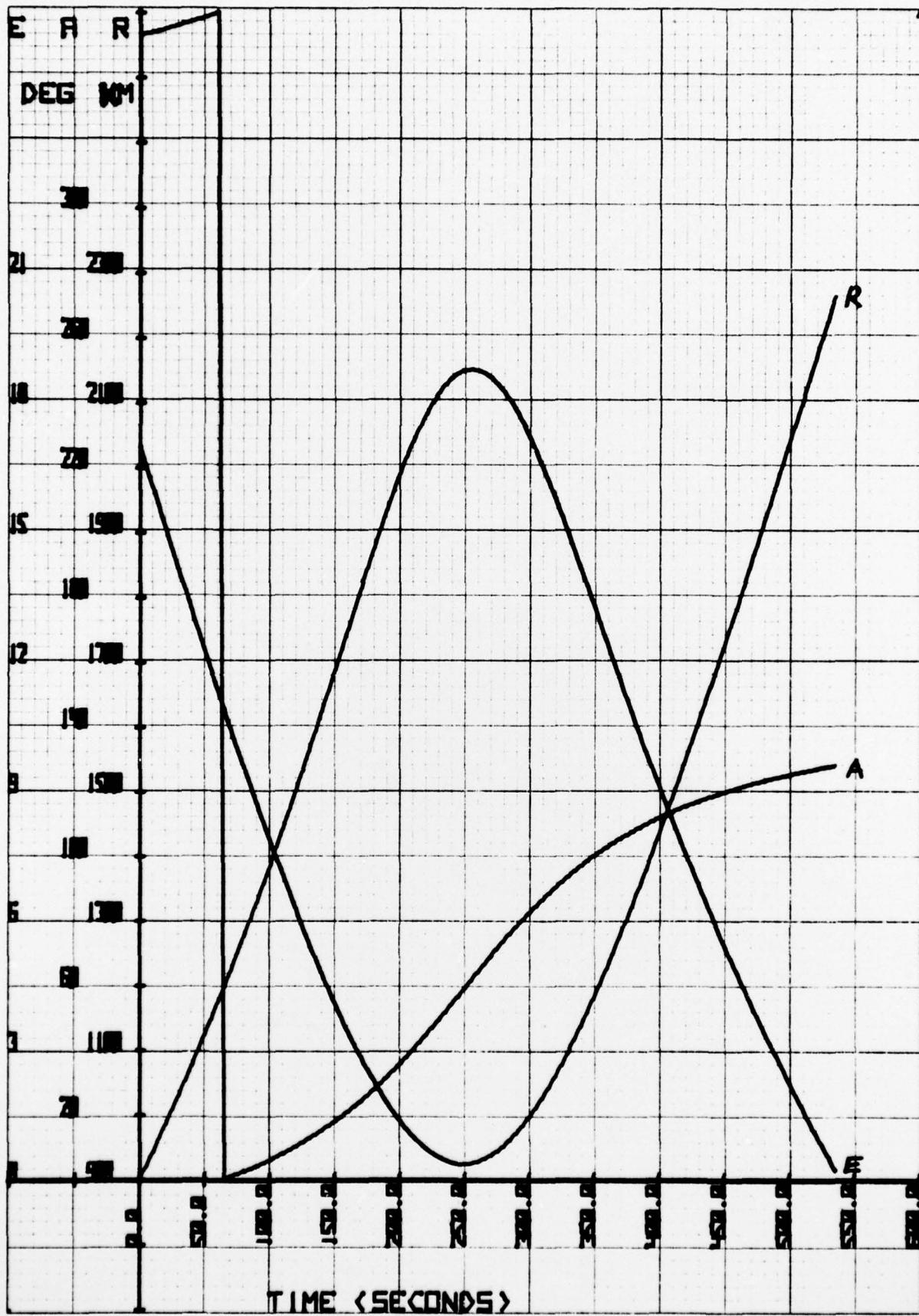
302-1 - 0 MIN. EARLY

RASS NO.    NODAL CROSSING DATA - DAY NO. 91. , 8. HRS. 32. MIN. 57. SEC. - LAMBDA = 96.100

RISE TIME - 12 HRS., 4 MIN. 47 SEC. EDT

TIME SEC.	AZIMUTH DEGREES	AZIMUTH RADIAN S	ELEVATION DEGREES	ELEVATION RADIAN S	RANGE KM.
490	124.243	2.1685	2.845	0.04965	1972.36
495	124.734	2.1770	2.539	0.04432	2004.11
500	125.210	2.1851	2.238	0.03905	2035.98
505	125.671	2.1931	1.940	0.03385	2067.96
510	126.118	2.2011	1.645	0.02872	2100.05
515	126.552	2.2085	1.355	0.02364	2132.25
520	126.973	2.2160	1.067	0.01863	2164.54
525	127.382	2.2234	0.783	0.01367	2196.92
530	127.780	2.2308	0.503	0.00877	2220.39
535	128.166	2.2369	0.225	0.00393	2251.94

**Plot from the Sample Output**



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of  
Rome Air Development Center*

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